

Problem 1) a) The two E -fields are linearly polarized along the y -axis and co-propagate along the x -axis. Noting that $E_{y1} = E_s + E_d$ and $E_{y2} = E_s - E_d$, we write

$$\begin{aligned} \mathbf{E}(\mathbf{r}, t) &= E_{y1} \cos[(n_1\omega_1/c)x - \omega_1 t + \varphi_1] \hat{\mathbf{y}} + E_{y2} \cos[(n_2\omega_2/c)x - \omega_2 t + \varphi_2] \hat{\mathbf{y}} \\ &= \{(E_s + E_d) \cos[(n_1\omega_1/c)x - \omega_1 t + \varphi_1] + (E_s - E_d) \cos[(n_2\omega_2/c)x - \omega_2 t + \varphi_2]\} \hat{\mathbf{y}}. \end{aligned}$$

b) Using the trigonometric identities, we combine the two fields with amplitudes E_s , and also the two fields with amplitudes E_d , to arrive at

$$\begin{aligned} \mathbf{E}(\mathbf{r}, t) &= 2E_s \cos[\tfrac{1}{2}(\omega_1 n_1 + \omega_2 n_2)(x/c) - \tfrac{1}{2}(\omega_1 + \omega_2)t + \tfrac{1}{2}(\varphi_1 + \varphi_2)] \\ &\quad \times \cos[\tfrac{1}{2}(\omega_1 n_1 - \omega_2 n_2)(x/c) - \tfrac{1}{2}(\omega_1 - \omega_2)t + \tfrac{1}{2}(\varphi_1 - \varphi_2)] \hat{\mathbf{y}} \\ &\quad - 2E_d \sin[\tfrac{1}{2}(\omega_1 n_1 + \omega_2 n_2)(x/c) - \tfrac{1}{2}(\omega_1 + \omega_2)t + \tfrac{1}{2}(\varphi_1 + \varphi_2)] \\ &\quad \times \sin[\tfrac{1}{2}(\omega_1 n_1 - \omega_2 n_2)(x/c) - \tfrac{1}{2}(\omega_1 - \omega_2)t + \tfrac{1}{2}(\varphi_1 - \varphi_2)] \hat{\mathbf{y}} \\ &\cong (E_{y1} + E_{y2}) \cos[(\omega_c n_c/c)x - \omega_c t + \tfrac{1}{2}(\varphi_1 + \varphi_2)] \\ &\quad \times \cos[-\tfrac{1}{2}n_g(\omega_c)(\Delta\omega)(x/c) + \tfrac{1}{2}(\Delta\omega)t + \tfrac{1}{2}(\varphi_1 - \varphi_2)] \hat{\mathbf{y}} \\ &\quad - (E_{y1} - E_{y2}) \sin[(\omega_c n_c/c)x - \omega_c t + \tfrac{1}{2}(\varphi_1 + \varphi_2)] \\ &\quad \times \sin[-\tfrac{1}{2}n_g(\omega_c)(\Delta\omega)(x/c) + \tfrac{1}{2}(\Delta\omega)t + \tfrac{1}{2}(\varphi_1 - \varphi_2)] \hat{\mathbf{y}}. \end{aligned}$$

c) The pair of beat signals may be further streamlined, as follows:

$$\begin{aligned} \mathbf{E}(\mathbf{r}, t) &= (E_{y1} + E_{y2}) \cos\{(\omega_c n_c/c)[x - (c/n_c)t] + \tfrac{1}{2}(\varphi_1 + \varphi_2)\} \leftarrow \begin{array}{l} \text{carrier 1: frequency} = \omega_c, \\ \text{phase velocity} = c/n(\omega_c). \end{array} \\ &\quad \times \cos\{\tfrac{1}{2}n_g(\omega_c)(\Delta\omega/c)[x - (c/n_g)t] - \tfrac{1}{2}(\varphi_1 - \varphi_2)\} \hat{\mathbf{y}} \leftarrow \begin{array}{l} \text{envelope 1: frequency} = \tfrac{1}{2}\Delta\omega, \\ \text{group velocity} = c/n_g(\omega_c), \\ \text{amplitude} = E_{y1} + E_{y2}. \end{array} \\ &\quad + (E_{y1} - E_{y2}) \sin\{(\omega_c n_c/c)[x - (c/n_c)t] + \tfrac{1}{2}(\varphi_1 + \varphi_2)\} \leftarrow \begin{array}{l} \text{carrier 2: frequency} = \omega_c, \\ \text{phase velocity} = c/n(\omega_c). \end{array} \\ &\quad \times \sin\{\tfrac{1}{2}n_g(\omega_c)(\Delta\omega/c)[x - (c/n_g)t] - \tfrac{1}{2}(\varphi_1 - \varphi_2)\} \hat{\mathbf{y}}. \leftarrow \begin{array}{l} \text{envelope 2: frequency} = \tfrac{1}{2}\Delta\omega, \\ \text{group velocity} = c/n_g(\omega_c), \\ \text{amplitude} = E_{y1} - E_{y2}. \end{array} \end{aligned}$$

Note that the peak envelope of the first beat signal coincides with the zero of the envelope of the second beat signal and vice-versa. Also, in the special case where $E_{y1} = E_{y2}$, the second beat signal disappears.

Problem 2) a) At normal incidence, $k_x^{(i)} = k_y^{(i)} = 0$. Application of the generalized Snell's law now yields $\omega^{(r)} = \omega^{(t)} = \omega^{(i)}$ and $k_x^{(r)} = k_x^{(t)} = 0$, as well as $k_y^{(r)} = k_y^{(t)} = 0$. From the dispersion relation, $\mathbf{k} \cdot \mathbf{k} = (\omega/c)^2 \mu(\omega) \varepsilon(\omega)$, we find

$$k_z = \pm [(\omega/c)^2 \mu(\omega) \varepsilon(\omega) - k_x^2 - k_y^2]^{1/2} = \pm (\omega/c) \sqrt{\mu(\omega) \varepsilon(\omega)}, \quad (1)$$

where the plus or minus signs for $k_z^{(i)}$, $k_z^{(r)}$, and $k_z^{(t)}$ must be chosen judiciously. We will have

$$k_z^{(i)} = -(\omega/c) \sqrt{\mu_a(\omega) \varepsilon_a(\omega)} = -n_a \omega/c, \quad (2)$$

$$k_z^{(r)} = (\omega/c)\sqrt{\mu_a(\omega)\varepsilon_a(\omega)} = n_a\omega/c, \quad \text{understanding that } n_b'' > 0 \quad (3)$$

$$k_z^{(t)} = -(\omega/c)\sqrt{\mu_b(\omega)\varepsilon_b(\omega)} = -(n_b' + in_b'')\omega/c. \quad (4)$$

b) $\nabla \cdot \mathbf{D}(\mathbf{r}, t) = \rho_{\text{free}}(\mathbf{r}, t) = 0 \rightarrow \mathbf{i}\mathbf{k} \cdot \varepsilon_0 \varepsilon(\omega) \mathbf{E}_0 e^{i(\mathbf{k} \cdot \mathbf{r} - \omega t)} = 0 \rightarrow \mathbf{k} \cdot \mathbf{E}_0 = 0$
 $\rightarrow \cancel{k_x} E_{0x} + \cancel{k_y} E_{0y} + k_z E_{0z} = 0 \rightarrow E_{0z}^{(i)} = E_{0z}^{(r)} = E_{0z}^{(t)} = 0.$ (5)

c) $\nabla \times \mathbf{E}(\mathbf{r}, t) = -\partial \mathbf{B}(\mathbf{r}, t) / \partial t \rightarrow \mathbf{i}\mathbf{k} \times \mathbf{E}_0 e^{i(\mathbf{k} \cdot \mathbf{r} - \omega t)} = i\omega \mu_0 \mu(\omega) \mathbf{H}_0 e^{i(\mathbf{k} \cdot \mathbf{r} - \omega t)}$
 $\rightarrow (\cancel{k_x} \hat{\mathbf{x}} + \cancel{k_y} \hat{\mathbf{y}} + k_z \hat{\mathbf{z}}) \times (E_{0x} \hat{\mathbf{x}} + E_{0y} \hat{\mathbf{y}} + \cancel{E_{0z}} \hat{\mathbf{z}}) = \omega \mu_0 \mu(\omega) \mathbf{H}_0$
 $\rightarrow \mathbf{H}_0 = -(\omega \mu_0 \mu)^{-1} k_z (E_{0y} \hat{\mathbf{x}} - E_{0x} \hat{\mathbf{y}}).$ (6)

Recalling that $E_{0y}^{(i)} = 0$, we arrive at

$$n_a = \sqrt{\mu_a \varepsilon_a} c = (\mu_0 \varepsilon_0)^{-1/2}$$

$$\mathbf{H}_0^{(i)} = (\omega \mu_0 \mu_a)^{-1} k_z^{(i)} E_{0x}^{(i)} \hat{\mathbf{y}} = -(n_a/c \mu_0 \mu_a) E_{0x}^{(i)} \hat{\mathbf{y}} = -\sqrt{\frac{\varepsilon_0 \varepsilon_a}{\mu_0 \mu_a}} E_{0x}^{(i)} \hat{\mathbf{y}}. \quad (7)$$

$$\mathbf{H}_0^{(r)} = -(\omega \mu_0 \mu_a)^{-1} k_z^{(r)} (E_{0y}^{(r)} \hat{\mathbf{x}} - E_{0x}^{(r)} \hat{\mathbf{y}}) = -\sqrt{\frac{\varepsilon_0 \varepsilon_a}{\mu_0 \mu_a}} (E_{0y}^{(r)} \hat{\mathbf{x}} - E_{0x}^{(r)} \hat{\mathbf{y}}). \quad (8)$$

$$\mathbf{H}_0^{(t)} = -(\omega \mu_0 \mu_b)^{-1} k_z^{(t)} (E_{0y}^{(t)} \hat{\mathbf{x}} - E_{0x}^{(t)} \hat{\mathbf{y}}) = \sqrt{\frac{\varepsilon_0 \varepsilon_b}{\mu_0 \mu_b}} (E_{0y}^{(t)} \hat{\mathbf{x}} - E_{0x}^{(t)} \hat{\mathbf{y}}). \quad (9)$$

d) The continuity conditions for E_y and H_x fields at the interface (i.e., at $z = 0^\pm$) now become

$$\cancel{E_{0y}^{(i)}} + E_{0y}^{(r)} = E_{0y}^{(t)} \rightarrow E_{0y}^{(r)} = E_{0y}^{(t)}, \quad (10)$$

$$\cancel{H_{0x}^{(i)}} + H_{0x}^{(r)} = H_{0x}^{(t)} \rightarrow -\sqrt{\frac{\varepsilon_0 \varepsilon_a}{\mu_0 \mu_a}} E_{0y}^{(r)} = \sqrt{\frac{\varepsilon_0 \varepsilon_b}{\mu_0 \mu_b}} E_{0y}^{(t)}. \quad (11)$$

The only solution of Eqs.(10) and (11) is $E_{0y}^{(r)} = E_{0y}^{(t)} = 0$. The remaining boundary conditions (i.e., those pertaining to the continuity of E_x and H_y at $z = 0^\pm$) yield

$$E_{0x}^{(i)} + E_{0x}^{(r)} = E_{0x}^{(t)}, \quad (12)$$

$$H_{0y}^{(i)} + H_{0y}^{(r)} = H_{0y}^{(t)} \rightarrow -\sqrt{\frac{\varepsilon_0 \varepsilon_a}{\mu_0 \mu_a}} E_{0x}^{(i)} + \sqrt{\frac{\varepsilon_0 \varepsilon_a}{\mu_0 \mu_a}} E_{0x}^{(r)} = -\sqrt{\frac{\varepsilon_0 \varepsilon_b}{\mu_0 \mu_b}} E_{0x}^{(t)}$$

$$\rightarrow \sqrt{\varepsilon_a / \mu_a} (E_{0x}^{(i)} - E_{0x}^{(r)}) = \sqrt{\varepsilon_b / \mu_b} E_{0x}^{(t)}. \quad (13)$$

Substituting from Eq.(12) into Eq.(13), we arrive at

$$\sqrt{\varepsilon_a / \mu_a} (E_{0x}^{(i)} - E_{0x}^{(r)}) = \sqrt{\varepsilon_b / \mu_b} (E_{0x}^{(i)} + E_{0x}^{(r)}). \quad (14)$$

Solving the above equations, we find

$$\rho = E_{0x}^{(r)} / E_{0x}^{(i)} = \frac{\sqrt{\varepsilon_a / \mu_a} - \sqrt{\varepsilon_b / \mu_b}}{\sqrt{\varepsilon_a / \mu_a} + \sqrt{\varepsilon_b / \mu_b}}, \quad (15)$$

$$\tau = E_{0x}^{(t)} / E_{0x}^{(i)} = \frac{2\sqrt{\varepsilon_a / \mu_a}}{\sqrt{\varepsilon_a / \mu_a} + \sqrt{\varepsilon_b / \mu_b}}. \quad (16)$$

e) The reflected and transmitted plane-waves consist of the following \mathbf{E} and \mathbf{H} fields:

$$\mathbf{E}^{(r)}(\mathbf{r}, t) = \rho E_{0x}^{(i)} e^{i(k_z^{(r)} z - \omega t)} \hat{\mathbf{x}}, \quad (17)$$

$$\mathbf{E}^{(t)}(\mathbf{r}, t) = \tau E_{0x}^{(i)} e^{i(k_z^{(t)} z - \omega t)} \hat{\mathbf{x}}, \quad (18)$$

$$\mathbf{H}^{(r)}(\mathbf{r}, t) = H_{0y}^{(r)} e^{i(k_z^{(r)} z - \omega t)} \hat{\mathbf{y}} = \rho \sqrt{\varepsilon_0 \varepsilon_a / \mu_0 \mu_a} E_{0x}^{(i)} e^{i(k_z^{(r)} z - \omega t)} \hat{\mathbf{y}}, \quad \leftarrow \text{see Eq.(8)} \quad (19)$$

$$\mathbf{H}^{(t)}(\mathbf{r}, t) = H_{0y}^{(t)} e^{i(k_z^{(t)} z - \omega t)} \hat{\mathbf{y}} = (\omega \mu_0 \mu_b)^{-1} k_z^{(t)} E_{0x}^{(t)} e^{i(k_z^{(t)} z - \omega t)} \hat{\mathbf{y}}. \quad \leftarrow \text{see Eq.(6)} \quad (20)$$

The above expression of $\mathbf{H}^{(t)}$ can be further simplified, but Eq.(20) is convenient for use in part (f).

f) In the limit when $\mu_b \rightarrow \infty$, we will have $\sqrt{\varepsilon_b / \mu_b} \rightarrow 0$, in which case $\rho \rightarrow 1$ and $\tau \rightarrow 2$; see Eqs.(15) and (16). The tangential H -field immediately above the interface, namely, $H_{0y}^{(i)} + H_{0y}^{(r)}$, now approaches $-\sqrt{\varepsilon_0 \varepsilon_a / \mu_0 \mu_a} (1 - \rho) E_{0x}^{(i)} = 0$; see Eqs.(7) and (19). Inside the transmittance medium b , the H -field drops to zero everywhere due to the rapid exponential decay of $e^{ik_z^{(t)} z}$; see Eq.(4) — also, in accordance with Eq.(9), $H_{0y}^{(t)} \rightarrow 0$ as $\mu_b \rightarrow \infty$. The tangential H -field thus remains continuous and a surface-electric-current does *not* appear in the system.

The situation is markedly different for \mathbf{E}_{\parallel} at the $z = 0$ interface as $\mu_b \rightarrow \infty$ (and, consequently, $\rho \rightarrow 1$ and $\tau \rightarrow 2$). Here, \mathbf{E}_{\parallel} immediately above the interface will be $E_{0x}^{(i)} + E_{0x}^{(r)} = (1 + \rho) E_{0x}^{(i)} \rightarrow 2E_{0x}^{(i)}$. However, inside the transmittance medium b , the E -field everywhere approaches zero due to the rapid exponential decline of $e^{ik_z^{(t)} z}$ for $z < 0$. Considering that $\mathbf{B}^{(t)}(\mathbf{r}, t) = \mu_0 \mu_b \mathbf{H}^{(t)}(\mathbf{r}, t)$, Eq.(20) yields

$$\partial B_y^{(t)}(\mathbf{r}, t) / \partial t = -i\omega \mu_0 \mu_b H_y^{(t)}(\mathbf{r}, t) = -ik_z^{(t)} E_{0x}^{(t)} e^{i(k_z^{(t)} z - \omega t)}. \quad (21)$$

Integrating the above expression over the entire penetration depth of the transmitted B -field, one arrives at

$$\int_{z=-\infty}^0 [\partial B_y^{(t)}(\mathbf{r}, t) / \partial t] dz = -E_{0x}^{(t)} e^{i(k_z^{(t)} z - \omega t)} \Big|_{z=-\infty}^0 = -E_{0x}^{(t)} e^{-i\omega t} = -\tau E_{0x}^{(i)} e^{-i\omega t}. \quad (22)$$

Thus, in the limit when $\mu_b \rightarrow \infty$, while $\partial \mathbf{B}^{(t)} / \partial t$ goes to zero everywhere that z is negative, the integral of $\partial B_y^{(t)} / \partial t$ over the entire depth of medium b approaches $-2E_{0x}^{(i)} e^{-i\omega t}$; see Eq.(22). This, of course, is consistent with the boundary condition according to Maxwell's third equation, $\nabla \times \mathbf{E} = -\partial \mathbf{B} / \partial t$, because the time-derivative of the magnetic induction \mathbf{B} , now confined to the surface of medium b and acting as a surface-magnetic-current-density (directed along the y -axis), accounts for the discontinuity of E_x at the $z = 0$ interface.

Problem 3) a) According to the generalized Snell's law, $\omega^{(i)} = \omega^{(r)} = \omega^{(t)}$ and $k_x^{(i)} = k_x^{(r)} = k_x^{(t)}$; also, $k_y^{(i)} = k_y^{(r)} = k_y^{(t)} = 0$. Therefore, $k_z^{(r)} = \sqrt{(\omega/c)^2 n_a^2 - k_x^2} = (\omega/c) n_a \cos \theta$. Note that the chosen sign for $k_z^{(r)}$ is positive, ensuring that the reflected beam propagates upward, along the z -axis. As for the transmitted beam, the dispersion relation yields $k_z^{(t)} = \pm \sqrt{(\omega/c)^2 n_b^2 - k_x^2}$. The sign of $k_z^{(t)}$ must be chosen to ensure the exponential decay of the transmitted wave along the negative z -axis; in other words, the imaginary part of $k_z^{(t)}$ must be negative. With this understanding, we proceed to use the minus sign for $k_z^{(t)}$ in the equations that follow.

$$\begin{aligned}
\text{b) } \nabla \cdot \mathbf{D}(\mathbf{r}, t) = \rho_{\text{free}}(\mathbf{r}, t) = 0 &\rightarrow \mathbf{k} \cdot \varepsilon_0 \varepsilon(\omega) \mathbf{E}_0 e^{i(\mathbf{k} \cdot \mathbf{r} - \omega t)} = 0 \rightarrow \mathbf{k} \cdot \mathbf{E}_0 = 0 \\
&\rightarrow k_x E_{0x} + k_y E_{0y} + k_z E_{0z} = 0 \rightarrow E_{0z} = -k_x E_{0x} / k_z.
\end{aligned} \tag{1}$$

The above identity holds for all three plane-waves. Therefore,

$$E_{0z}^{(i)} = -\frac{(\omega/c)n_a \sin \theta E_{0x}^{(i)}}{-(\omega/c)n_a \cos \theta} = (\tan \theta) E_{0x}^{(i)}, \tag{2}$$

$$E_{0z}^{(r)} = -\frac{(\omega/c)n_a \sin \theta E_{0x}^{(r)}}{(\omega/c)n_a \cos \theta} = -(\tan \theta) E_{0x}^{(r)}, \tag{3}$$

$$E_{0z}^{(t)} = -\frac{(\omega/c)n_a \sin \theta E_{0x}^{(t)}}{-[(\omega/c)^2 n_b^2 - k_x^2]^{1/2}} = \frac{n_a \sin \theta}{[n_b^2 - n_a^2 \sin^2 \theta]^{1/2}} E_{0x}^{(t)}. \tag{4}$$

$$\text{c) } \nabla \times \mathbf{E}(\mathbf{r}, t) = -\partial \mathbf{B}(\mathbf{r}, t) / \partial t \rightarrow \mathbf{k} \times \mathbf{E}_0 e^{i(\mathbf{k} \cdot \mathbf{r} - \omega t)} = i\omega \mu_0 \mu(\omega) \mathbf{H}_0 e^{i(\mathbf{k} \cdot \mathbf{r} - \omega t)}$$

$$\rightarrow (k_x \hat{\mathbf{x}} + k_y \hat{\mathbf{y}} + k_z \hat{\mathbf{z}}) \times (E_{0x} \hat{\mathbf{x}} + E_{0y} \hat{\mathbf{y}} + E_{0z} \hat{\mathbf{z}}) = \omega \mu_0 \mu(\omega) \mathbf{H}_0$$

$$\rightarrow \mathbf{H}_0 = (\omega \mu_0 \mu)^{-1} [-k_z E_{0y} \hat{\mathbf{x}} + (k_z E_{0x} - k_x E_{0z}) \hat{\mathbf{y}} + k_x E_{0y} \hat{\mathbf{z}}]$$

invoking Eq.(1)

$$\rightarrow \mathbf{H}_0 = (\omega \mu_0 \mu)^{-1} \left[-k_z E_{0y} \hat{\mathbf{x}} + \left(\frac{k_x^2 + k_z^2}{k_z} \right) E_{0x} \hat{\mathbf{y}} + k_x E_{0y} \hat{\mathbf{z}} \right]. \tag{5}$$

Substituting $(\omega/c)n_a \sin \theta$ for k_x and also the relevant expressions for $k_x^{(i)}$, $k_x^{(r)}$ and $k_x^{(t)}$, we find

$$\mathbf{H}_0^{(i)} = \sqrt{\varepsilon_0 \varepsilon_a / \mu_0 \mu_a} [\cos \theta E_{0y}^{(i)} \hat{\mathbf{x}} - (E_{0x}^{(i)} / \cos \theta) \hat{\mathbf{y}} + \sin \theta E_{0y}^{(i)} \hat{\mathbf{z}}], \tag{6}$$

$$\mathbf{H}_0^{(r)} = \sqrt{\varepsilon_0 \varepsilon_a / \mu_0 \mu_a} [-\cos \theta E_{0y}^{(r)} \hat{\mathbf{x}} + (E_{0x}^{(r)} / \cos \theta) \hat{\mathbf{y}} + \sin \theta E_{0y}^{(r)} \hat{\mathbf{z}}], \tag{7}$$

$$\mathbf{H}_0^{(t)} = (c\mu_0 \mu_b)^{-1} \left[\sqrt{n_b^2 - n_a^2 \sin^2 \theta} E_{0y}^{(t)} \hat{\mathbf{x}} - \frac{n_b^2}{(n_b^2 - n_a^2 \sin^2 \theta)^{1/2}} E_{0x}^{(t)} \hat{\mathbf{y}} + n_a \sin \theta E_{0y}^{(t)} \hat{\mathbf{z}} \right]. \tag{8}$$

d) The continuity of E_x , E_y , H_x and H_y at the $z = 0$ boundary between media a and b yields

$$\text{i) } E_{0x}^{(i)} + E_{0x}^{(r)} = E_{0x}^{(t)}, \tag{9}$$

$$\begin{aligned}
\text{ii) } H_{0y}^{(i)} + H_{0y}^{(r)} = H_{0y}^{(t)} &\rightarrow \sqrt{\frac{\varepsilon_a}{\mu_a}} \left(\frac{E_{0x}^{(i)}}{\cos \theta} - \frac{E_{0x}^{(r)}}{\cos \theta} \right) = \frac{n_b^2 E_{0x}^{(t)}}{\mu_b (n_b^2 - n_a^2 \sin^2 \theta)^{1/2}} \\
&\rightarrow E_{0x}^{(i)} - E_{0x}^{(r)} = \frac{\varepsilon_b n_a \cos \theta}{\varepsilon_a (n_b^2 - n_a^2 \sin^2 \theta)^{1/2}} E_{0x}^{(t)},
\end{aligned} \tag{10}$$

$$\text{iii) } E_{0y}^{(i)} + E_{0y}^{(r)} = E_{0y}^{(t)}, \tag{11}$$

$$\begin{aligned}
\text{iv) } H_{0x}^{(i)} + H_{0x}^{(r)} = H_{0x}^{(t)} &\rightarrow \sqrt{\varepsilon_a / \mu_a} (\cos \theta E_{0y}^{(i)} - \cos \theta E_{0y}^{(r)}) = (1/\mu_b) \sqrt{n_b^2 - n_a^2 \sin^2 \theta} E_{0y}^{(t)} \\
&\rightarrow E_{0y}^{(i)} - E_{0y}^{(r)} = \frac{\mu_a (n_b^2 - n_a^2 \sin^2 \theta)^{1/2}}{\mu_b n_a \cos \theta} E_{0y}^{(t)}.
\end{aligned} \tag{12}$$

Equations (9) and (10) are a pair of coupled equations that can be solved for the Fresnel reflection and transmission coefficients for p -polarized incident light, namely, $\rho_p = E_{0x}^{(r)} / E_{0x}^{(i)}$ and $\tau_p = E_{0x}^{(t)} / E_{0x}^{(i)}$. Similarly, Eqs.(11) and (12) are a coupled pair that can be solved for $\rho_s = E_{0y}^{(r)} / E_{0y}^{(i)}$ and $\tau_s = E_{0y}^{(t)} / E_{0y}^{(i)}$ (i.e., the Fresnel reflection and transmission coefficients for s -polarized light.)