1. Suppose we have a Shack-Hartmann system with a relay magnification $m=-1.0$. The lenslet array focal length is 8 mm and the pitch is 0.5 mm . If we measure a wavefront with spherical aberration $W(r, \theta)=W_{040} r^{4}$, with $W_{040}=0.001 \mathrm{~mm}^{-3}$ over a 5 mm diameter pupil, do the following:
(a) Plot the spot positions for a perfect plane wave.
(b) Calculate the spot deviations $\Delta x$ and $\Delta y$ for the aberrated wavefront.
(c) On the plot from part (a), superimpose the spot pattern for the aberrated wavefront.
(d) Use the least squares technique to fit the measured slope values to Zernike polynomials. How does this result compare to the theoretical Zernike representation of the wavefront?
2. A Moiré deflectometry system is shown below (original online). The patterns are separated by a distance of 17.036 mm and the camera is 530 mm from the first grating.
(a) The white sheet of paper is $8.5^{\prime \prime} \times 11$ ". How many pixels $/ \mathrm{mm}$ in the image?
(b) The two gratings are identical. What are the grating periods $g_{1}=g_{2}$ ?
(c) Measure the angle $\theta_{o}$ of the Moiré fringes formed by the two rotated gratings. How does this compare to the theoretical value? By our sign convention $\alpha$ is negative in the image.
(d) The four lenses are placed in contact with the first grating. Measure the angle of the Moiré fringes for each of the lenses. What is the power of each lens?

3. The anterior radius of a test part is 24.5 mm and its diameter is 18.8 mm . Examine the test plate library from Pacific Coast Optics (www.pcoptics.com/servicesLargeTestPlate.html) and specify the plate which best matches the surface. Create a simulation of the Newton's Ring pattern resulting from testing this surface with the chosen test plate. Assume a wavelength of $\lambda=546.1 \mathrm{~nm}$.
4. Download the file Interferograms.zip from the course website. The zip file contains five files in total. Each file is a comma delimited text file that contains the pixel values for the image sensor of an interferometer. The files frame1.csv, frame2.csv, frame3.csv and frame4.csv contain interferograms with phase shifts of $0, \pi / 2, \pi$ and $3 \pi / 2$, respectively. Read in these files and normalize them by 1024 to get the relative intensity at each pixel. The file mask.csv has a value of 1 for valid data and a value of 0 for invalid data.
a) Use the Four-Step algorithm to reconstruct the wrapped phase function $\phi(x, y)$. Use the mask data to hide invalid data. Plot the wrapped phase map.
b) Plot a map of the visibility $\gamma(x, y)$ for the valid data.
c) What is the range of visibility values? Why are some values greater than 1 ?
5. The following page is a non-ISO10110 compliant drawing of a double from Edmund Optics. Based on the details provided on this drawing, create two ISO10110 compliant drawings, one for each of the optical elements. You can just hand sketch the optical elements. A blank ISO10110 sheet is included at the end.

## NOTES:

1. SUBSTRATE:

ELEMENT A: GRADE A FINE ANNEALED SCHOTT: N-BK7 517/642

ELEMENT B: GRADE A FINE ANNEALED SCHOTT: N-SF5 673/322
2. ROHS COMPLIANT
3. CENTERING TOLERANCE (AT 587.6nm) BEAM DEVIATION (HALF ANGLE): <1 ARCMIN
4. COATING (APPLY ACROSS COATING APERTURE)

S1 \& S4: VIS $0^{\circ}$
$R(A V G) \leq 0.4 \%$ FROM 425-675nm @ $0^{\circ}$ AO
S2 \& S3: NONE
5. FINE GRIND SURFACE
6. POWER, IRREGULARITY, AND SURFACE QUALITY SPECIFICATIONS APPLY ACROSS CLEAR APERTURE
7. FOCAL LENGTH (EFL): $100.00 \mathrm{~mm} \pm 2 \%$ BACK FOCAL LENGTH (BFL): 95.92 mm
8. PROTECTIVE BEVEL AS NEEDED
9. DESIGN WAVELENGTH: 587.6 nm
10. ELEMENTS TO BE CEMENTED WITH NORLAND OPTICAL ADHESIVE NOA6


SECTION A-A

FOR INFORMATION ONLY: DO NOT MANUFACTURE PARTS TO THIS DRAWING


## Dimensions in Millimeters



