Problem 1) a) N is the number of oscillating electrons per unit volume; its SI units are $[1/m^3]$.

q is the effective charge of the oscillating particle (typically an electron); its units are [coulomb].

- ε_0 is the permittivity of free space; its units are [farad/m].
- *m* is the effective mass of the oscillating particle (typically an electron); its units are [kg].
- α is the spring constant. The model assumes that a spring connects the oscillating particle to the atomic/molecular nucleus (or the underlying lattice). α is the proportionality coefficient between the restoring force acting on the particle and the particle's displacement from equilibrium. The SI units of α are [newton/m].
- β , the friction coefficient, is the proportionality constant relating the overall frictional force acting on the oscillating particle to the particle's instantaneous velocity. The SI units of β are [newton \cdot sec/m].

The plasma frequency ω_p , the resonance frequency ω_0 , and the damping coefficient γ , all have the units of frequency, namely, [1/sec]. This should be clear from the way these parameters appear in the mathematical expression of $\chi_e(\omega)$.

b) Conduction electrons differ from bound electrons in that they are *not* connected to a nucleus (or to an underlying lattice) by a fictitious spring that would apply a restoring force to the electron. Therefore, for a conduction electron, the spring constant α is essentially zero, which makes the resonance frequency ω_0 equal to zero as well.

The Clausius-Mossotti correction is intended to remove the contribution of the local electric field $E(r)e^{-i\omega t}$ to the restoring force that acts on the oscillating particle—i.e., that part of the local *E*-field that is considered to be the self-field. This is because the Lorentz oscillator model incorporates an overall restoring force by allowing for a spring, whose spring constant is α . However, for conduction electrons, no such spring has been assumed and, therefore, there is no chance of double-counting the restoring force. Consequently, the Drude model of the conduction electron (i.e., the Lorentz oscillator model in which ω_0 is set to zero) has no need for correction.

c) Given $P(\mathbf{r},t) = \varepsilon_0 \chi_e(\omega) E(\mathbf{r}) e^{-i\omega t}$, the electric current density will be

$$\boldsymbol{J}(\boldsymbol{r},t) = \partial \boldsymbol{P}/\partial t = -\mathrm{i}\omega\varepsilon_0\chi_e(\omega)\boldsymbol{E}(\boldsymbol{r})e^{-\mathrm{i}\omega t} \quad \rightarrow \quad \sigma(\omega) = -\mathrm{i}\omega\varepsilon_0\chi_e(\omega).$$

In the Drude model, we have $\omega_0 = 0$. Consequently, $\chi_e(\omega) = -\omega_p^2 / (\omega^2 + i\gamma\omega)$, which leads to

$$\sigma(\omega) = i\varepsilon_0 \omega_p^2 / (\omega + i\gamma) = (Nq^2/m) / (\gamma - i\omega).$$

One can readily verify that the units of $\sigma(\omega)$ are [ampere/(volt · m)], i.e., the units of the current-density [ampere/m²] divided by those of the electric field [volt/m]. The electrical conductivity $\sigma(\omega)$ is related to electric resistance, whose units are [volt/ampere] or ohm [Ω]. Thus, the units of $\sigma(\omega)$ may also be described as [1/($\Omega \cdot$ m)].

Problem 2) a) Considering that $c_2^* = c_2' - ic_2''$, the real part of c_2 can be written as $\frac{1}{2}(c_2 + c_2^*)$. Therefore, $\operatorname{Re}(c_1)\operatorname{Re}(c_2) = \operatorname{Re}[c_1\operatorname{Re}(c_2)] = \frac{1}{2}\operatorname{Re}[c_1(c_2 + c_2^*)]$.

b)
$$\tilde{\mathbf{S}} = \operatorname{Re}(\mathbf{E} \times \mathbf{H}) = \operatorname{Re}[(\mathbf{E}' + i\mathbf{E}'') \times (\mathbf{H}' + i\mathbf{H}'')]$$
$$= \operatorname{Re}[(\mathbf{E}' \times \mathbf{H}' - \mathbf{E}'' \times \mathbf{H}'') + i(\mathbf{E}' \times \mathbf{H}'' + \mathbf{E}'' \times \mathbf{H}')] = \mathbf{E}' \times \mathbf{H}' - \mathbf{E}'' \times \mathbf{H}''.$$
(1)

Clearly, \tilde{S} differs from $S = \text{Re}(E) \times \text{Re}(H) = E' \times H'$, because an additional term, $E'' \times H''$, appears in the above expression of \tilde{S} .

c)
$$S(r,t) = \operatorname{Re}(E) \times \operatorname{Re}(H) = \operatorname{Re}(E) \times \frac{1}{2}(H + H^*) = \frac{1}{2}\operatorname{Re}[E \times (H + H^*)]$$

= $\frac{1}{2}\operatorname{Re}(E \times H + E \times H^*) = \frac{1}{2}\operatorname{Re}(E \times H) + \frac{1}{2}\operatorname{Re}(E \times H^*).$ (2)

d)
$$S(\mathbf{r},t) = \frac{1}{2} \operatorname{Re} \left[\mathbf{E}(\mathbf{r}) e^{-i\omega t} \times \mathbf{H}(\mathbf{r}) e^{-i\omega t} \right] + \frac{1}{2} \operatorname{Re} \left[\mathbf{E}(\mathbf{r}) e^{-i\omega t} \times \mathbf{H}^{*}(\mathbf{r}) e^{+i\omega t} \right]$$
$$= \frac{1}{2} \operatorname{Re} \left[\mathbf{E}(\mathbf{r}) \times \mathbf{H}(\mathbf{r}) (\cos 2\omega t - i\sin 2\omega t) \right] + \frac{1}{2} \operatorname{Re} \left[\mathbf{E}(\mathbf{r}) \times \mathbf{H}^{*}(\mathbf{r}) \right]$$
$$= \frac{1}{2} \operatorname{Re} \left[\mathbf{E}(\mathbf{r}) \times \mathbf{H}(\mathbf{r}) \right] \cos(2\omega t) + \frac{1}{2} \operatorname{Im} \left[\mathbf{E}(\mathbf{r}) \times \mathbf{H}(\mathbf{r}) \right] \sin(2\omega t)$$
$$+ \frac{1}{2} \operatorname{Re} \left[\mathbf{E}(\mathbf{r}) \times \mathbf{H}^{*}(\mathbf{r}) \right]. \tag{3}$$

e)
$$\langle \cos(2\omega_0 t) \rangle = T^{-1} \int_{t_0}^{t_0+T} \cos(2\omega_0 t) dt = (2\omega_0 T)^{-1} \sin(2\omega_0 t) |_{t=t_0}^{t_0+T}$$

= $(2\omega_0 T)^{-1} [\sin(2\omega_0 t_0 + 2\pi) - \sin(2\omega_0 t_0)] = 0.$ (4)

A similar calculation shows that $(\sin(2\omega_0 t)) = 0$. Substitution into Eq.(3) now yields

$$\langle \mathbf{S}(\mathbf{r},t) \rangle = \frac{1}{2} \operatorname{Re}[\mathbf{E}(\mathbf{r}) \times \mathbf{H}^{*}(\mathbf{r})].$$
(5)

Problem 3) a) From the generalized Snell's law, we have $\omega^{(i)} = \omega^{(r)} = \omega^{(t)} = \omega$, $k_x^{(i)} = k_x^{(r)} = k_x^{(t)} = k_x$ and $k_y^{(i)} = k_y^{(r)} = k_y^{(t)} = k_y$. Since the plane of incidence is chosen to be the *xz*-plane, we have $k_y = 0$. Since the incident plane-wave is said to be homogeneous, the dispersion relation yields $|\mathbf{k}^{(i)}| = n_0 \omega/c$ and, therefore, $k_x = (n_0 \omega/c) \sin \theta$. Since the incident plane-wave is downward propagating, we have $k_z^{(i)} = -(n_0 \omega/c) \cos \theta$. Similar arguments can be used to obtain the expressions of $k_z^{(r)}$ and $k_z^{(t)}$. Consequently,

$$\mathbf{k}^{(i)} = (n_0 \omega/c) (\sin \theta \, \hat{\mathbf{x}} - \cos \theta \, \hat{\mathbf{z}}), \tag{1}$$

$$\boldsymbol{k}^{(\mathrm{r})} = (n_0 \omega/c)(\sin\theta \,\hat{\boldsymbol{x}} + \cos\theta \,\hat{\boldsymbol{z}}), \qquad (2)$$

$$\boldsymbol{k}^{(t)} = (n_0 \omega/c) \left(\sin \theta \, \hat{\boldsymbol{x}} - \sqrt{(n_1/n_0)^2 - \sin^2 \theta} \, \hat{\boldsymbol{z}} \right). \tag{3}$$

The incident *E*-field is written as $\mathbf{E}^{(i)}(\mathbf{r},t) = (E_{ox}^{(i)}\hat{\mathbf{x}} + E_{oz}^{(i)}\hat{\mathbf{z}}) \exp[i(\mathbf{k}^{(i)} \cdot \mathbf{r} - \omega t)]$. Maxwell's 1st equation now relates the *z*-component of the *E*-field to its *x*-component, as follows:

$$\nabla \cdot E^{(i)}(\mathbf{r},t) = 0 \quad \rightarrow \quad \mathbf{k}^{(i)} \cdot E_0^{(i)} = 0 \quad \rightarrow \quad k_x E_{0x}^{(i)} + k_z^{(i)} E_{0z}^{(i)} = 0 \quad \rightarrow \quad E_{0z}^{(i)} = (\tan \theta) E_{0x}^{(i)}.$$
(4)

Similar expressions are found for $E_{0z}^{(r)}$ and $E_{0z}^{(t)}$; that is,

$$k_x E_{0x}^{(r)} + k_z^{(r)} E_{0z}^{(r)} = 0 \quad \rightarrow \quad E_{0z}^{(r)} = -(\tan\theta) E_{0x}^{(r)},$$
 (5)

$$k_x E_{0x}^{(t)} + k_z^{(t)} E_{0z}^{(t)} = 0 \quad \rightarrow \quad E_{0z}^{(t)} = \frac{(\sin\theta) E_{0x}^{(t)}}{\sqrt{(n_1/n_0)^2 - \sin^2\theta}}.$$
 (6)

For each plane-wave, the magnetic field H(r, t) has only one component along the *y*-axis. This component can be found from Maxwell's 3rd equation, as follows:

$$\nabla \times \boldsymbol{E} = -\partial \boldsymbol{B} / \partial t \rightarrow (k_x \hat{\boldsymbol{x}} + k_z \hat{\boldsymbol{z}}) \times (E_{0x} \hat{\boldsymbol{x}} + E_{0z} \hat{\boldsymbol{z}}) = \mu_0 \omega \boldsymbol{H}_0 \rightarrow \boldsymbol{H}_{0y} = (\mu_0 \omega)^{-1} (k_z E_{0x} - k_x E_{0z}).$$
(7)

The general expression for a *p*-polarized plane-wave's *H*-field is $H(\mathbf{r}, t) = H_{0y} \hat{\mathbf{y}} e^{i(\mathbf{k} \cdot \mathbf{r} - \omega t)}$. The various H_{0y} are found from Eq.(7) with the aid of Eqs.(1), (2), (3), (5), (6) to be

$$H_{0y}^{(i)} = (\mu_0 \omega)^{-1} [-(n_0 \omega/c) \cos \theta - (n_0 \omega/c) \sin \theta \tan \theta] E_{0x}^{(i)} = -\frac{n_0 E_{0x}^{(i)}}{Z_0 \cos \theta},$$
(8)

$$H_{0y}^{(r)} = (\mu_0 \omega)^{-1} [(n_0 \omega/c) \cos \theta + (n_0 \omega/c) \sin \theta \tan \theta] E_{0x}^{(r)} = \frac{n_0 E_{0x}^{(r)}}{Z_0 \cos \theta},$$
(9)

$$H_{0y}^{(t)} = (\mu_0 \omega)^{-1} \left[-(n_0 \omega/c) \sqrt{(n_1/n_0)^2 - \sin^2 \theta} - \frac{(n_0 \omega/c) \sin^2 \theta}{\sqrt{(n_1/n_0)^2 - \sin^2 \theta}} \right] E_{0x}^{(t)} = -\frac{(n_1^2/n_0) E_{0x}^{(t)}}{Z_0 \sqrt{(n_1/n_0)^2 - \sin^2 \theta}}.$$
 (10)

b) At the interfacial *xy*-plane separating the incidence and transmittance media, the tangential component E_x of the *E*-field must be continuous, and so does the tangential component H_y of the *H*-field. Recalling that $\rho_p = E_{0x}^{(r)}/E_{0x}^{(i)}$ and $\tau_p = E_{0x}^{(r)}/E_{0x}^{(i)}$, we write

Continuity of
$$E_{\parallel}$$
: $E_{0x}^{(i)} + E_{0x}^{(r)} = E_{0x}^{(t)} \to 1 + \rho_p = \tau_p.$ (11)

Continuity of
$$\boldsymbol{H}_{\parallel}$$
: $H_{0y}^{(i)} + H_{0y}^{(r)} = H_{0y}^{(t)} \rightarrow -\frac{n_0 E_{0x}^{(1)}}{Z_0 \cos \theta} + \frac{n_0 E_{0x}^{(r)}}{Z_0 \cos \theta} = -\frac{(n_1^2/n_0) E_{0x}^{(t)}}{Z_0 \sqrt{(n_1/n_0)^2 - \sin^2 \theta}}$
 $\rightarrow 1 - \rho_p = \frac{(n_1/n_0)^2 \cos \theta}{\sqrt{(n_1/n_0)^2 - \sin^2 \theta}} \tau_p.$ (12)

c) Considering that $n^2(\omega) = \mu(\omega)\varepsilon(\omega) = 1 + \chi_e(\omega)$, the material polarization within the transmittance medium should be written as

$$\boldsymbol{P}(\boldsymbol{r},t) = \varepsilon_0 \chi_e(\omega) \boldsymbol{E}_0^{(t)} \exp[\mathrm{i}(\boldsymbol{k}^{(t)} \cdot \boldsymbol{r} - \omega t)] = \varepsilon_0 [n_1^2(\omega) - 1] \left(E_{0x}^{(t)} \hat{\boldsymbol{x}} + E_{0z}^{(t)} \hat{\boldsymbol{z}} \right) e^{\mathrm{i}(k_x x - \omega t)} e^{\mathrm{i}k_z^{(t)} z}.$$
(13)

The bound electric charge-density $\rho_{\text{bound}}^{(e)}(\mathbf{r},t) = -\mathbf{\nabla} \cdot \mathbf{P}(\mathbf{r},t) = -i\mathbf{k} \cdot \mathbf{P}_0 e^{i(\mathbf{k} \cdot \mathbf{r} - \omega t)}$ vanishes everywhere within the transmittance medium, simply because $\mathbf{k}^{(t)} \cdot \mathbf{E}_0^{(t)} = 0$ (in accordance with Maxwell's 1st equation). As for the bound electric current-density, we will have

$$\boldsymbol{J}_{\text{bound}}^{(e)}(\boldsymbol{r},t) = \partial \boldsymbol{P} / \partial t = -i\omega\varepsilon_0 (n_1^2 - 1)(E_{0x}^{(t)}\boldsymbol{\hat{x}} + E_{0z}^{(t)}\boldsymbol{\hat{z}})e^{i(k_xx - \omega t)}e^{ik_z^{(t)}\boldsymbol{z}}.$$
 (14)

The above expression can be further streamlined by substituting for k_x and $k_z^{(t)}$ from Eq.(3), and for $E_{0z}^{(t)}$ from Eq.(6).

Digression. If the imaginary part of n_1 is taken to be positive, the imaginary part of $k_z^{(t)}$ will turn out to be negative. The integral of the bound current-density $J_{\text{bound}}^{(e)}$ over the infinite depth of the transmittance medium can then be evaluated as follows:

$$\int_{z=-\infty}^{0} \boldsymbol{J}_{\text{bound}}^{(e)}(\boldsymbol{r},t) dz = -\varepsilon_{0} (\omega/k_{z}^{(t)}) (n_{1}^{2}-1) (E_{0x}^{(t)} \hat{\boldsymbol{x}} + E_{0z}^{(t)} \hat{\boldsymbol{z}}) e^{i(k_{x}x - \omega t)} e^{ik_{z}^{(t)}z} \Big|_{z=-\infty}^{0}$$
$$= \frac{\varepsilon_{0} \omega (n_{1}^{2}-1)\tau_{p}}{(n_{0}\omega/c)\sqrt{(n_{1}/n_{0})^{2} - \sin^{2}\theta}} \Big[\hat{\boldsymbol{x}} + \frac{\sin\theta}{\sqrt{(n_{1}/n_{0})^{2} - \sin^{2}\theta}} \hat{\boldsymbol{z}} \Big] E_{0x}^{(i)} e^{i(k_{x}x - \omega t)}. \quad (15)$$

Solving Eqs.(11) and (12) for ρ_p and τ_p , we arrive at the Fresnel reflection and transmission coefficients for *p*-polarized light, as follows:

$$\rho_p = \frac{\sqrt{(n_1/n_0)^2 - \sin^2\theta} - (n_1/n_0)^2 \cos\theta}{\sqrt{(n_1/n_0)^2 - \sin^2\theta} + (n_1/n_0)^2 \cos\theta},\tag{16}$$

$$\tau_p = \frac{2\sqrt{(n_1/n_0)^2 - \sin^2\theta}}{\sqrt{(n_1/n_0)^2 - \sin^2\theta} + (n_1/n_0)^2\cos\theta}.$$
(17)

In the limit when $n_1 \to \infty$, we have $\sqrt{(n_1/n_0)^2 - \sin^2 \theta} \to (n_1/n_0)$ and $\tau_p \to 2n_0/(n_1 \cos \theta)$. The integrated current density of Eq.(15) then approaches $2n_0 E_{0x}^{(i)} \hat{x} e^{i(k_x x - \omega t)}/(Z_0 \cos \theta)$. This can be interpreted as a surface-current-density $J_s(x, y, z = 0^-, t)$ residing within the skin-depth of a highly conductive (or absorptive) transmittance medium. In the same limit, $\rho_p \to -1$, resulting in the tangential *H*-field at the *xy*-plane immediately above the interface to approach $H_{0y}^{(i)} + H_{0y}^{(r)} = -2n_0 E_{0x}^{(i)}/(Z_0 \cos \theta)$. Immediately below the interfacial *xy*-plane at $z = 0^-$, we have, in the limit,

$$H_{0y}^{(t)} = -\frac{(n_1^2/n_0 Z_0)\tau_p E_{0x}^{(i)}}{\sqrt{(n_1/n_0)^2 - \sin^2\theta}} \to -2n_0 E_{0x}^{(i)} / (Z_0 \cos\theta).$$
(18)

Consequently, the tangential *H*-field at the interface remains continuous even in the limit when $n_1 \rightarrow \infty$. However, in this limit, the fields inside the transmittance medium decay exponentially rapidly toward zero, indicating that slightly below the skin-depth (which has now shrunk to nothingness) the *H*-field vanishes. The discontinuity of the tangential *H*-field across the skin-depth is thus seen to be equal in magnitude and perpendicular in direction to the aforementioned surface-current-density J_s .

It is also worthwhile to examine the boundary condition associated with the perpendicular *D*-field across the interfacial plane. Given that $\mathbf{D} = \varepsilon_0 \varepsilon(\omega) \mathbf{E} = \varepsilon_0 n^2 \mathbf{E}$, we will have

$$D_{\perp}(x, y, z = 0^+, t) = \varepsilon_0 n_0^2 (E_{0z}^{(i)} + E_{0z}^{(r)}) e^{i(k_x x - \omega t)} = \varepsilon_0 n_0^2 \tan \theta (1 - \rho_p) E_{0x}^{(i)} e^{i(k_x x - \omega t)}, \quad (19)$$

$$D_{\perp}(x, y, z = 0^{-}, t) = \varepsilon_0 n_1^2 E_{0z}^{(t)} e^{i(k_x x - \omega t)} = \frac{\varepsilon_0 n_1^2 (\sin \theta) \tau_p}{\sqrt{(n_1/n_0)^2 - \sin^2 \theta}} E_{0x}^{(i)} e^{i(k_x x - \omega t)}.$$
 (20)

Substituting for ρ_p from Eq.(16) into Eq.(19), and for τ_p from Eq.(17) into Eq.(20), it is now easy to confirm that indeed D_1 remains continuous across the interfacial xy-plane.

The bound electric charge-density was shown in part (c) to vanish everywhere inside the transmittance medium. A similar argument can be made for the absence of $\rho_{\text{bound}}^{(e)}$ inside the incidence medium. However, the bound surface-charge-density is not zero at the interface between the two media. The material polarization of the incidence medium is given by

$$P(\mathbf{r},t) = \varepsilon_0 (n_0^2 - 1) \left[(E_{0x}^{(i)} \hat{\mathbf{x}} + E_{0z}^{(i)} \hat{\mathbf{z}}) e^{-i(n_0 \omega/c) \cos \theta z} + (E_{0x}^{(r)} \hat{\mathbf{x}} + E_{0z}^{(r)} \hat{\mathbf{z}}) e^{i(n_0 \omega/c) \cos \theta z} \right] e^{i(k_x x - \omega t)} \text{step}(z).$$
(21)

The bound electric charge-density $\rho_{\text{bound}}^{(e)}(\mathbf{r},t) = -\nabla \cdot \mathbf{P}(\mathbf{r},t)$ has an additional term arising from $\partial \text{step}(z)/\partial z = \delta(z)$, which gives rise to a surface-charge-density at $z = 0^+$, as follows:

$$\sigma_s(x, y, z = 0^+, t) = -\varepsilon_0 (n_0^2 - 1) (E_{0z}^{(i)} + E_{0z}^{(r)}) e^{i(k_x x - \omega t)}.$$
(22)

There is also a similar surface charge-density on the surface of the transmittance medium at $z = 0^{-}$, which is obtained from Eq.(13) as

$$\sigma_s(x, y, z = 0^-, t) = \varepsilon_0(n_1^2 - 1)E_{0z}^{(t)}e^{i(k_x x - \omega t)}.$$
(23)

The total surface charge-density is the sum of Eqs.(22) and (23). The terms corresponding to the continuity of D_{\perp} add up to zero (see Eqs.(19) and (20)); what remains then is

$$\sigma_{s}(x, y, z = 0^{+}, t) + \sigma_{s}(x, y, z = 0^{-}, t) = \varepsilon_{0}(E_{0z}^{(i)} + E_{0z}^{(r)} - E_{0z}^{(t)})e^{i(k_{x}x - \omega t)}.$$
 (24)

This equation reveals that the discontinuity of the perpendicular *E*-field at the interfacial *xy*-plane equals the (bound) surface-charge-density σ_s divided by ε_0 , precisely as expected from the boundary condition associated with Maxwell's 1st equation.