

Problem 1) a) At normal incidence, $\theta = 0$, we find

$$r_p = \frac{n_1 \sqrt{\epsilon_2} - \epsilon_2}{n_1 \sqrt{\epsilon_2} + \epsilon_2} = \frac{n_1 - \sqrt{\epsilon_2}}{n_1 + \sqrt{\epsilon_2}},$$

$$r_s = \frac{n_1 - \sqrt{\epsilon_2}}{n_1 + \sqrt{\epsilon_2}}.$$

Thus $r_p = r_s$ at normal incidence. This is expected, of course, because at normal incidence there is no difference between p- and s-polarizations; that is, at $\theta = 0$ the plane of incidence, relative to which p- and s- directions are defined, becomes indeterminate.

b) TIR occurs when the second medium is also transparent, that is, when ϵ_2 is real and positive. In TIR we must have $|r_p| = 1$ and $|r_s| = 1$. Each expression is the ratio of the sum to the difference of two numbers. When two complex numbers have a phase difference of 90° , their sum and difference will have exactly the same magnitudes and, therefore, the ratio of difference to sum will have a magnitude of 1. In the formulas for r_p and r_s , since n_1 , ϵ_2 , $\sin \theta$, and $\cos \theta$ are all real numbers, the only way that the numbers in the numerator and denominator of r_p and r_s could acquire a 90° phase difference would be for the square-roots to become purely imaginary. Therefore, when $\epsilon_2 - n_1^2 \sin^2 \theta < 0$, the square-roots become imaginary, the two numbers appearing in the numerator and denominator of each expression for the Fresnel coefficient become 90° apart, and we obtain $|r_p| = |r_s| = 1$. The condition for TIR is, therefore,

$$\epsilon_2 - n_1^2 \sin^2 \theta < 0 \Rightarrow \sin^2 \theta > \frac{\epsilon_2}{n_1^2} = \frac{n_2^2}{n_1^2}$$

$$\Rightarrow \sin \theta > \frac{n_2}{n_1}$$

Since $\sin \theta$ can't exceed unity, we must have $n_2 < n_1$. The critical angle $\theta_c = \sin^{-1} \left(\frac{n_2}{n_1} \right)$.

From the above argument it is clear that the same critical angle pertains to both p- and s-polarized plane-waves. However, one can argue on physical grounds that the critical angles must be the same, as follows: For $|r_p| = 1$ and/or $|r_s| = 1$, we must have 100% of the incident optical energy reflected back into the incidence medium. This means that the transmitted beam in both cases (i.e., p- and s-polarization) can't carry any energy and must, therefore, be evanescent. Now, the condition for evanescence is a condition on the k-vector of the transmitted plane-wave, not on its E- and H-field amplitudes. When the boundary conditions are matched, the k-vector is determined by the requirement that k_x and k_y (and also ω) be the same for the incident, reflected, and transmitted plane-waves. This step in matching the boundary condition is what we've called "Snell's law." Thus, transition from propagating to evanescent field occurs as a result of the application of Snell's law to the k-vectors, which is independent of the incident beam being p- or s-polarized. The condition for TIR, therefore, is not dependent on the state of polarization of the incident beam.

c) At Brewster's angle $r_p = 0 \Rightarrow n_1 \sqrt{\epsilon_2 - n_1^2 \sin^2 \theta} = \epsilon_2 \cos \theta \Rightarrow$

$$n_1^2 (\epsilon_2 - n_1^2 \sin^2 \theta) = \epsilon_2^2 \cos^2 \theta \Rightarrow \frac{n_1^2 \epsilon_2}{\epsilon_2^2 \cos^2 \theta} - \frac{n_1^4 \sin^2 \theta}{\epsilon_2^2 \cos^2 \theta} = 1 \Rightarrow \left(\frac{n_1^2}{\epsilon_2}\right) (1 + \tan^2 \theta) - \left(\frac{n_1^2}{\epsilon_2}\right)^2 \tan^2 \theta = 1$$

$$\Rightarrow \frac{n_1^2}{\epsilon_2} - 1 = \left(\frac{n_1^2}{\epsilon_2}\right) \left(\frac{n_1^2}{\epsilon_2} - 1\right) \tan^2 \theta \Rightarrow \tan^2 \theta = \frac{\epsilon_2}{n_1^2} \Rightarrow \tan \theta = \frac{n_2 + ik_2}{n_1}$$

(In the above derivation, we have ignored the trivial solution $\frac{n_1^2}{\epsilon_2} - 1 = 0$, which yields $n_1^2 = \epsilon_2 \Rightarrow n_1 = \sqrt{\epsilon_2} \Rightarrow$ no mismatch of impedances at the interface.)

Now, for a non-trivial solution to exist, we must have $\tan \theta = (n_2/n_1) + i(k_2/n_1)$. However, $\tan \theta$ is real-valued; therefore k_2 must be zero. Moreover, $0 < \theta < 90^\circ$ requires that $\tan \theta > 0$. Therefore $n_2 > 0$. Thus for Brewster's angle to exist we must have ϵ_2 real-valued and positive. The incidence angle at which $r_p = 0$ is then given by $\theta = \tan^{-1}(\sqrt{\epsilon_2}/n_1)$. Note that $n_2 = \sqrt{\epsilon_2} > n_1$ and $n_2 < n_1$ are both possible.

Brewster's angle does not exist for s-light because:

$$P_s = 0 \Rightarrow n_1 \cos \theta = \sqrt{\epsilon_2 - n_1^2 \sin^2 \theta} \Rightarrow n_1^2 \cos^2 \theta = \epsilon_2 - n_1^2 \sin^2 \theta \Rightarrow n_1^2 (\cos^2 \theta + \sin^2 \theta) = \epsilon_2$$

$$\Rightarrow n_1^2 = \epsilon_2, \text{ i.e., trivial case when there is no impedance mis-match at the interface between the two media.}$$

d) We already saw in part (c) above that for P_p to become zero, we must have $K_2 = 0$. Thus any absorption (or gain for that matter) is incompatible with the existence of a Brewster's angle.

e) When $\theta \rightarrow 90^\circ$, $\sin \theta \rightarrow 1$ and $\cos \theta \rightarrow 0$. Therefore,

$$P_p \rightarrow \frac{n_1 \sqrt{\epsilon_2 - n_1^2}}{n_1 \sqrt{\epsilon_2 - n_1^2}} = +1 \quad P_s \rightarrow \frac{-\sqrt{\epsilon_2 - n_1^2}}{+\sqrt{\epsilon_2 - n_1^2}} = -1$$

With s-light, the incident and reflected plane-waves cancel each other out, and there will be no E-field parallel to the surface, nor an H-field \perp to the surface. The same thing happens with p-light; however, one must be careful in interpreting the meaning of P_p , as it is the ratio of $E_{x_0}^r$ to $E_{x_0}^i$. Indeed, the ratio of $E_{z_0}^r$ to $E_{z_0}^i$ approaches -1 for p-light as well, and so does $H_{y_0}^r/H_{y_0}^i$.

f) The answer is yes, there can be total reflection at the interface when $K_2 \neq 0$ but then we must have $n_2 = 0$; in other words, we must have ϵ_2 real-valued and negative. The proof is as follows:

i) Case of s-polarization.

$$|P_s|^2 = 1 \Rightarrow (n_1 \cos \theta - \sqrt{\epsilon_2 - n_1^2 \sin^2 \theta}) (n_1 \cos \theta - \sqrt{\epsilon_2 - n_1^2 \sin^2 \theta})^* = (n_1 \cos \theta + \sqrt{\epsilon_2 - n_1^2 \sin^2 \theta}) (n_1 \cos \theta + \sqrt{\epsilon_2 - n_1^2 \sin^2 \theta})^*$$

$$\Rightarrow -n_1 \cos \theta \sqrt{\epsilon_2 - n_1^2 \sin^2 \theta}^* - n_1 \cos \theta \sqrt{\epsilon_2 - n_1^2 \sin^2 \theta} = n_1 \cos \theta \sqrt{\epsilon_2 - n_1^2 \sin^2 \theta}^* + n_1 \cos \theta \sqrt{\epsilon_2 - n_1^2 \sin^2 \theta}$$

$$\Rightarrow \sqrt{\epsilon_2 - n_1^2 \sin^2 \theta} + \sqrt{\epsilon_2 - n_1^2 \sin^2 \theta}^* = 0 \Rightarrow \sqrt{\epsilon_2 - n_1^2 \sin^2 \theta} = \text{purely imaginary} = i\alpha$$

$$\Rightarrow \epsilon_2 - n_1^2 \sin^2 \theta = -\alpha^2 \Rightarrow \epsilon_2 = n_1^2 \sin^2 \theta - \alpha^2 \Rightarrow \epsilon_2 \text{ is purely real.}$$

↑
real number

↑
arbitrary
real number

Now, if ϵ_2 is a positive real number, we'll have the condition for conventional TIR at the interface between two transparent media, namely, $\sin \theta > \frac{n_2}{n_1} = \frac{\sqrt{\epsilon_2}}{n_1}$. However, if ϵ_2 is a negative real number, then $\sqrt{\epsilon_2 - n_1^2 k^2 \theta}$ will be ~~negative~~ ^{imaginary} for all values of θ and, therefore, 100% reflection occurs at all θ .

ii) Case of P-polarization:

$$|r_p|^2 = 1 \Rightarrow (n_1 \sqrt{\epsilon_2 - n_1^2 k^2 \theta} - \epsilon_2 \cos \theta) (n_1 \sqrt{\epsilon_2 - n_1^2 k^2 \theta} - \epsilon_2 \cos \theta)^* = (n_1 \sqrt{\epsilon_2 - n_1^2 k^2 \theta} + \epsilon_2 \cos \theta) (n_1 \sqrt{\epsilon_2 - n_1^2 k^2 \theta} + \epsilon_2 \cos \theta)^*$$

$$\Rightarrow n_1 \sqrt{\epsilon_2 - n_1^2 k^2 \theta} \epsilon_2^* \cos \theta - \epsilon_2 \cos \theta n_1 \sqrt{\epsilon_2 - n_1^2 k^2 \theta} = n_1 \sqrt{\epsilon_2 - n_1^2 k^2 \theta} \epsilon_2^* \cos \theta + \epsilon_2 \cos \theta n_1 \sqrt{\epsilon_2 - n_1^2 k^2 \theta}$$

$$\Rightarrow \epsilon_2^* \sqrt{\epsilon_2 - n_1^2 k^2 \theta} + \epsilon_2 \sqrt{\epsilon_2 - n_1^2 k^2 \theta} = 0 \Rightarrow \epsilon_2^* \sqrt{\epsilon_2 - n_1^2 k^2 \theta} = \text{Purely imaginary} = i \alpha$$

$$\Rightarrow (\epsilon_2' - i \epsilon_2'')^2 (\epsilon_2' - n_1^2 k^2 \theta + i \epsilon_2'') = -\alpha^2$$

↑ arbitrary real number

$$\Rightarrow (\epsilon_2'^2 - \epsilon_2''^2 - 2i \epsilon_2' \epsilon_2'') (\epsilon_2' - n_1^2 k^2 \theta + i \epsilon_2'') = -\alpha^2 \Rightarrow \begin{cases} (\epsilon_2'^2 - \epsilon_2''^2) (\epsilon_2' - n_1^2 k^2 \theta) + 2 \epsilon_2' \epsilon_2'' = -\alpha^2 \\ (\epsilon_2'^2 - \epsilon_2''^2) \epsilon_2'' - 2 \epsilon_2' \epsilon_2'' (\epsilon_2' - n_1^2 k^2 \theta) = 0 \end{cases}$$

$$\Rightarrow \begin{cases} \epsilon_2'^3 - \epsilon_2'^2 n_1^2 k^2 \theta - \epsilon_2''^2 (\epsilon_2' - n_1^2 k^2 \theta - 2 \epsilon_2') = -\alpha^2 \\ \epsilon_2'' (\epsilon_2'' + \epsilon_2'^2 - 2 \epsilon_2' n_1^2 k^2 \theta) = 0 \end{cases} \Rightarrow \begin{cases} \epsilon_2'' = 0 & \leftarrow \text{First solution} \\ \epsilon_2''^2 = 2 \epsilon_2' n_1^2 k^2 \theta - \epsilon_2'^2 & \leftarrow \text{Second solution} \end{cases}$$

First solution: $\epsilon_2'' = 0 \Rightarrow \epsilon_2'^3 - \epsilon_2'^2 n_1^2 k^2 \theta = -\alpha^2 \Rightarrow \epsilon_2'^2 (\epsilon_2' - n_1^2 k^2 \theta) = -\alpha^2$

$$\Rightarrow \epsilon_2' - n_1^2 k^2 \theta = \text{negative real number} \Rightarrow \begin{cases} \epsilon_2' < 0 \\ 0 < \epsilon_2' < n_1^2 k^2 \theta \end{cases}$$

Therefore, there exists two possibilities: (i) Conventional TIR, where ϵ_2 is real and positive, and $\sin \theta > \frac{n_2}{n_1} \Rightarrow \sin \theta > \frac{\sqrt{\epsilon_2}}{n_1}$.

(ii) ϵ_2 real and negative, in which case $|r_p| = 1$ for all angles of incidence θ ,

Second solution: $\epsilon_2''^2 = 2\epsilon_2' \eta_1^2 A^2 \theta - \epsilon_2'^2 \Rightarrow \epsilon_2'^3 - \epsilon_2'^2 \eta_1^2 A^2 \theta + (2\epsilon_2' \eta_1^2 A^2 \theta - \epsilon_2'^2)(\epsilon_2' + \eta_1^2 A^2 \theta) = -\alpha^2$

$$\Rightarrow \cancel{\epsilon_2'^3} - \cancel{\epsilon_2'^2 \eta_1^2 A^2 \theta} + 2\epsilon_2'^2 \eta_1^2 A^2 \theta + 2\epsilon_2' \eta_1^4 A^4 \theta - \cancel{\epsilon_2'^3} - \cancel{\epsilon_2'^2 \eta_1^2 A^2 \theta} = -\alpha^2$$

$$\Rightarrow 2\epsilon_2' \eta_1^4 A^4 \theta = -\alpha^2 \Rightarrow \epsilon_2' \text{ must be purely negative.}$$

However, if this happens, we'll have $\epsilon_2''^2 = 2\epsilon_2' \eta_1^2 A^2 \theta - \epsilon_2'^2 < 0$,

which is unacceptable for $\epsilon_2''^2$, a purely positive number. Therefore, a second solution does not exist.

Problem 2) a) $\vec{\nabla} \cdot \vec{J} + \frac{\partial \rho}{\partial t} = 0 \Rightarrow I(t) = \frac{dq(t)}{dt} \Rightarrow \frac{dq}{dt} = I_0 \sin(2\pi f t) \Rightarrow$

$$q(t) = \int_{-\infty}^t I_0 \sin(2\pi f t') dt' = -\frac{I_0}{2\pi f} \cos(2\pi f t) + \text{Constant.}$$

b) $\vec{p}(t) = q(t) d \hat{z} = -\frac{I_0 d}{2\pi f} \cos(2\pi f t) \hat{z} \leftarrow \text{Constant (static) dipole has been ignored.}$

c) In spherical coordinates $\hat{z} = \cos\theta \hat{r} - \sin\theta \hat{\theta}$.

$$\mu_0 \vec{H}(\vec{r}, t) = \vec{B}(\vec{r}, t) = \vec{\nabla} \times \vec{A}(\vec{r}, t) = \frac{\mu_0 I_0 d}{4\pi} \vec{\nabla} \times \left\{ \frac{1}{r} \sin[2\pi f(t - \frac{r}{c})] (\cos\theta \hat{r} - \sin\theta \hat{\theta}) \right\} \Rightarrow$$

$$\vec{H}(\vec{r}, t) = \frac{I_0 d}{4\pi r} \left[\frac{\partial}{\partial r} (r A_\theta) - \frac{\partial A_r}{\partial \theta} \right] \hat{\phi} = \frac{I_0 d \hat{\phi}}{4\pi r} \left\{ -\sin\theta \frac{\partial}{\partial r} \sin[2\pi f(t - \frac{r}{c})] - \frac{1}{r} \sin[2\pi f(t - \frac{r}{c})] \frac{\partial \cos\theta}{\partial \theta} \right\}$$

$$\Rightarrow \vec{H}(\vec{r}, t) = \frac{I_0 d \sin\theta}{4\pi r} \left\{ \frac{2\pi f}{c} \cos[2\pi f(t - \frac{r}{c})] + \frac{1}{r} \sin[2\pi f(t - \frac{r}{c})] \right\} \hat{\phi}$$

d) $\vec{E}(\vec{r}, t) = -\vec{\nabla} \psi - \frac{\partial \vec{A}}{\partial t} = -\frac{\partial \psi}{\partial r} \hat{r} - \frac{1}{r} \frac{\partial \psi}{\partial \theta} \hat{\theta} - \frac{\partial \vec{A}}{\partial t} \Rightarrow$

$$\vec{E}(\vec{r}, t) = -\frac{Z_0 I_0 d}{4\pi} \cos\theta \frac{\partial}{\partial r} \left\{ \frac{1}{r} \sin[\dots] - \frac{\lambda_0}{2\pi r^2} \cos[\dots] \right\} \hat{r} + \frac{Z_0 I_0 d}{4\pi r} \sin\theta \left\{ \frac{1}{r} \sin[\dots] - \frac{\lambda_0}{2\pi r^2} \cos[\dots] \right\} \hat{\theta} \\ - \frac{\mu_0 I_0 d}{4\pi r} (2\pi f) \cos[\dots] (\cos\theta \hat{r} - \sin\theta \hat{\theta}) \Rightarrow$$

$$\vec{E}(\vec{r}, t) = \frac{Z_0 I_0 d}{4\pi} \left\{ \left[\frac{1}{r^2} \sin[2\pi f(t - r/c)] - \frac{\lambda_0}{2\pi r^3} \cos[2\pi f(t - r/c)] \right] (2\cos\theta \hat{r} + \sin\theta \hat{\theta}) \right. \\ \left. + \frac{2\pi}{\lambda_0 r} \sin\theta \cos[2\pi f(t - r/c)] \hat{\theta} \right\}$$

e) In the far field region all terms that decrease as $1/r^2$ and $1/r^3$ can be ignored. We'll have:

$$\left. \begin{aligned} \vec{E}(\vec{r}, t) &\simeq \frac{Z_0 I_0 d}{2\lambda_0 r} \sin\theta \cos[2\pi f(t - r/c)] \hat{\theta} \\ \vec{H}(\vec{r}, t) &\simeq \frac{I_0 d}{2\lambda_0 r} \sin\theta \cos[2\pi f(t - r/c)] \hat{\phi} \end{aligned} \right\} \leftarrow \text{Note: } \frac{2\pi f}{c} = \frac{2\pi}{\lambda_0}$$

$$\vec{S}(\vec{r}, t) = \vec{E}(\vec{r}, t) \times \vec{H}(\vec{r}, t) = \frac{Z_0}{4} \left(\frac{I_0 d}{\lambda_0} \right)^2 \frac{\sin^2\theta}{r^2} \cos^2[2\pi f(t - r/c)] \hat{r}$$