1. Suppose we have a Shack-Hartmann system with a relay magnification m = -1.0. The lenslet array focal length is 8mm and the pitch is 0.5mm. If we measure a wavefront with spherical aberration  $W(r, \theta) = W_{040}r^4$ , with  $W_{040} = 0.001mm^{-3}$  over a 5mm diameter

pupil, do the following:

- (a) Plot the spot positions for a perfect plane wave.
- (b) Calculate the spot deviations  $\Delta x$  and  $\Delta y$  for the aberrated wavefront.
- (c) On the plot from part (a), superimpose the spot pattern for the aberrated wavefront.
- (d) Use the least squares technique to fit the measured slope values to Zernike polynomials. How does this result compare to the theoretical Zernike representation of the wavefront?
- 2. A Moiré deflectometry system is shown below (original online). The patterns are separated by a distance of 17.036mm and the camera is 530mm from the first grating.
  - (a) The white sheet of paper is  $8.5" \times 11"$ . How many pixels/mm in the image?
  - (b) The two gratings are identical. What are the grating periods  $g_1 = g_2$ ?
  - (c) Measure the angle  $\theta_o$  of the Moiré fringes formed by the two rotated gratings. How does this compare to the theoretical value? By our sign convention  $\alpha$  is negative in the image.

(d) The four lenses are placed in contact with the first grating. Measure the angle of the

Moiré fringes for each of the lenses. What is the power of each lens?



- 3. The anterior radius of a test part is 24.5mm and its diameter is 18.8mm. Examine the test plate library from Pacific Coast Optics (www.pcoptics.com/servicesLargeTestPlate.html) and specify the plate which best matches the surface. Create a simulation of the Newton's Ring pattern resulting from testing this surface with the chosen test plate. Assume a wavelength of  $\lambda = 546.1nm$ .
- 4. Download the file Interferograms.zip from the course website. The zip file contains five files in total. Each file is a comma delimited text file that contains the pixel values for the image sensor of an interferometer. The files frame1.csv, frame2.csv, frame3.csv and frame4.csv contain interferograms with phase shifts of 0, π/2, π and 3π /2, respectively. Read in these files and normalize them by 1024 to get the relative intensity at each pixel. The file mask.csv has a value of 1 for valid data and a value of 0 for invalid data.
  - a) Use the Four-Step algorithm to reconstruct the wrapped phase function  $\phi(x, y)$ . Use the mask data to hide invalid data. Plot the wrapped phase map.
  - b) Plot a map of the visibility  $\gamma(x, y)$  for the valid data.
  - c) What is the range of visibility values? Why are some values greater than 1?
- 5. The following page is a *non*-ISO10110 compliant drawing of a double from Edmund Optics. Based on the details provided on this drawing, create two ISO10110 compliant drawings, one for each of the optical elements. You can just hand sketch the optical elements. A blank ISO10110 sheet is included at the end.

## N

NOTES:									
1. SUBSTRATE: ELEMENT A: SCHC	GRADE A FINE A DTT: N-BK7 517/	NNEALED 642							
ELEMENT B: ( SCHC	GRADE A FINE A DTT: N-SF5 673/3	NNEALED 322							
2. ROHS COMPLIA	ANT .					- 025000	0.000		
3. CENTERING TO BEAM DEVIATIO	LERANCE (AT 58 DN (HALF ANGL	87.6nm): E): <1 ARCMIN			Α ┥		0.025		
4. COATING (APP	LY ACROSS CO	ATING APERTUR	E)			i /		(0.01)	
S1 & S4: VIS ( R(AV) S2 & S3: NOT	)° G) ≤ 0.4% FROM NE	425-675nm @ 0	° AOI	/				S2 & S3	
6. POWER, IRREGI	JLARITY, AND SU S APPLY ACROS	IRFACE QUALITY S CLEAR APERTI	, JRE					S1	
7. FOCAL LENGTH BACK FOCAL L	I (EFL): 100.00m ENGTH (BFL): 95	m ±2% 5.92mm	-			- *			
8. PROTECTIVE BE	VEL AS NEEDED						1		
9. DESIGN WAVEL	ENGTH: 587.6nr	TH: 587.6nm							
10. Elements to be Adhesive Noa	E CEMENTED WI 61	TH NORLAND OI	PTICAL	·					
								ELEMENT A	
					A ┥ —			6.00±0.10 - 2.50±0.10	
<i>FOR INFO</i> DO NOT PARTS T	<u>ORMATI</u> MANUFA O THIS I	<i>on onl</i> Acture Drawin	<u>Y:</u> IG					Section A-A	
SPECIFICATIONS AFTER CEMENTING				SPECIFICATIONS SUBJECT TO CHANGE WITHOUT NOTICE					
ELEMENT TITLE	ELEM	ENT A	ELEM	ENT B			L		
SURFACE		S2		S4	-				
RADIUS	61 47	44 64		129.94	-			Edmund Optics <sup>®</sup>	
SURFACE QUALITY	40 - 20	40 - 20	40 - 20	40 - 20	1		╞╴╼┛		
MIN CLEAR APERTURE	Ø24.00	Ø24.00	Ø24.00	Ø24.00	THIRD ANG		TITLE	25mm Dia. x 100mm FL, VIS 0 Coated, Achromatic Lens	
MIN COATING APERTURE	Ø24.00	N/A	N/A	Ø24.00	PROJECTIC				
POWER AT 632.8nm	3.00 RINGS	3.00 RINGS	3.00 RINGS	3.00 RINGS		mm	DWGNO	A76A1 SHEET	
IRREGULARITY AT 632.8nm	0.50 RINGS	0.50 RINGS	0.50 RINGS	0.50 RINGS	, LE DIVIS IN		DINGINO	4/041 1 OF 1	

Left S	Surface	Mate	rial	Right Surface					
R Ø <sub>E</sub> <b>3</b> / 4/ - 5/ - 6/ -		GLASS: Nd = Vd = 0/ - 1/ - 2/ -		R Ø <sub>E</sub> Ø 3/ 4/ - 5/ - 6/ -					
ISO Element Drawing Indications According to ISO 10110									
DATE 1/25/2016	scale 2.5000:1	DRAWN	APPRV	n Star Star Star Star Star Star Star Star					
32718				Stand and Alexandra and a second and a second se					
PART/DRAWING		REVISION							