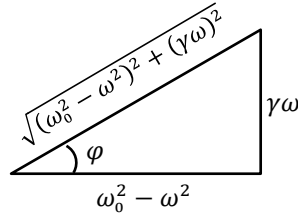


Problem 1) Substituting the suggested solution for $\mathbf{P}(t)$ in the governing differential equation, we arrive at

$$-\omega^2 \mathbf{P}'_0 \cos(\omega t + \varphi'_0) - \omega^2 \mathbf{P}''_0 \sin(\omega t + \varphi''_0) - \gamma \omega \mathbf{P}'_0 \sin(\omega t + \varphi'_0) + \gamma \omega \mathbf{P}''_0 \cos(\omega t + \varphi''_0) \\ + \omega_0^2 \mathbf{P}'_0 \cos(\omega t + \varphi'_0) + \omega_0^2 \mathbf{P}''_0 \sin(\omega t + \varphi''_0) = \varepsilon_0 \omega_p^2 \mathbf{E}'_0 \cos(\omega t) + \varepsilon_0 \omega_p^2 \mathbf{E}''_0 \sin(\omega t).$$

The above equation may now be split into two, one for \mathbf{P}'_0 and φ'_0 , the other for \mathbf{P}''_0 and φ''_0 , as follows:

$$[(\omega_0^2 - \omega^2) \cos(\omega t + \varphi'_0) - \gamma \omega \sin(\omega t + \varphi'_0)] \mathbf{P}'_0 = \varepsilon_0 \omega_p^2 \mathbf{E}'_0 \cos(\omega t), \\ [(\omega_0^2 - \omega^2) \sin(\omega t + \varphi''_0) + \gamma \omega \cos(\omega t + \varphi''_0)] \mathbf{P}''_0 = \varepsilon_0 \omega_p^2 \mathbf{E}''_0 \sin(\omega t).$$



$0 \leq \omega \leq \omega_0 \rightarrow 0 \leq \varphi \leq 90^\circ,$
$\omega > \omega_0 \rightarrow 90^\circ < \varphi < 180^\circ.$

In the right triangle depicted above, the length of the hypotenuse is $\sqrt{(\omega_0^2 - \omega^2)^2 + (\gamma\omega)^2}$ and the angle φ is $\arctan[\gamma\omega/(\omega_0^2 - \omega^2)]$. The above equations may thus be written as

$$\sqrt{(\omega_0^2 - \omega^2)^2 + (\gamma\omega)^2} [\cos(\varphi) \cos(\omega t + \varphi'_0) - \sin(\varphi) \sin(\omega t + \varphi'_0)] \mathbf{P}'_0 = \varepsilon_0 \omega_p^2 \mathbf{E}'_0 \cos(\omega t), \\ \sqrt{(\omega_0^2 - \omega^2)^2 + (\gamma\omega)^2} [\cos(\varphi) \sin(\omega t + \varphi''_0) + \sin(\varphi) \cos(\omega t + \varphi''_0)] \mathbf{P}''_0 = \varepsilon_0 \omega_p^2 \mathbf{E}''_0 \sin(\omega t).$$

The equations are further simplified with the aid of standard trigonometric identities, as follows:

$$\sqrt{(\omega_0^2 - \omega^2)^2 + (\gamma\omega)^2} \cos(\omega t + \varphi'_0 + \varphi) \mathbf{P}'_0 = \varepsilon_0 \omega_p^2 \mathbf{E}'_0 \cos(\omega t), \\ \sqrt{(\omega_0^2 - \omega^2)^2 + (\gamma\omega)^2} \sin(\omega t + \varphi''_0 + \varphi) \mathbf{P}''_0 = \varepsilon_0 \omega_p^2 \mathbf{E}''_0 \sin(\omega t).$$

It is thus seen that $\varphi'_0 = \varphi''_0 = -\varphi$ and that, therefore,

$$\mathbf{P}(t) = \frac{\varepsilon_0 \omega_p^2}{[(\omega_0^2 - \omega^2)^2 + (\gamma\omega)^2]^{1/2}} [\mathbf{E}'_0 \cos(\omega t - \varphi) + \mathbf{E}''_0 \sin(\omega t - \varphi)].$$

The above solution is in agreement with that obtained in the textbook using complex notation, as shown below.

$$\mathbf{P}(t) = \text{Re} \left[\frac{\varepsilon_0 \omega_p^2}{\omega_0^2 - \omega^2 - i\gamma\omega} \mathbf{E}_0 e^{-i\omega t} \right] = \text{Re} \left\{ \frac{\varepsilon_0 \omega_p^2}{[(\omega_0^2 - \omega^2)^2 + (\gamma\omega)^2]^{1/2} e^{-i\varphi}} (\mathbf{E}'_0 + i\mathbf{E}''_0) e^{-i\omega t} \right\} \\ \quad \quad \quad \uparrow \\ \quad \quad \quad \boxed{\varphi = \arctan[\gamma\omega/(\omega_0^2 - \omega^2)]} \\ = \frac{\varepsilon_0 \omega_p^2}{[(\omega_0^2 - \omega^2)^2 + (\gamma\omega)^2]^{1/2}} \text{Re}\{(\mathbf{E}'_0 + i\mathbf{E}''_0)[\cos(\omega t - \varphi) - i\sin(\omega t - \varphi)]\} \\ = \frac{\varepsilon_0 \omega_p^2}{[(\omega_0^2 - \omega^2)^2 + (\gamma\omega)^2]^{1/2}} [\mathbf{E}'_0 \cos(\omega t - \varphi) + \mathbf{E}''_0 \sin(\omega t - \varphi)].$$

Problem 2) a) At normal incidence, we have $\theta = 0$ and, therefore, $k_x = (\omega/c)n_a \sin \theta = 0$. We will have

$$\begin{aligned} \rho_p &= \frac{\varepsilon_a \sqrt{\mu_b \varepsilon_b} - \varepsilon_b \sqrt{\mu_a \varepsilon_a}}{\varepsilon_a \sqrt{\mu_b \varepsilon_b} + \varepsilon_b \sqrt{\mu_a \varepsilon_a}} \xrightarrow{\text{divide numerator and denominator by } \sqrt{\mu_a \varepsilon_a \mu_b \varepsilon_b}} \frac{\sqrt{\varepsilon_a/\mu_a} - \sqrt{\varepsilon_b/\mu_b}}{\sqrt{\varepsilon_a/\mu_a} + \sqrt{\varepsilon_b/\mu_b}}, \\ \rho_s &= \frac{\mu_b \sqrt{\mu_a \varepsilon_a} - \mu_a \sqrt{\mu_b \varepsilon_b}}{\mu_b \sqrt{\mu_a \varepsilon_a} + \mu_a \sqrt{\mu_b \varepsilon_b}} \xrightarrow{\text{divide numerator and denominator by } \mu_a \mu_b} \frac{\sqrt{\varepsilon_a/\mu_a} - \sqrt{\varepsilon_b/\mu_b}}{\sqrt{\varepsilon_a/\mu_a} + \sqrt{\varepsilon_b/\mu_b}}. \end{aligned}$$

It is seen that $\rho_p = \rho_s$ at $\theta = 0$. (Alternatively, you may start by setting $k_x = 0$, then write $\rho_p = A/B$ and $\rho_s = C/D$, then proceed to verify that $AD = BC$.)

b) At grazing incidence, where $\theta = 90^\circ$, we have $k_x = (\omega/c)n_a \sin \theta = (\omega/c)n_a$. Consequently,

$$\begin{aligned} \rho_p &= \frac{E_{x0}^{(r)}}{E_{x0}^{(i)}} = \frac{\varepsilon_a \sqrt{\mu_b \varepsilon_b} - \mu_a \varepsilon_a}{\varepsilon_a \sqrt{\mu_b \varepsilon_b} - \mu_a \varepsilon_a} = 1, \\ \rho_s &= \frac{E_{y0}^{(r)}}{E_{y0}^{(i)}} = -\frac{\mu_a \sqrt{\mu_b \varepsilon_b} - \mu_a \varepsilon_a}{\mu_a \sqrt{\mu_b \varepsilon_b} - \mu_a \varepsilon_a} = -1. \end{aligned}$$

In the case of s -polarization, we find $\tau_s = 1 + \rho_s = 0$, which indicates the vanishing of the transmitted beam, as expected. In the immediate vicinity of the interfacial xy -plane at $z = 0^+$, the reflected beam propagates parallel to the incident beam, albeit with its y -oriented E -field flipped to the $-y$ direction. Similarly, the reflected beam's H -field has flipped from $+z$ to $-z$ orientation. Thus, there are no electric and magnetic fields parallel to the interface, nor any such fields perpendicular to the interfacial plane.

In the case of p -polarization, the Fresnel reflection coefficient represents the E -field's amplitude along the x -axis. However, at grazing incidence, E_x is essentially zero, for both the incident and reflected beams. The equality of the incident and reflected E_x (i.e., the fact that ρ_p approaches 1.0 as $\theta \rightarrow 90^\circ$) thus indicates the equality of the incident and reflected E_z , albeit with a sign change, as can be inferred from the provided figure in the statement of the problem. In other words, it is the reflection coefficient for E_z that approaches -1 as $\theta \rightarrow 90^\circ$. The H -field (always aligned with the y -axis for p -light) similarly flips upon reflection. All in all, the total E_z and the total H_y immediately above the xy -plane at $z = 0^+$ vanish. Consequently, the \mathbf{E} and \mathbf{H} fields of the transmitted plane-wave immediately below the interface at $z = 0^-$ approach zero as $\theta \rightarrow 90^\circ$.

$$\begin{aligned} \text{c) } \rho_p = 0 &\rightarrow \varepsilon_a \sqrt{\mu_b \varepsilon_b - (ck_x/\omega)^2} = \varepsilon_b \sqrt{\mu_a \varepsilon_a - (ck_x/\omega)^2} \\ &\rightarrow \varepsilon_a^2 [\mu_b \varepsilon_b - (n_a \sin \theta)^2] = \varepsilon_b^2 [\mu_a \varepsilon_a - (n_a \sin \theta)^2] \\ &\rightarrow \varepsilon_a^2 \mu_b \varepsilon_b - \varepsilon_a^2 \mu_a \varepsilon_a \sin^2 \theta = \varepsilon_b^2 \mu_a \varepsilon_a - \varepsilon_b^2 \mu_a \varepsilon_a \sin^2 \theta \\ &\rightarrow \sin^2 \theta = \frac{(\varepsilon_a \mu_b - \varepsilon_b \mu_a) \varepsilon_b}{\mu_a (\varepsilon_a^2 - \varepsilon_b^2)} \\ &\rightarrow \cos^2 \theta = 1 - \sin^2 \theta = \frac{(\mu_a \varepsilon_a - \mu_b \varepsilon_b) \varepsilon_a}{\mu_a (\varepsilon_a^2 - \varepsilon_b^2)} \\ &\rightarrow \tan^2 \theta = \frac{(\mu_b \varepsilon_a - \mu_a \varepsilon_b) \varepsilon_b}{(\mu_a \varepsilon_a - \mu_b \varepsilon_b) \varepsilon_a}. \end{aligned}$$

If $\mu_b = \mu_a$, we will have $\tan^2 \theta = \mu_b \varepsilon_b / \mu_a \varepsilon_a = (n_b/n_a)^2$. Now, if ε_b happens to be real and positive, there will exist a solution for θ . The Brewster angle will then be $\theta_B = \tan^{-1}(n_b/n_a)$.

Digression. To explore the situations in which a Brewster's angle might exist for s-polarized light, we set ρ_s to zero, then examine the conditions under which a solution for θ might exist.

$$\begin{aligned} \rho_s = 0 & \rightarrow \mu_b \sqrt{\mu_a \varepsilon_a - (ck_x/\omega)^2} = \mu_a \sqrt{\mu_b \varepsilon_b - (ck_x/\omega)^2} \\ & \rightarrow \mu_b^2 \mu_a \varepsilon_a (1 - \sin^2 \theta) = \mu_a^2 (\mu_b \varepsilon_b - \mu_a \varepsilon_a \sin^2 \theta) \\ & \rightarrow (\mu_b \varepsilon_a - \mu_a \varepsilon_b) \mu_b = \varepsilon_a (\mu_b^2 - \mu_a^2) \sin^2 \theta \rightarrow \sin^2 \theta = \frac{(\mu_b \varepsilon_a - \mu_a \varepsilon_b) \mu_b}{(\mu_b^2 - \mu_a^2) \varepsilon_a}. \end{aligned}$$

Clearly, it is possible to have a real-valued angle θ that satisfies the above equation — hence the feasibility of a Brewster's angle for s-light — but *not* if $\mu_b = \mu_a$. In other words, $\mu_b \neq \mu_a$ is a necessary condition for the existence of such an angle, provided that the values of $\mu_a, \varepsilon_a, \mu_b, \varepsilon_b$ are such that the above expression for $\sin^2 \theta$ turns out to yield a real number in the (0,1) interval.

d) Setting $ck_x/\omega = n_a \sin \theta$, we note that $\sqrt{n_b^2 - (n_a \sin \theta)^2}$ becomes imaginary when $n_a \sin \theta$ exceeds n_b . The critical angle beyond which this change occurs is $\theta_c = \arcsin(n_b/n_a)$. Thus, upon substituting $n_a^2 \sin^2(\theta_c)$ for n_b^2 , and also setting $\mu_b = \mu_a$, the simplified Fresnel reflection coefficients become

$$\begin{aligned} \rho_p &= \frac{\varepsilon_a (n_a^2 \sin^2 \theta_c - n_a^2 \sin^2 \theta)^{1/2} - \varepsilon_b (n_a^2 - n_a^2 \sin^2 \theta)^{1/2}}{\varepsilon_a (n_a^2 \sin^2 \theta_c - n_a^2 \sin^2 \theta)^{1/2} + \varepsilon_b (n_a^2 - n_a^2 \sin^2 \theta)^{1/2}} = \frac{\sqrt{\sin^2 \theta_c - \sin^2 \theta} - (\varepsilon_b/\varepsilon_a) \cos \theta}{\sqrt{\sin^2 \theta_c - \sin^2 \theta} + (\varepsilon_b/\varepsilon_a) \cos \theta}, \\ \rho_s &= \frac{(n_a^2 - n_a^2 \sin^2 \theta)^{1/2} - (n_a^2 \sin^2 \theta_c - n_a^2 \sin^2 \theta)^{1/2}}{(n_a^2 - n_a^2 \sin^2 \theta)^{1/2} + (n_a^2 \sin^2 \theta_c - n_a^2 \sin^2 \theta)^{1/2}} = \frac{\cos \theta - \sqrt{\sin^2 \theta_c - \sin^2 \theta}}{\cos \theta + \sqrt{\sin^2 \theta_c - \sin^2 \theta}}. \end{aligned}$$

At incidence angles $\theta > \theta_c$, the term under the square root in the above expressions of ρ_p and ρ_s becomes negative, in which case we can write

$$\rho_p = \frac{i\sqrt{\sin^2 \theta - \sin^2 \theta_c} - \sin^2 \theta_c \cos \theta}{i\sqrt{\sin^2 \theta - \sin^2 \theta_c} + \sin^2 \theta_c \cos \theta} = -\frac{\sin^2 \theta_c \cos \theta - i\sqrt{\sin^2 \theta - \sin^2 \theta_c}}{\sin^2 \theta_c \cos \theta + i\sqrt{\sin^2 \theta - \sin^2 \theta_c}} = -\exp \left[-2i \tan^{-1} \left(\frac{\sqrt{\sin^2 \theta - \sin^2 \theta_c}}{(\sin^2 \theta_c) \cos \theta} \right) \right].$$

It is seen that $|\rho_p| = 1$ and $\varphi_p = \pi - 2 \tan^{-1} \left(\frac{\sqrt{\sin^2 \theta - \sin^2 \theta_c}}{(\sin^2 \theta_c) \cos \theta} \right)$ for all angles $\theta \geq \theta_c$. Similarly, in the case of s-polarized (or TE) incident light, we have

$$\rho_s = \frac{\cos \theta - i\sqrt{\sin^2 \theta - \sin^2 \theta_c}}{\cos \theta + i\sqrt{\sin^2 \theta - \sin^2 \theta_c}} = \exp \left[-2i \tan^{-1} \left(\frac{\sqrt{\sin^2 \theta - \sin^2 \theta_c}}{\cos \theta} \right) \right].$$

In this case, $|\rho_s| = 1$ and $\varphi_s = -2 \tan^{-1} \left(\frac{\sqrt{\sin^2 \theta - \sin^2 \theta_c}}{\cos \theta} \right)$ for all angles $\theta \geq \theta_c$.

Problem 3 a) Considering that $\mathbf{k}^{\uparrow\downarrow} = (\omega/c)n_a(\omega)(\sin \theta \hat{\mathbf{x}} \pm \cos \theta \hat{\mathbf{z}})$, the sequence starting with the incident E -field at the lower facet (i.e., at $z = 0$), followed by total internal reflection (TIR) at the lower facet, propagation to the upper facet (at $z = d$), TIR at the upper facet, and, finally, a downward propagation to the lower facet is listed below for p -polarized light.

$$\text{i) } E_x^{\downarrow}(x, y, z = 0, t) = E_{0x} e^{i(k_x x + k_z^{\downarrow} z - \omega t)} \Big|_{z=0} = E_{0x} e^{i(k_x x - \omega t)}, \quad (1)$$

$$\text{ii) } E_x^{\uparrow}(x, y, z = 0, t) = \rho_p E_{0x} e^{i(k_x x - \omega t)}, \quad (2)$$

$$\text{iii)} \quad E_x^\uparrow(x, y, z = d, t) = \rho_p E_{0x} e^{i(k_x x + k_z^\uparrow z - \omega t)} \Big|_{z=d} = \rho_p E_{0x} e^{i(k_x x + k_z^\uparrow d - \omega t)}, \quad (3)$$

$$\text{iv)} \quad E_x^\downarrow(x, y, z = d, t) = \rho_p^2 E_{0x} e^{i(k_x x + k_z^\uparrow d - \omega t)}, \quad (4)$$

$$\text{v)} \quad E_x^\downarrow(x, y, z = 0, t) = \rho_p^2 E_{0x} e^{i(k_x x + k_z^\uparrow d - \omega t)} e^{ik_z^\downarrow(-d)} = \rho_p^2 E_{0x} e^{i(k_x x + 2k_z^\uparrow d - \omega t)}. \quad (5)$$

Self-consistency demands that the E -field after one roundtrip coincide with the E -field at the starting point — aside from an integer-multiple of 2π phase-shift. Equating the E -field in step (v) with that in step (i) and accounting for the possible $2\pi m$ phase-shift, we find

$$\begin{aligned} \rho_p^2 E_{0x} e^{i(k_x x + 2k_z^\uparrow d - \omega t)} &= E_{0x} e^{i(k_x x - \omega t)} e^{i2\pi m} \quad \rightarrow \quad \rho_p^2 e^{i2k_z^\uparrow d} = e^{i2\pi m} \\ &\rightarrow \left(\frac{i\sqrt{\sin^2 \theta - \sin^2 \theta_c} - \sin^2 \theta_c \cos \theta}{i\sqrt{\sin^2 \theta - \sin^2 \theta_c} + \sin^2 \theta_c \cos \theta} \right)^2 e^{i2(\omega/c)n_a d \cos \theta} = e^{i2\pi m} \\ &\rightarrow 2\pi - 4 \arctan \left(\frac{\sqrt{\sin^2 \theta - \sin^2 \theta_c}}{\sin^2 \theta_c \cos \theta} \right) + 2(\omega/c)n_a d \cos \theta = 2m\pi \\ &\rightarrow \arctan \left(\frac{\sqrt{\sin^2 \theta - \sin^2 \theta_c}}{\sin^2 \theta_c \cos \theta} \right) = \frac{1}{2}(\omega/c)n_a d \cos \theta - \frac{1}{2}(m-1)\pi. \end{aligned} \quad (6)$$

Depending on whether m (an integer) is odd or even, Eq.(6) can be further streamlined to yield

$$m \text{ odd:} \quad \frac{\sqrt{\sin^2 \theta - \sin^2 \theta_c}}{\sin^2 \theta_c \cos \theta} = \tan[\frac{1}{2}(\omega/c)n_a d \cos \theta], \quad (7)$$

$$m \text{ even:} \quad \frac{\sqrt{\sin^2 \theta - \sin^2 \theta_c}}{\sin^2 \theta_c \cos \theta} = -\cot[\frac{1}{2}(\omega/c)n_a d \cos \theta]. \quad (8)$$

As for s -polarized light, a similar procedure yields the acceptable values of θ as follows:

$$\arctan \left(\frac{\sqrt{\sin^2 \theta - \sin^2 \theta_c}}{\cos \theta} \right) = \frac{1}{2}(\omega/c)n_a d \cos \theta - \frac{1}{2}m\pi. \quad (9)$$

Once again, depending on whether m is odd or even, we find

$$m \text{ even:} \quad \frac{\sqrt{\sin^2 \theta - \sin^2 \theta_c}}{\cos \theta} = \tan[\frac{1}{2}(\omega/c)n_a d \cos \theta], \quad (10)$$

$$m \text{ odd:} \quad \frac{\sqrt{\sin^2 \theta - \sin^2 \theta_c}}{\cos \theta} = -\cot[\frac{1}{2}(\omega/c)n_a d \cos \theta], \quad (11)$$

Equation (7), (8), (10), and (11) can be solved graphically by plotting the left- and right-hand sides of each equation versus θ (over the interval $\theta_c < \theta < 90^\circ$), then identifying the crossing points of each pair of graphs.

b) The acceptable values of θ are not necessarily the same for p -light and s -light. This is because $\sin^2(\theta_c)$ appears in the denominator on the left-hand sides of Eqs.(7) and (8), but is absent from Eqs.(10) and (11). This indicates that the characteristics of the p -polarized (or TM) modes of a slab waveguide generally differ from those of the s -polarized (or TE) modes, as the modes associated with different polarizations will have different allowed values of θ for any given set of values of ω , $n_a(\omega)$, and d . Also, for each polarization, the odd and even modes will have different k_x values and different E -field profiles (as well as H -field profiles) along the z -axis.
