

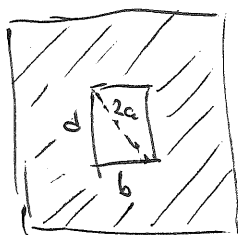
Example: Fraunhofer diffraction of a plane wave striking at rectangular aperture. Find ~~distance~~ irradiance pattern on screen a distance z away.



First let's figure out where the Fraunhofer approximation is valid.

We require

$$N_F = \frac{a^2}{\lambda z} \ll 1$$



The maximum extent of the aperture is along the diagonal so

$$4a^2 = b^2 + d^2$$

Require $\frac{b^2 + d^2}{4\lambda z} \ll 1 \Rightarrow z \gg \frac{b^2 + d^2}{4\lambda}$

If $b = d = 1\text{mm}$ and $\lambda = 0.5\mu\text{m} \Rightarrow z \gg 1\text{m}$

If $b = d = 25\mu\text{m}$ and $\lambda = 0.5\mu\text{m} \Rightarrow z \gg 625\text{m}$

The plane wave incident on the aperture has the form Ae^{ikz} , but this is just A when $z = 0$, so

$$U(x_0, y_0, 0) = A \text{rect}\left(\frac{x_0}{b}, \frac{y_0}{d}\right)$$

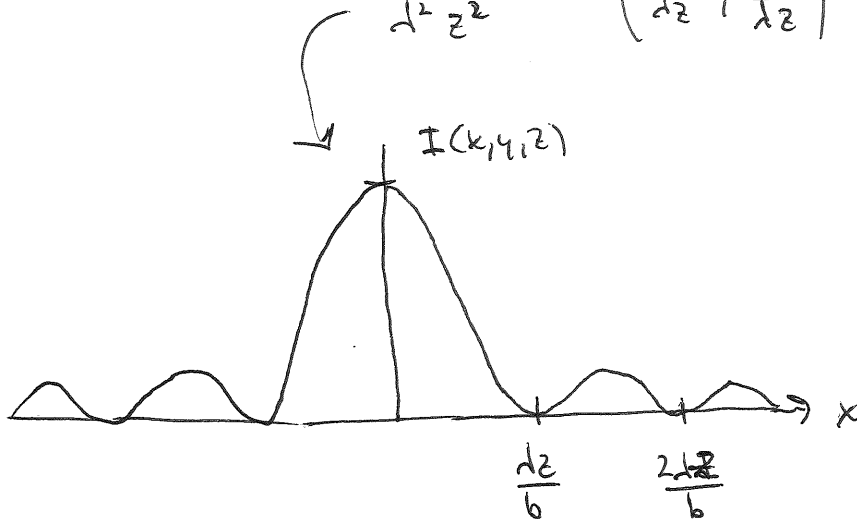
$$\mathcal{F}\{U(x_0, y_0, 0)\} = Abd \text{sinc}(b\xi, d\eta)$$

The spatial frequency variables $\xi = \frac{x}{\lambda z}$ and $\eta = \frac{y}{\lambda z}$. These basically convert the spatial frequency values into spatial coordinates on the plane a distance z away. From the Fraunhofer diffraction formula

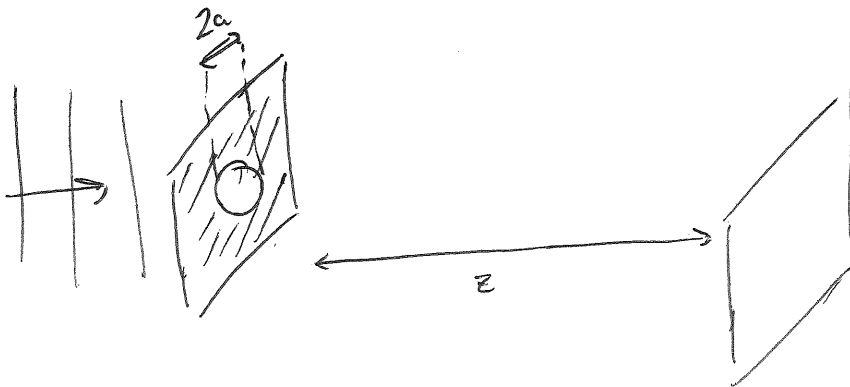
$$U(x, y, z) = A b d \frac{\exp(ikz)}{i\lambda z} \exp\left[\frac{i\pi}{\lambda z}(x^2 + y^2)\right] \text{sinc}\left(\frac{bx}{\lambda z}, \frac{dy}{\lambda z}\right)$$

Irradiance

$$I(x, y, z) = |U(x, y, z)|^2 = \frac{A^2 b^2 d^2}{\lambda^2 z^2} \text{sinc}^2\left(\frac{bx}{\lambda z}, \frac{dy}{\lambda z}\right)$$



Example: Fraunhofer diffraction of a plane wave illuminating a circular aperture. Find the irradiance pattern at distance z .



$z \gg \frac{a^2}{\lambda}$ to have valid approximation

$$U(x_0, y_0, 0) = A \text{cyl} \left(\frac{r}{2a} \right)$$

$$\mathcal{F}\{U(x_0, y_0, 0)\} = (2a)^2 A \frac{\pi}{4} \text{somb}(2ap) \quad \text{where } p = \sqrt{\xi^2 + \eta^2}$$

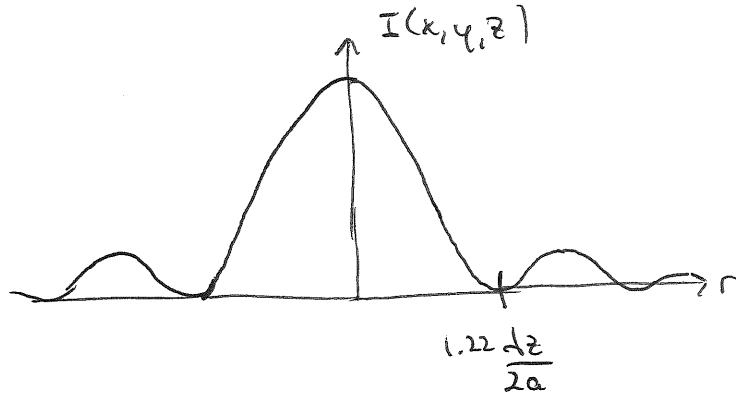
Replace $\xi = \frac{x}{dz}$ $\eta = \frac{y}{dz} \Rightarrow p = \frac{r}{dz}$ $r = \sqrt{x^2 + y^2}$

Our field is

$$U(x, y, z) = \frac{2aA\pi}{dz} \frac{\exp(ikz)}{i dz} \exp\left(\frac{i\pi}{dz} (x^2 + y^2)\right) \text{somb}\left(\frac{2ar}{dz}\right)$$

Irradiance

$$I(x, y, z) = |U(x, y, z)|^2 = \left(\frac{2aA\pi}{dz}\right)^2 \text{somb}^2\left(\frac{2ar}{dz}\right) \quad \text{AIRY PATTERN}$$

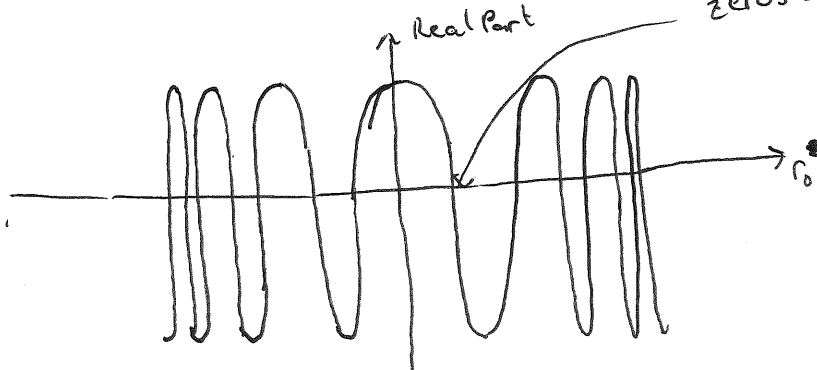


1st zero when $\frac{2ar}{dz} = 1.22$

$$r = 1.22 \frac{dz}{2a}$$

Fraunhofer diffraction requires large distances z which can quickly become impractical. Let's try to understand the term

$$\exp\left[-\frac{i\pi}{dz} (x_0^2 + y_0^2)\right]$$



zeros when $\frac{\pi r_0^2}{dz} = (2m+1)\frac{\pi}{2}$ m integer

$$r_0 = \sqrt{\frac{(2m+1) dz}{2}}$$

Another way to handle the quadratic phase factor is to try and cancel it with a component of the incident field. With Fraunhofer, we just assumed we're really far away. Now we can move into the Fresnel region if an input field is

$$U(x_0, y_0, 0) = U'(x_0, y_0, 0) \exp\left[-\frac{i\pi}{\lambda z} (x_0^2 + y_0^2)\right]$$

with $r_0^2 = x_0^2 + y_0^2$, the Fresnel diffraction integral becomes

$$U(x, y, z) = \frac{\exp(ikz)}{i\lambda z} \exp\left[\frac{i\pi}{\lambda z} r^2\right] \mathcal{F}_{20} \left\{ U'(x_0, y_0, 0) \right\}$$

with $\xi = \frac{x}{\lambda z}$ $\eta = \frac{y}{\lambda z}$

What is this term $\exp\left[\frac{-i\pi}{\lambda z} r_0^2\right]$?

When we looked at spherical waves, we had

$$U(x, y, z) = \frac{A}{r} \exp(ikr)$$

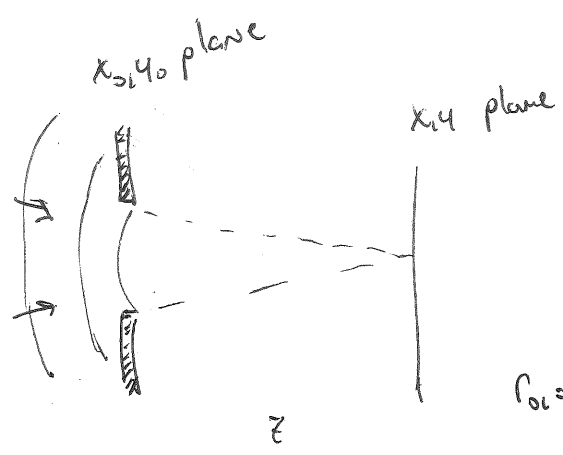
which is an expanding wavefront leaving the origin. We know it's expanding because if we include the time dependence

$$U(x, y, z; t) = \frac{A}{r} \exp(i(kr - \omega t))$$

As t increases, r has to increase to keep the phase of this fraction constant. A surface of constant phase is just the wavefront. If instead we have

$$U(x, y, z; t) = \frac{A}{r} \exp(-i(kr + \omega t)) = \frac{A}{r} \exp(i(-kr - \omega t))$$

then as t increases, then r must decrease to keep the phase term constant. This is a converging ~~but~~ spherical wave.



$$\frac{A}{r_{01}} \exp(-ikr_{01})$$

$$r_{01} = \left[x_0^2 + y_0^2 + z^2 \right]^{1/2}$$

$$r_{01} = z \left[1 + \frac{x_0^2 + y_0^2}{z^2} \right]^{1/2}$$

Converging spherical wave approximation

$$\frac{A}{z} \exp(-ikz) \exp\left[-\frac{i\pi}{2z} (x_0^2 + y_0^2)\right]$$

parabolic wavefront
converging to (0, 0, z)

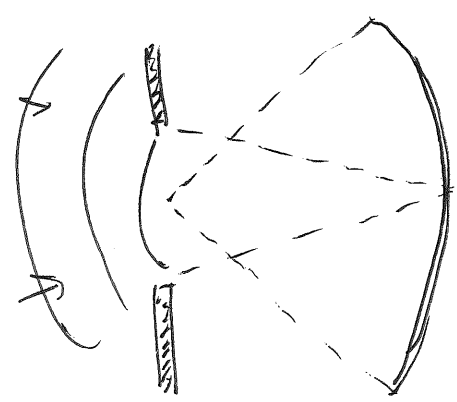
Fresnel Diffraction becomes

$$U(x_1, y_1, z) = \frac{A}{i\lambda z^2} \exp\left[\frac{i\pi}{2z} r^2\right] \int_{z=0} \left\{ U(x_0, y_0, 0) \right\}$$

field introduced to at
plane z=0

Note $A/z^2 \approx$ constant over aperture = Amplitude of spherical wave

So we get something that is related to the Fourier transform, but with quadratic phase in observation plane



If we curved the observation plane, the Fresnel diffraction pattern would just be Fourier transform. often we don't even care about quadratic phase pattern since we are looking at $|U(x_1, y_1, z)|^2$,

COMPLEX FOURIER SERIES REVISITED

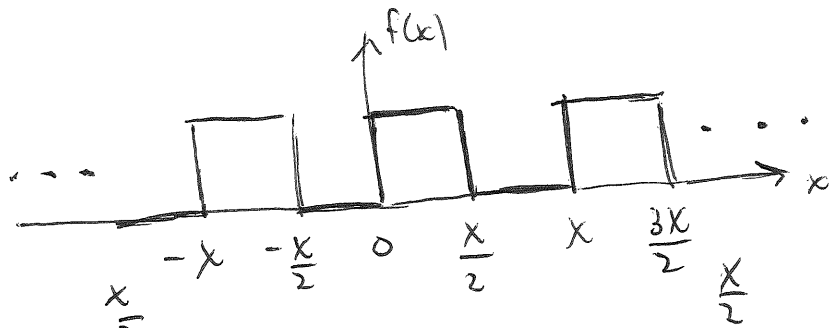
Recall from page (34) of the notes the definition of the complex Fourier series

$$f(x) = \sum_{m=-\infty}^{\infty} a_m \exp(i2\pi m \xi_0 x)$$

where $X = \frac{1}{\xi_0} = \text{period}$

$$a_m = \frac{1}{X} \int_{-\frac{X}{2}}^{\frac{X}{2}} f(x) \exp[-i2\pi m \xi_0 x] dx$$

Let's find the Fourier series of



$$a_{m'} = \frac{1}{X} \int_{-\frac{X}{2}}^{\frac{X}{2}} f(x) \exp[-i2\pi m' \xi_0 x] dx = \frac{1}{X} \int_0^{\frac{X}{2}} \exp[-i2\pi m' \xi_0 x] dx$$

use m' for the moment.

$$a_{m'} = \frac{1}{X} \frac{\exp[-i2\pi m' \xi_0 x]}{-i2\pi m' \xi_0} \Big|_0^{\frac{X}{2}} = \frac{1}{-i2\pi m'} \left[\exp[-im'\pi] - 1 \right]$$

$$a_{m'} = \frac{\exp[-im'\frac{\pi}{2}]}{-i2\pi m'} \left(\exp[-im'\frac{\pi}{2}] - \exp[im'\frac{\pi}{2}] \right)$$

$$a_{m'} = \frac{1}{2} \exp[-im'\frac{\pi}{2}] \text{sinc}\left(\frac{m'}{2}\right)$$

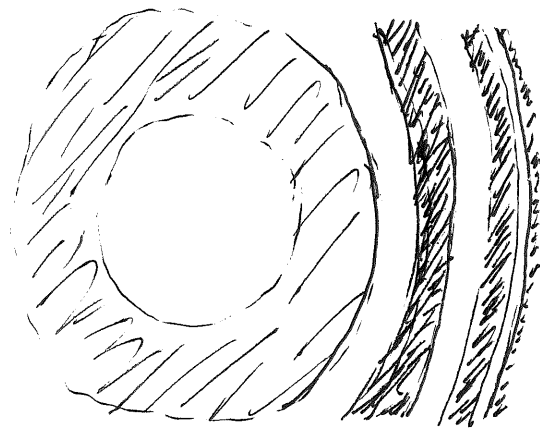
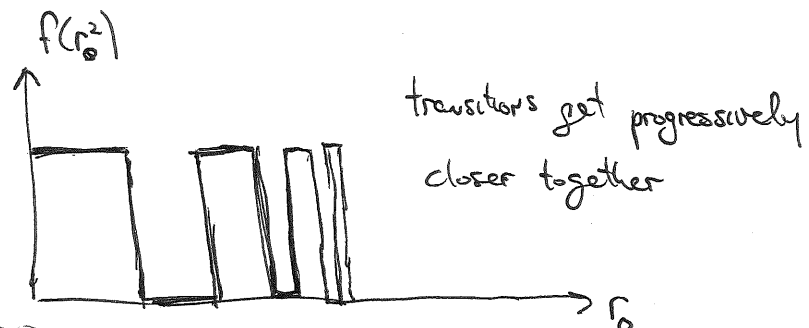
So we can write this example as

$$f(x) = \frac{1}{2} \sum_{m=-\infty}^{\infty} \exp(+im\frac{\pi}{2}) \operatorname{sinc}\left(\frac{m}{2}\right) \exp(-i2\pi m \xi_0 x) \quad \text{let } m = -m'$$

Suppose now I define a transmission mask $t(r)$ where

$$t(r_0) = f(r_0^2) = \frac{1}{2} \sum_{m=-\infty}^{\infty} \exp(+im\frac{\pi}{2}) \operatorname{sinc}\left(\frac{m}{2}\right) \exp(-i2\pi m \xi_0 r_0^2)$$

T	$r_0^2 = x$	r_0
$1 \Rightarrow 0$	$x/2$	\sqrt{x} $\sqrt{\frac{x}{2}}$
$0 \Rightarrow 1$	x	\sqrt{x}
$1 \Rightarrow 0$	$3x/2$	$\sqrt{\frac{3x}{2}}$
$0 \Rightarrow 1$	$2x$	$\sqrt{2x}$



What happens when we put this mask into the Fresnel diffraction formula?

$$U(x, y, z) = \frac{\exp(ikz)}{iz} \exp\left(\frac{i\pi}{2z} r^2\right) \cdot \frac{1}{2} \sum_{m=-\infty}^{\infty} \exp(+im\frac{\pi}{2}) \operatorname{sinc}\left(\frac{m}{2}\right) \exp(-i2\pi m \xi_0 r^2)$$

Ignore finite aperture for the time being.

$$\cdot \int_{-\infty}^{\infty} \left\{ \exp(-i2\pi m \xi_0 r^2) \exp\left(\frac{i\pi}{2z} r^2\right) \right\}$$

with $\xi = \frac{x}{2z}$ $\eta = \frac{y}{2z}$

For the vast majority of terms, the quadratic phase factor will remain. However, there are certain cases where we can get one term to cancel.

If $2\pi m_i^* \frac{z}{\lambda} \neq \frac{\pi}{\lambda} r_0^2$ then the terms cancel

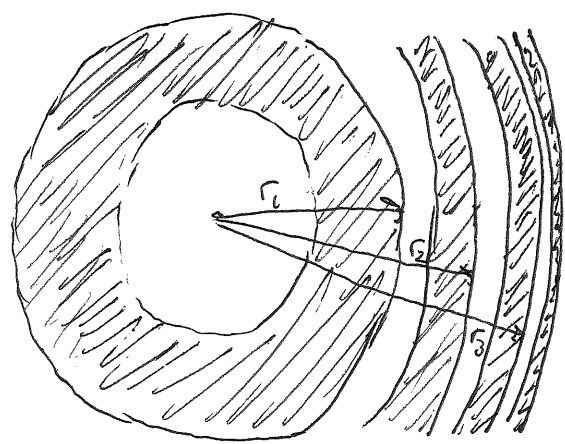
$\frac{1}{\lambda} = X = 2m_i^* \frac{z}{\lambda} \quad m_i^*$ is a specific value of m

So if we build a zone plate with this constraint, the locations of the ~~ring~~ rings (one complete cycle of bright to dark in this case)

are

$r_j^2 = 2j m_i^* \lambda z_{m_i^*} \rightarrow r_j = \sqrt{2j m_i^* \lambda z_{m_i^*}}$

j	r_j
0	0
1	$\sqrt{2m_i^* \lambda z_{m_i^*}}$
2	$\sqrt{4m_i^* \lambda z_{m_i^*}}$
3	$\sqrt{6m_i^* \lambda z_{m_i^*}}$



each of these is called a Fresnel zone.

Fresnel Diffraction

$$U(x, y, z) = \frac{\exp(ikz)}{i\lambda z} \exp\left(\frac{i\pi}{\lambda z} r^2\right) \frac{1}{2} \left[\int_{-\infty}^{\infty} \exp\left(im' \frac{\pi}{\lambda z}\right) \text{sinc}\left(\frac{m'}{2}\right) + \sum_{\substack{m=-\infty \\ m \neq m'}}^{\infty} \exp\left(im' \frac{\pi}{\lambda z}\right) \text{sinc}\left(\frac{m}{2}\right) \right]$$

(Note: The above equation is a simplified representation of the complex integral shown in the image, which includes terms like $\exp\left(\frac{i\pi}{\lambda z} \left(-\frac{m}{m'}\right) r_0^2\right)$ and various cancellations.)

Fresnel Diffraction

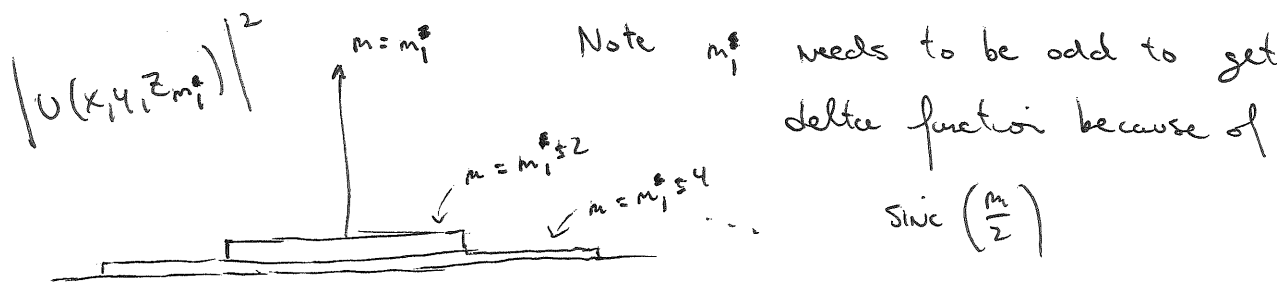
$$U(x, y, z) = \frac{\exp(ikz)}{i\lambda z} \exp\left(\frac{i\pi}{\lambda z} r^2\right) \frac{1}{z} \sum_{m=-\infty}^{\infty} \exp\left(im\frac{\pi}{z}\right) \text{sinc}\left(\frac{m}{z}\right) \mathcal{F}_{2D} \left\{ \exp\left[\frac{i\pi}{\lambda} \left[\frac{m}{m_1^* z_{m_1^*}} - \frac{1}{z}\right] r_0^2\right] \right\}$$

examining the Fourier transform term

When $m = m_1^*$ and $z = z_{m_1^*}$, we have $\mathcal{F}_{2D} \{ 1 \} = \delta\left(\frac{x}{\lambda z_{m_1^*}}, \frac{y}{\lambda z_{m_1^*}}\right)$

All other terms in series still have quadratic phase factor,

From a geometric viewpoint, the incidence at $z = z_{m_1^*}$ looks like



A portion of the incident light is getting focused to a point of the plane $z = z_{m_1^*}$. The remainder is an out of focus "halo" around the point.

If we include an aperture to limit the size of the Fresnel zone plate then this appears in the Fourier transform. For example, a circular aperture of diameter d has in the above

$$\mathcal{F}_{2D} \left\{ \exp\left[\frac{i\pi}{\lambda} \left[\frac{m}{m_1^* z_{m_1^*}} - \frac{1}{z}\right] r_0^2\right] \text{cyl}\left(\frac{r_0}{d}\right) \right\}$$

When $m = m_1^*$ and $z = z_{m_1^*}$

$$\mathcal{F}_{2D} \left\{ \text{cyl}\left(\frac{r_0}{d}\right) \right\} = \frac{d\pi}{4} \text{somb}\left(\frac{dr}{\lambda z_{m_1^*}}\right)$$

delta function becomes Airy pattern in incidence.

Let's look at other distances

$$\frac{m}{m_1^2 z_{m_1^2}} - \frac{1}{z} = 0$$

$$z = \frac{m_1^2 z_{m_1^2}}{m}$$

Again m can only be odd or zero because of $\text{sinc}\left(\frac{m}{2}\right)$

At distances that satisfy this expression, a portion of the light will come into focus. We can think of the Fresnel zone plate as a "lens" with multiple focal lengths. If $f_{m_1^2} = z_{m_1^2}$ is the primary focal length of the zone plate, then the other focal lengths will be

$$f_m = \frac{m_1^2}{m} f_{m_1^2}$$

Note f_m can be positive or negative depending upon the sign of m

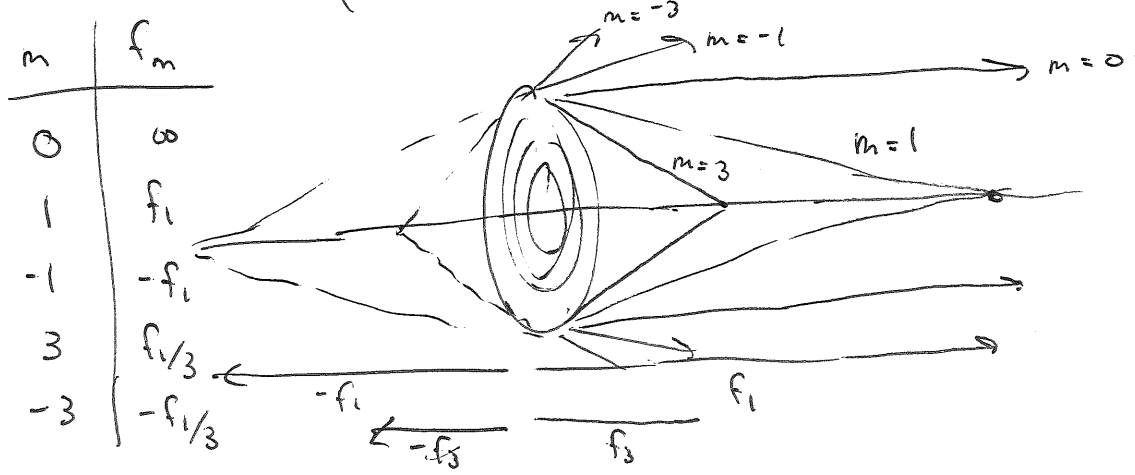
Examples $m_1^2 = 1$

We have the 1st zone of the Fresnel zone plate as

$$r_1 = \sqrt{2df_1} \Rightarrow f_1 = \frac{r_1^2}{2d}$$

So physical dimensions of zone plate define the focal length.

Possible values of $m = 0, \pm 1, \pm 3, \dots$



Each value of m corresponds to a diffraction order. Thus we can refer to the respective foci of the Fresnel zone plate by their diffraction order. The 0^{th} order ($m=0$) is light that passes straight through the zone plate. The $+1^{st}$ order is the primary focal length f_1 . The -1^{st} order has focal length $f_{-1} = -f_1$. The $+3^{rd}$ order has focal length $f_3 = \frac{1}{3} f_1$, etc.

Diffraction Efficiency

We now would like to know how much energy goes into each of these foci. Way back on page (71) of the notes, we described Parseval's theorem for Fourier Series, which says

$$\int_{-\infty}^{\infty} |f(x)|^2 dx = \sum_{n=-\infty}^{\infty} |a_n|^2 \quad \text{in our current notation}$$

The a_n here are the expansion coefficients of our complex Fourier series (Note we have already switched $n \leftrightarrow -n$) in our description from page (143). Parseval's theorem is a statement about conservation of energy. Each term $|a_n|^2$ describes the relative amount of energy going into the n^{th} diffraction order. The sum of all these terms represents the total energy.

For the Fresnel zone plate

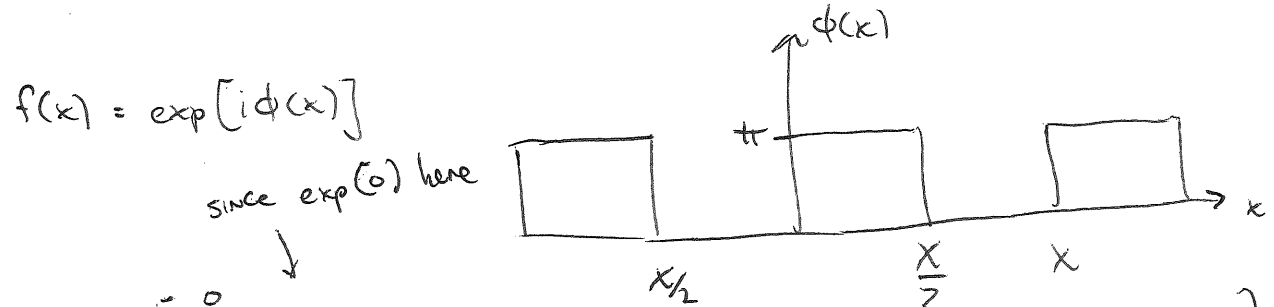
$$a_m = \frac{1}{2} \exp\left[im\frac{\pi}{2}\right] \text{sinc}\left(\frac{m}{2}\right) \quad \boxed{\text{DIFFRACTION EFFICIENCY } R_m} \quad \left| |a_m|^2 = \frac{1}{4} \text{sinc}^2\left(\frac{m}{2}\right) \right|$$

m	N_m	
± 5	0.004	For m even $N_m = 0$
± 3	0.011	25% of the light passes straight through unaffected
± 1	0.101	$\sum_{m=-\infty}^{\infty} a_m ^2 = 0.5$ 50% of the light is blocked by opaque rings
0	0.25	$N_1 = 0.101$ 10.1% of the light goes to primary focal point.

The problem with Fresnel zone plates are that they are highly inefficient, but may be the only choice in some cases like x-rays where limited choices are available for lenses.

FRESNEL ZONE PHASE PLATE (PHASE REVERSAL ZONE PLATE)

Instead of modulating the amplitude, let's use a function that is periodic in phase.



$$a_m = \frac{1}{X} \left[\int_{-\frac{X}{2}}^0 \exp[-i2\pi m \xi_0 x] dx + \int_0^{\frac{X}{2}} \exp[i\pi] \exp[-i2\pi m \xi_0 x] dx \right]$$

$$a_m = \frac{1}{X} \left[\frac{\exp[-i2\pi m \xi_0 x]}{-i2\pi m \xi_0} \Big|_{-\frac{X}{2}}^0 - \frac{\exp[-i2\pi m \xi_0 x]}{-i2\pi m \xi_0} \Big|_0^{\frac{X}{2}} \right]$$

$$a_m = \frac{1}{-i2\pi m} \left[1 - \exp[i m \pi] - (\exp[-i m \pi] - 1) \right]$$

$$a_m = \frac{1}{-im\pi} [1 - \cos m\pi] = i \frac{m\pi}{2} \operatorname{sinc}^2\left(\frac{m}{2}\right)$$

The diffraction efficiency is now

$$\eta_m = |a_m|^2 = \left(\frac{m\pi}{2}\right)^2 \operatorname{sinc}^4\left(\frac{m}{2}\right)$$

m	η_m
± 5	0.016
± 3	0.045
± 1	0.405
0	0

For m even $\eta_m = 0$ including $\eta_0 = 0$

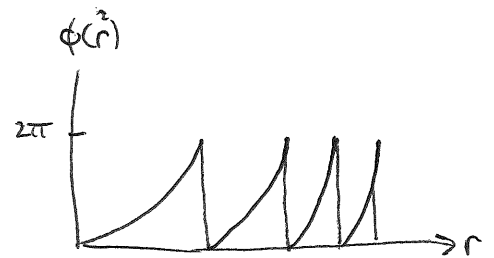
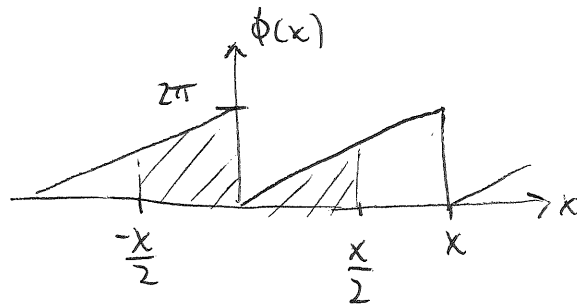
$$\sum_{m=-\infty}^{\infty} |a_m|^2 = 1 \quad 100\% \text{ passes through}$$

$\eta_1 = 0.405$ 40.5% of light goes to primary focal point, a 4x increase from Fresnel zone plate.

Can we do even better?

Kinoform

$$f(x) = \exp[i\phi(x)]$$



Let's make our lives a little easier and integrate from 0 to X instead.

$$a_m = \frac{1}{X} \int_0^X \exp(i2\pi \xi_0 x) \exp(-i2\pi m \xi_0 x) dx$$

$$a_m = \frac{1}{X} \frac{\exp(-i2\pi(m-1)\xi_0 X)}{-i2\pi(m-1)\xi_0} \Big|_0^X$$

$$a_m = \frac{1}{-i2\pi(m-1)} \left[\exp(-i2\pi(m-1)) - 1 \right]$$

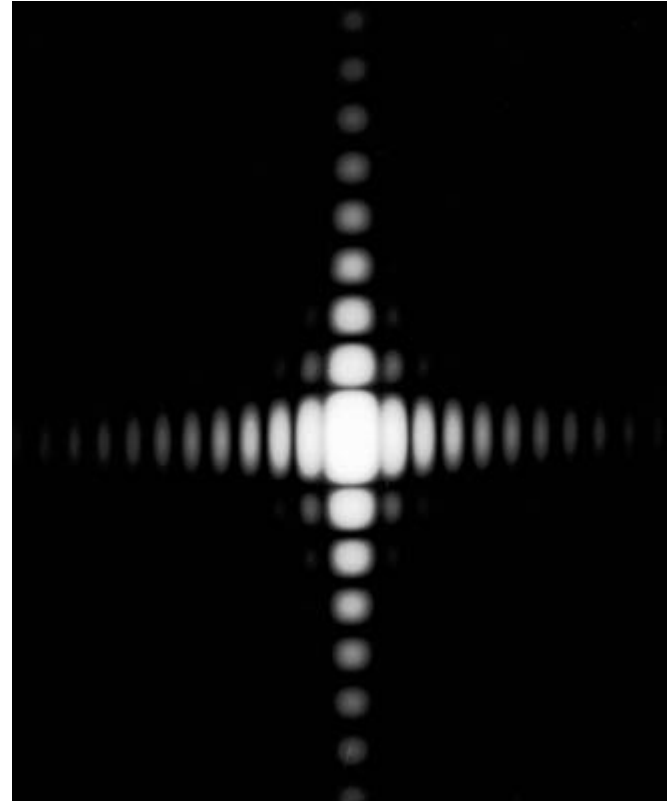
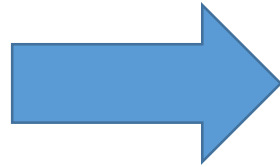
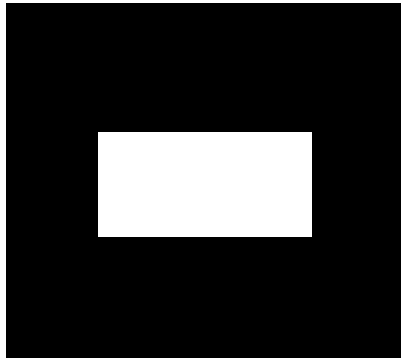
$$a_m = \exp[-i\pi(m-1)] \operatorname{sinc}(m-1)$$

The diffraction efficiency is now

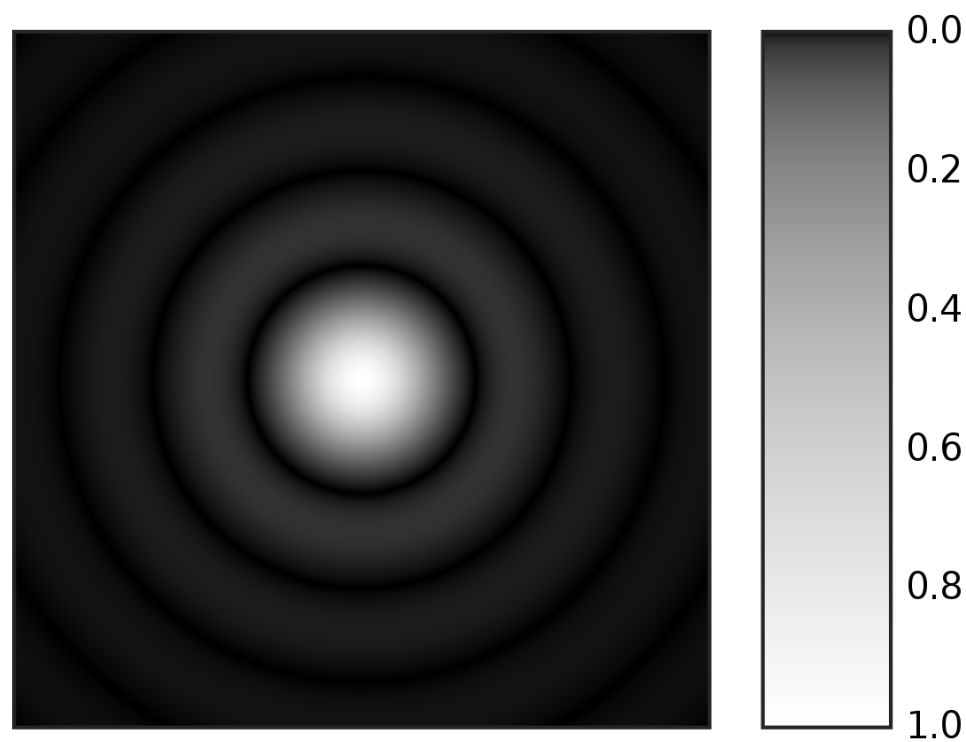
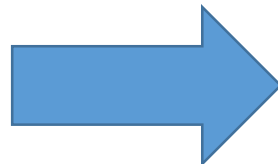
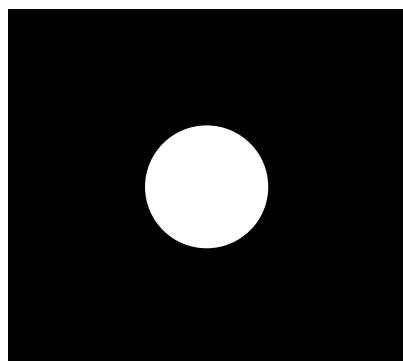
$$\eta_m = |a_m|^2 = \operatorname{sinc}^2(m-1) = \begin{cases} 1 & \text{for } m=1 \\ 0 & \text{otherwise} \end{cases}$$

All of the light goes into primary focal point!

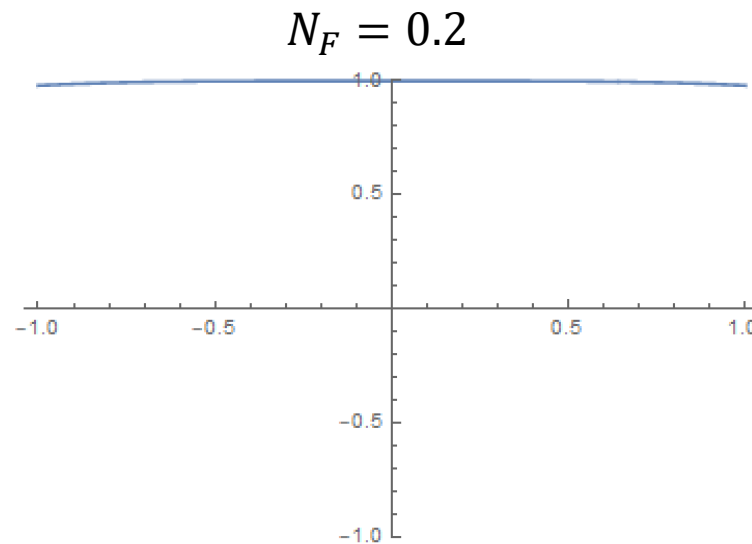
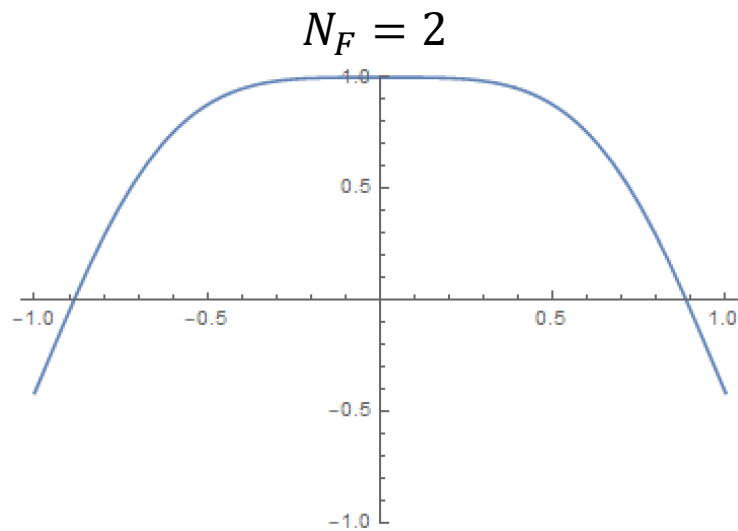
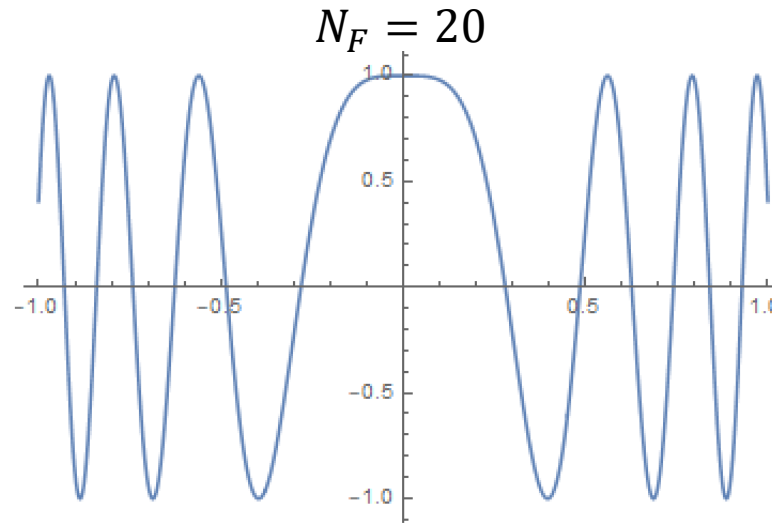
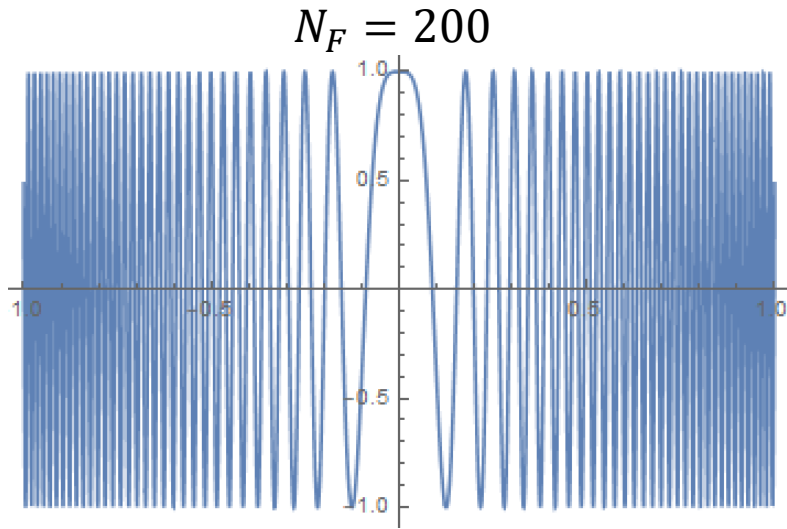
Fraunhofer Diffraction



Fraunhofer Diffraction

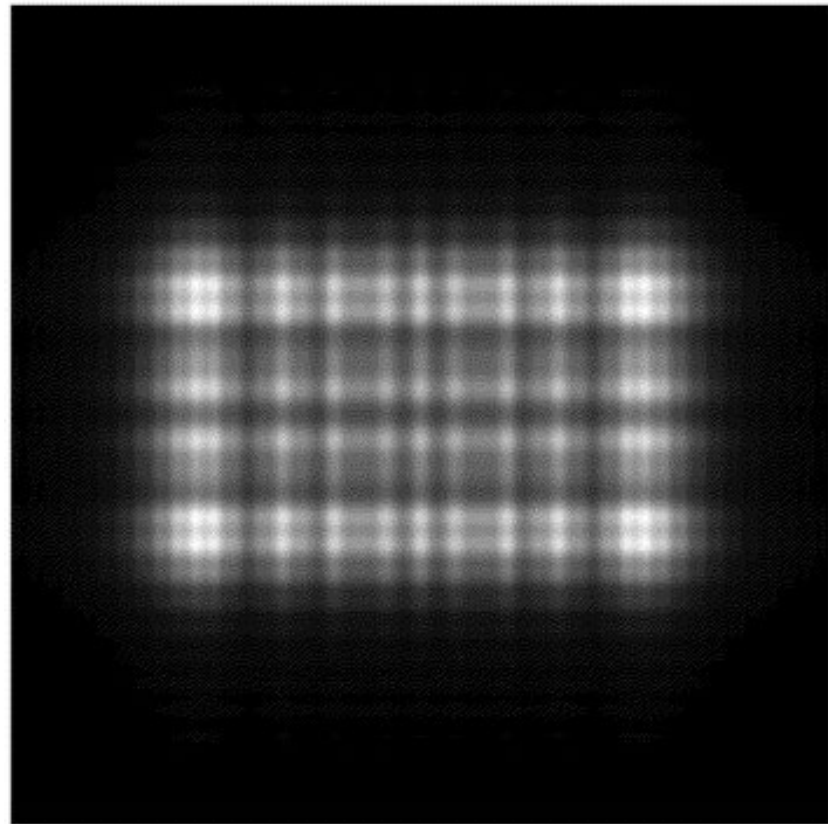
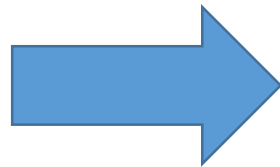
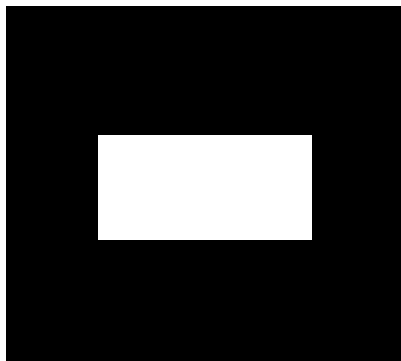


Quadratic Phase Factor

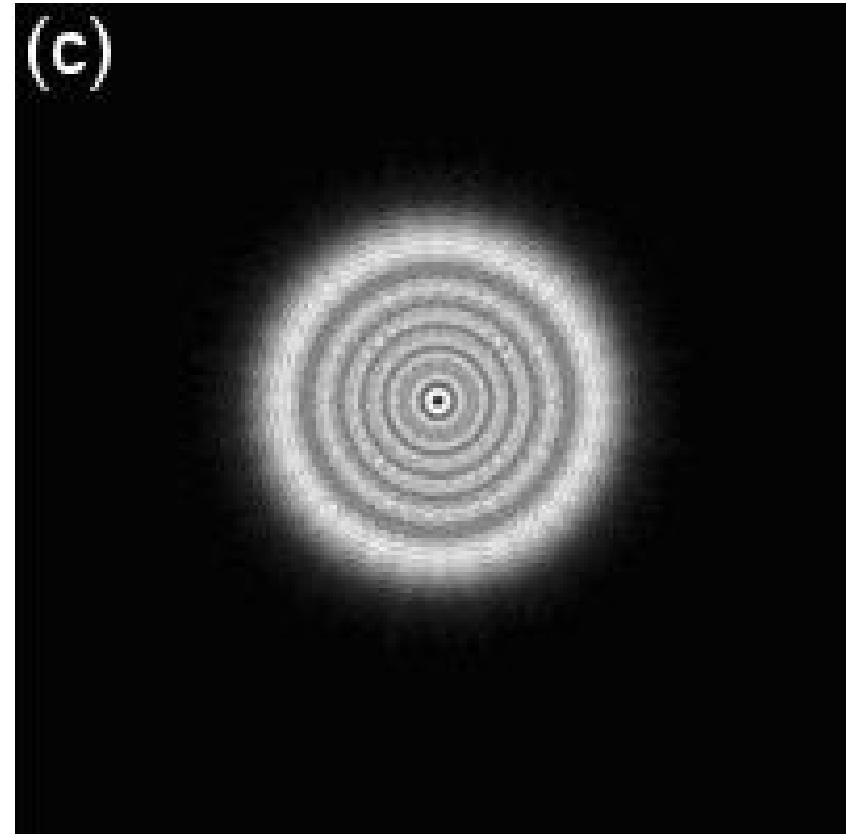
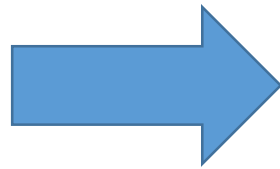
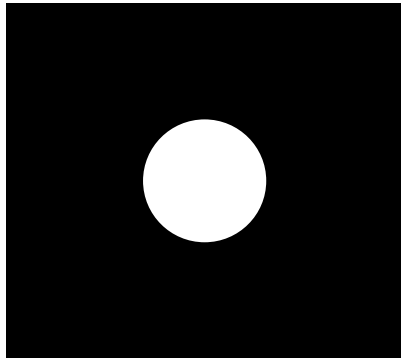


In general, moving into the Fresnel region means we need to calculate the fields numerically. In this case, you need to be wary of the sampling of this quadratic phase exponential to ensure accurate calculations.

Fresnel Diffraction



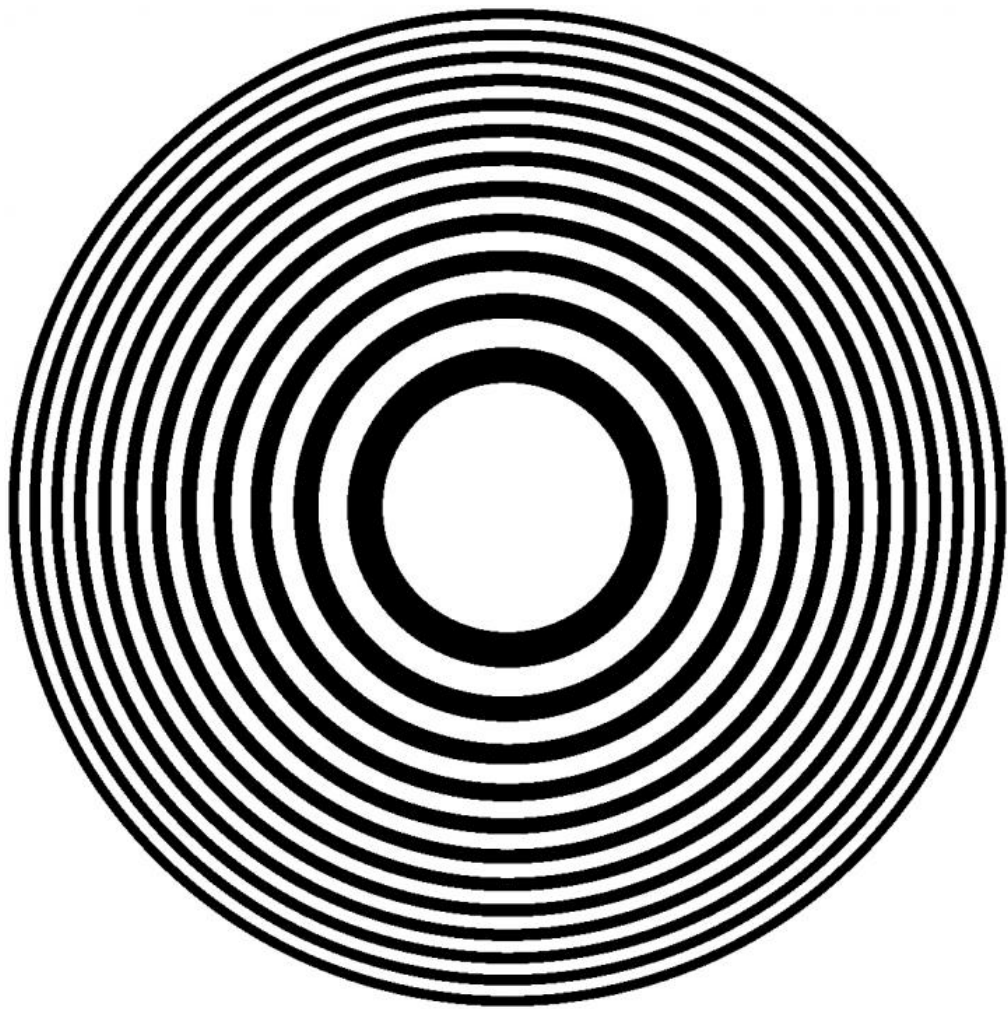
Fresnel Diffraction



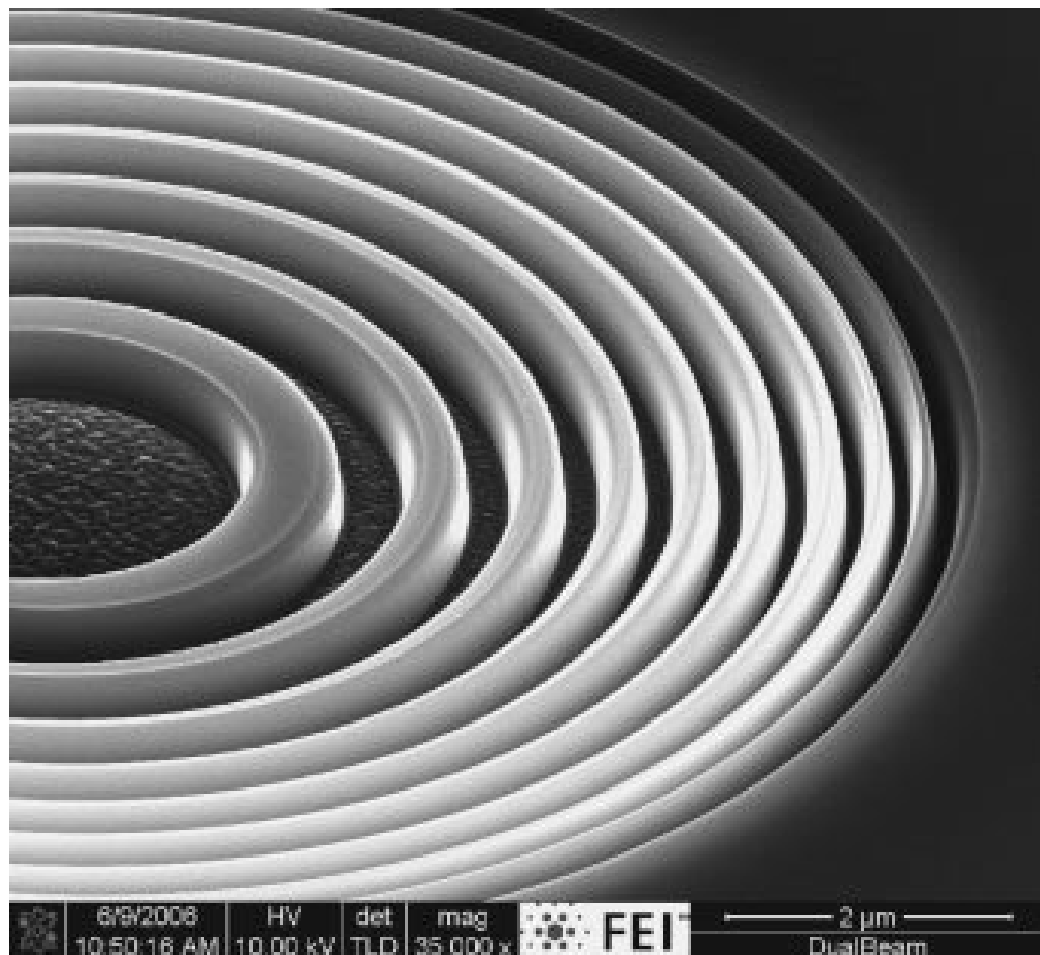
Fresnel Diffraction



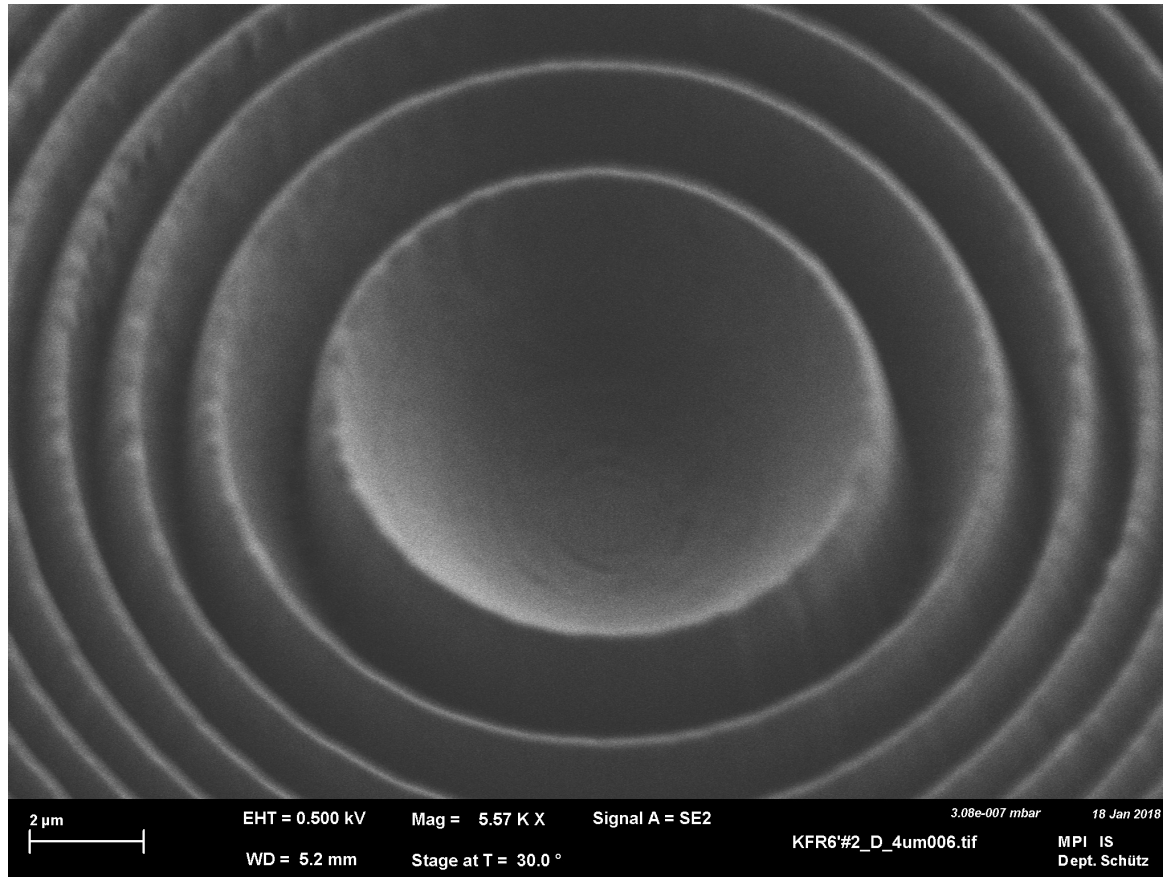
Fresnel Zone Plate



Phase Reversal Zone Plate

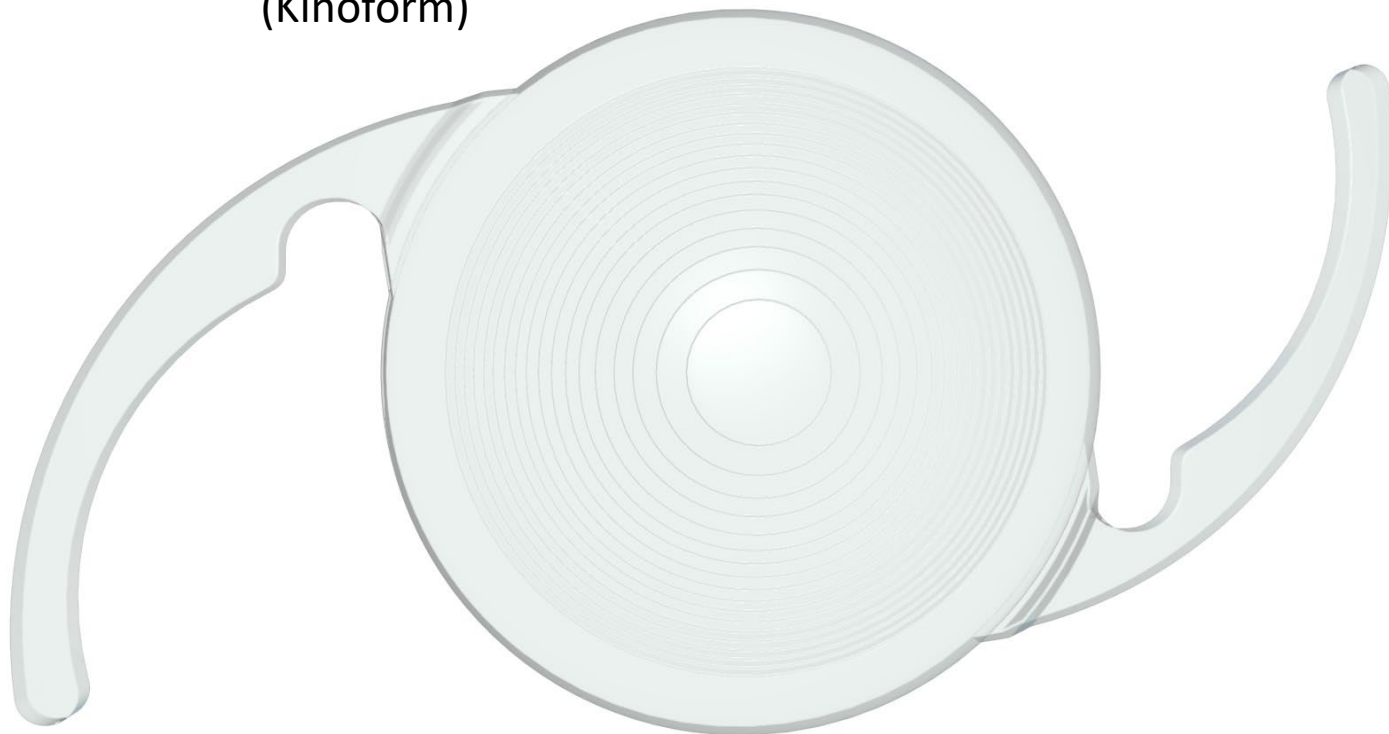


Kinoform Diffractive lens



These are not the same

Diffractive Lens
(Kinoform)



Fresnel Lens (Refractive)

