

Solution to Problem 1) a) Setting $\rho_{\text{free}} = 0$, $\mathbf{J}_{\text{free}} = 0$, $\mathbf{D} = \epsilon_0 \epsilon \mathbf{E}$, and $\mathbf{B} = \mu_0 \mu \mathbf{H}$, Maxwell's equations can be simplified as follows:

$$\begin{aligned}\nabla \cdot \mathbf{D}(\mathbf{r}, t) &= \epsilon_0 \epsilon \nabla \cdot \mathbf{E}(\mathbf{r}, t) = 0 && \rightarrow \nabla \cdot \mathbf{E}(\mathbf{r}) = 0. \\ \nabla \times \mathbf{H}(\mathbf{r}, t) &= \partial \mathbf{D}(\mathbf{r}, t) / \partial t = -i\omega \epsilon_0 \epsilon \mathbf{E}(\mathbf{r}, t) && \rightarrow \nabla \times \mathbf{H}(\mathbf{r}) = -i\omega \epsilon_0 \epsilon \mathbf{E}(\mathbf{r}). \\ \nabla \times \mathbf{E}(\mathbf{r}, t) &= -\partial \mathbf{B}(\mathbf{r}, t) / \partial t = i\omega \mu_0 \mu \mathbf{H}(\mathbf{r}, t) && \rightarrow \nabla \times \mathbf{E}(\mathbf{r}) = i\omega \mu_0 \mu \mathbf{H}(\mathbf{r}). \\ \nabla \cdot \mathbf{B}(\mathbf{r}, t) &= \mu_0 \mu \nabla \cdot \mathbf{H}(\mathbf{r}, t) = 0 && \rightarrow \nabla \cdot \mathbf{H}(\mathbf{r}) = 0.\end{aligned}$$

b) Taking the curl of the 3rd equation, then substituting for $\nabla \times \mathbf{H}$ from the 2nd equation, yields

$$\nabla \times \nabla \times \mathbf{E}(\mathbf{r}) = i\omega \mu_0 \mu \nabla \times \mathbf{H}(\mathbf{r}) = \mu_0 \epsilon_0 \mu \epsilon \omega^2 \mathbf{E}(\mathbf{r}) = (\sqrt{\mu \epsilon} \omega / c)^2 \mathbf{E}(\mathbf{r}).$$

From the 1st equation, we know that $\nabla \cdot \mathbf{E} = 0$. Therefore,

$$\nabla[\nabla \cdot \mathbf{E}(\mathbf{r})] - \nabla^2 \mathbf{E}(\mathbf{r}) = (\sqrt{\mu \epsilon} \omega / c)^2 \mathbf{E}(\mathbf{r}) \rightarrow \nabla^2 \mathbf{E}(\mathbf{r}) + (\sqrt{\mu \epsilon} \omega / c)^2 \mathbf{E}(\mathbf{r}) = 0.$$

c) Taking the curl of the 2nd equation, then substituting for $\nabla \times \mathbf{E}$ from the 3rd equation, yields

$$\nabla \times \nabla \times \mathbf{H}(\mathbf{r}) = -i\omega \epsilon_0 \epsilon \nabla \times \mathbf{E}(\mathbf{r}) = \mu_0 \epsilon_0 \mu \epsilon \omega^2 \mathbf{H}(\mathbf{r}) = (\sqrt{\mu \epsilon} \omega / c)^2 \mathbf{H}(\mathbf{r}).$$

From the 4th equation, we know that $\nabla \cdot \mathbf{H} = 0$. Therefore,

$$\nabla[\nabla \cdot \mathbf{H}(\mathbf{r})] - \nabla^2 \mathbf{H}(\mathbf{r}) = (\sqrt{\mu \epsilon} \omega / c)^2 \mathbf{H}(\mathbf{r}) \rightarrow \nabla^2 \mathbf{H}(\mathbf{r}) + (\sqrt{\mu \epsilon} \omega / c)^2 \mathbf{H}(\mathbf{r}) = 0.$$

Solution to Problem 2) a) The various plane-waves are all linearly-polarized along the x -axis, with their magnetic fields aligned with either $\hat{\mathbf{y}}$ or $-\hat{\mathbf{y}}$. The k -vector is either along $\hat{\mathbf{z}}$ or $-\hat{\mathbf{z}}$, its magnitude being $k_0 = \omega/c$ in air, $n_0 k_0$ in the dielectric layer, and $(n + i\kappa)k_0$ in the metallic substrate. The \mathbf{E} and \mathbf{H} fields in the three regions are

Incident beam: $\mathbf{E}^{(i)}(\mathbf{r}, t) = E_0 \hat{\mathbf{x}} \exp[-i(\omega/c)(z + ct)],$
 $\mathbf{H}^{(i)}(\mathbf{r}, t) = -(E_0/Z_0) \hat{\mathbf{y}} \exp[-i(\omega/c)(z + ct)].$

Reflected beam: $\mathbf{E}^{(r)}(\mathbf{r}, t) = \rho E_0 \hat{\mathbf{x}} \exp[i(\omega/c)(z - ct)],$
 $\mathbf{H}^{(r)}(\mathbf{r}, t) = \rho(E_0/Z_0) \hat{\mathbf{y}} \exp[i(\omega/c)(z - ct)].$

Inside dielectric: $\mathbf{E}^{(A)}(\mathbf{r}, t) = E_A \hat{\mathbf{x}} \exp[-i(\omega/c)(n_0 z + ct)],$
 $\mathbf{H}^{(A)}(\mathbf{r}, t) = -(n_0 E_A / Z_0) \hat{\mathbf{y}} \exp[-i(\omega/c)(n_0 z + ct)].$

$$\mathbf{E}^{(B)}(\mathbf{r}, t) = E_B \hat{\mathbf{x}} \exp[i(\omega/c)(n_0 z - ct)],$$

$$\mathbf{H}^{(B)}(\mathbf{r}, t) = (n_0 E_B / Z_0) \hat{\mathbf{y}} \exp[i(\omega/c)(n_0 z - ct)].$$

Inside metal: $\mathbf{E}^{(t)}(\mathbf{r}, t) = \tau E_0 \hat{\mathbf{x}} \exp\{-i(\omega/c)[(n + i\kappa)z + ct]\},$
 $\mathbf{H}^{(t)}(\mathbf{r}, t) = -[(n + i\kappa)\tau E_0 / Z_0] \hat{\mathbf{y}} \exp\{-i(\omega/c)[(n + i\kappa)z + ct]\}.$

b) Matching the boundary conditions at the air-glass interface ($z = 0$) yields

Continuity of E_{\parallel} : $E_0 + \rho E_0 = E_A + E_B \quad \rightarrow \quad (1 + \rho)E_0 = E_A + E_B.$

Continuity of H_{\parallel} : $-\frac{E_0}{Z_0} + \frac{\rho E_0}{Z_0} = -\frac{n_0 E_A}{Z_0} + \frac{n_0 E_B}{Z_0} \quad \rightarrow \quad (1 - \rho)E_0 = n_0(E_A - E_B).$

Dividing the above equations eliminates E_0 , yielding ρ in terms of $\rho_1 = (1 - n_0)/(1 + n_0)$ and E_B/E_A , as follows:

$$\frac{1 - \rho}{1 + \rho} = n_0 \frac{1 - (E_B/E_A)}{1 + (E_B/E_A)} \quad \rightarrow \quad \rho = \frac{[(1 - n_0)/(1 + n_0)] + (E_B/E_A)}{1 + [(1 - n_0)/(1 + n_0)](E_B/E_A)} = \frac{\rho_1 + (E_B/E_A)}{1 + \rho_1(E_B/E_A)}.$$

Matching the boundary conditions at the glass-metal interface ($z = -d_0$) yields

Continuity of E_{\parallel} : $E_A \exp(i\omega n_0 d_0/c) + E_B \exp(-i\omega n_0 d_0/c) = \tau E_0 \exp[i(\omega/c)(n + i\kappa)d_0].$

Continuity of H_{\parallel} : $-(n_0 E_A/Z_0) \exp(i\omega n_0 d_0/c) + (n_0 E_B/Z_0) \exp(-i\omega n_0 d_0/c) = -[(n + i\kappa)\tau E_0/Z_0] \exp[i(\omega/c)(n + i\kappa)d_0].$

Dividing the above equations eliminates the transmission coefficient τ , yielding an expression for E_B/E_A in terms of $\rho_2 = [n_0 - (n + i\kappa)]/[n_0 + (n + i\kappa)] = |\rho_2| \exp(i\varphi_2)$ and the round-trip phase $\varphi_0 = 2\omega n_0 d_0/c = 4\pi n_0 d_0/\lambda_0$, namely,

$$\frac{E_A \exp(i\omega n_0 d_0/c) - E_B \exp(-i\omega n_0 d_0/c)}{E_A \exp(i\omega n_0 d_0/c) + E_B \exp(-i\omega n_0 d_0/c)} = \frac{n + i\kappa}{n_0} \quad \rightarrow \quad \frac{\exp(i\varphi_0) - (E_B/E_A)}{\exp(i\varphi_0) + (E_B/E_A)} = (n + i\kappa)/n_0$$

$$\rightarrow \frac{E_B}{E_A} = \frac{n_0 - (n + i\kappa)}{n_0 + (n + i\kappa)} \exp(i\varphi_0) = \rho_2 \exp(i\varphi_0) = |\rho_2| \exp[i(\varphi_2 + \varphi_0)].$$

c) Substitution for E_B/E_A from the above equation into an earlier expression for ρ now yields

$$\rho = \frac{\rho_1 + |\rho_2| \exp[i(\varphi_2 + \varphi_0)]}{1 + \rho_1 |\rho_2| \exp[i(\varphi_2 + \varphi_0)]}.$$

The reflectance of the coated metallic surface is obtained by squaring the magnitude of the above Fresnel reflection coefficient, that is,

$$R = |\rho|^2 = \rho \rho^* = \frac{\rho_1^2 + |\rho_2|^2 + 2\rho_1 |\rho_2| \cos(\varphi_0 + \varphi_2)}{1 + \rho_1^2 |\rho_2|^2 + 2\rho_1 |\rho_2| \cos(\varphi_0 + \varphi_2)}.$$

d) The reflectance R is a function of the round-trip phase $\varphi_0 = 4\pi n_0 d_0/\lambda_0$, which may be adjusted by varying the thickness d_0 of the dielectric layer. The maximum and minimum values of R are determined by setting its derivative with respect to φ_0 equal to zero, that is,

$$\frac{dR}{d\varphi_0} = -\frac{2\rho_1 |\rho_2| (1 - \rho_1^2)(1 - |\rho_2|^2) \sin(\varphi_0 + \varphi_2)}{[1 + \rho_1^2 |\rho_2|^2 + 2\rho_1 |\rho_2| \cos(\varphi_0 + \varphi_2)]^2} = 0 \quad \rightarrow \quad \sin(\varphi_0 + \varphi_2) = 0.$$

Considering that $\rho_1 < 0$, the reflectance reaches a minimum when $\cos(\varphi_0 + \varphi_2) = 1$, that is,

$$R_{\min} = \left(\frac{\rho_1 + |\rho_2|}{1 + \rho_1 |\rho_2|} \right)^2.$$

The maximum reflectance is reached when $\cos(\varphi_0 + \varphi_2) = -1$, that is,

$$R_{\max} = \left(\frac{\rho_1 - |\rho_2|}{1 - \rho_1 |\rho_2|} \right)^2.$$