

**Problem 1)** a) The  $E$ - and  $H$ -fields of the incident plane-wave are given by

$$\mathbf{E}(\mathbf{r}, t) = \mathbf{E}_{p_0}^{(i)} \exp[i(\mathbf{k}^{(i)} \cdot \mathbf{r} - \omega t)]; \quad (1a)$$

$$\mathbf{H}(\mathbf{r}, t) = \mathbf{H}_{p_0}^{(i)} \exp[i(\mathbf{k}^{(i)} \cdot \mathbf{r} - \omega t)]. \quad (1b)$$

The dispersion relation in free space is  $k^2 = (\omega/c)^2$ . Therefore,

$$\mathbf{k}^{(i)} = k_x \hat{\mathbf{x}} + k_z \hat{\mathbf{z}} = (\omega/c)(\sin \theta \hat{\mathbf{x}} + \cos \theta \hat{\mathbf{z}}). \quad (2)$$

The incident  $E$ -field amplitude, as shown in the figure, is given by

$$\mathbf{E}_{p_0}^{(i)} = E_{p_0} (\cos \theta \hat{\mathbf{x}} - \sin \theta \hat{\mathbf{z}}). \quad (3)$$

It may be readily verified that this  $E$ -field satisfies Maxwell's first equation, namely,  $\nabla \cdot \mathbf{E} = 0$ , which is equivalent to  $\mathbf{k}^{(i)} \cdot \mathbf{E}_{p_0}^{(i)} = 0$ . As for the incident  $H$ -field, Maxwell's third equation,  $\nabla \times \mathbf{E} = -\partial \mathbf{B} / \partial t$ , yields

$$\begin{aligned} i\mathbf{k}^{(i)} \times \mathbf{E}_{p_0}^{(i)} = i\omega\mu_0 \mathbf{H}_{p_0}^{(i)} &\rightarrow (\omega/c)(\sin \theta \hat{\mathbf{x}} + \cos \theta \hat{\mathbf{z}}) \times E_{p_0} (\cos \theta \hat{\mathbf{x}} - \sin \theta \hat{\mathbf{z}}) = \omega\mu_0 \mathbf{H}_{p_0}^{(i)} \\ &\rightarrow \mathbf{H}_{p_0}^{(i)} = (E_{p_0}/Z_0) \hat{\mathbf{y}}. \end{aligned} \quad (4)$$

b) The  $E$ - and  $H$ -fields of the reflected wave are written

$$\mathbf{E}(\mathbf{r}, t) = \mathbf{E}_{p_0}^{(r)} \exp[i(\mathbf{k}^{(r)} \cdot \mathbf{r} - \omega t)]; \quad (5a)$$

$$\mathbf{H}(\mathbf{r}, t) = \mathbf{H}_{p_0}^{(r)} \exp[i(\mathbf{k}^{(r)} \cdot \mathbf{r} - \omega t)]. \quad (5b)$$

The reflected  $k$ -vector is similar to the incident  $k$ -vector, except for the sign of  $k_z$ , that is,

$$\mathbf{k}^{(r)} = k_x \hat{\mathbf{x}} - k_z \hat{\mathbf{z}} = (\omega/c)(\sin \theta \hat{\mathbf{x}} - \cos \theta \hat{\mathbf{z}}). \quad (6)$$

The reflected  $E$ -field amplitude must cancel out the tangential component of the incident  $E$ -field at the surface of the perfect conductor, as there cannot be any  $E$ -fields inside the conductor. We thus have

$$\mathbf{E}_{p_0}^{(r)} = -E_{p_0} (\cos \theta \hat{\mathbf{x}} + \sin \theta \hat{\mathbf{z}}). \quad (7)$$

As before, it may be readily verified that the above  $E$ -field satisfies Maxwell's first equation, namely,  $\mathbf{k}^{(r)} \cdot \mathbf{E}_{p_0}^{(r)} = 0$ . The reflected  $H$ -field is, once again, obtained from Maxwell's third equation, as follows:

$$\begin{aligned} i\mathbf{k}^{(r)} \times \mathbf{E}_{p_0}^{(r)} = i\omega\mu_0 \mathbf{H}_{p_0}^{(r)} &\rightarrow (\omega/c)(\sin \theta \hat{\mathbf{x}} - \cos \theta \hat{\mathbf{z}}) \times E_{p_0} (-\cos \theta \hat{\mathbf{x}} - \sin \theta \hat{\mathbf{z}}) = \omega\mu_0 \mathbf{H}_{p_0}^{(r)} \\ &\rightarrow \mathbf{H}_{p_0}^{(r)} = (E_{p_0}/Z_0) \hat{\mathbf{y}}. \end{aligned} \quad (8)$$

c) The rate of flow of energy per unit cross-sectional area per unit time is given by the time-averaged Poynting vector, namely,

$$\begin{aligned}
\langle \mathbf{S}^{(i)}(\mathbf{r}, t) \rangle &= \frac{1}{2} \text{Re}[\mathbf{E}_{p_0}^{(i)} \times \mathbf{H}_{p_0}^{(i)*}] = \frac{1}{2} \text{Re}[E_{p_0} (\cos \theta \hat{\mathbf{x}} - \sin \theta \hat{\mathbf{z}}) \times (E_{p_0}^*/Z_0) \hat{\mathbf{y}}] \\
&= \frac{|E_{p_0}|^2}{2Z_0} (\sin \theta \hat{\mathbf{x}} + \cos \theta \hat{\mathbf{z}}). \tag{9}
\end{aligned}$$

$$\begin{aligned}
\langle \mathbf{S}^{(r)}(\mathbf{r}, t) \rangle &= \frac{1}{2} \text{Re}[\mathbf{E}_{p_0}^{(r)} \times \mathbf{H}_{p_0}^{(r)*}] = \frac{1}{2} \text{Re}[-E_{p_0} (\cos \theta \hat{\mathbf{x}} + \sin \theta \hat{\mathbf{z}}) \times (E_{p_0}^*/Z_0) \hat{\mathbf{y}}] \\
&= \frac{|E_{p_0}|^2}{2Z_0} (\sin \theta \hat{\mathbf{x}} - \cos \theta \hat{\mathbf{z}}). \tag{10}
\end{aligned}$$

The incident and reflected waves are seen to have a time-averaged Poynting vector  $\langle \mathbf{S} \rangle$  directed along the corresponding  $k$ -vector. The magnitudes of these Poynting vectors, however, are the same, namely,  $|E_{p_0}|^2/(2Z_0)$ . Therefore, the incident and reflected energy fluxes are identical.

d) The surface-current-density  $\mathbf{J}_s(x, y, t)$  is equal in magnitude and perpendicular in direction to the total  $H$ -field at the surface of the perfect conductor. Taking into account the right-hand rule relating the direction of the surface current to that of the  $H$ -field, we will have

$$\begin{aligned}
\mathbf{J}_s(x, y, t) &= [H_y^{(i)}(x, y, z=0, t) + H_y^{(r)}(x, y, z=0, t)] \hat{\mathbf{x}} \\
&= 2(E_{p_0}/Z_0) \exp[i(k_x x - \omega t)] \hat{\mathbf{x}} = 2(E_{p_0}/Z_0) \exp[i(\omega/c)(x \sin \theta - ct)] \hat{\mathbf{x}}. \tag{11}
\end{aligned}$$

e) The surface-charge-density  $\sigma_s(x, y, t)$  is given by the discontinuity in the perpendicular component of the  $D$ -field, that is,

$$\begin{aligned}
\sigma_s(x, y, t) &= -\epsilon_0 [E_z^{(i)}(x, y, z=0, t) + E_z^{(r)}(x, y, z=0, t)] \\
&= 2\epsilon_0 E_{p_0} \sin \theta \exp[i(k_x x - \omega t)] = 2\epsilon_0 E_{p_0} \sin \theta \exp[i(\omega/c)(x \sin \theta - ct)]. \tag{12}
\end{aligned}$$

f) Substituting in the continuity equation for  $\mathbf{J}_s$  from Eq.(11) and for  $\sigma_s$  from Eq.(12), we find

$$\begin{aligned}
\partial J_{sx} / \partial x + \partial \sigma_s / \partial t &= [2i(\omega/c) \sin \theta (E_{p_0}/Z_0) - 2i\omega\epsilon_0 E_{p_0} \sin \theta] \exp[i(\omega/c)(x \sin \theta - ct)] \\
&= 2i\omega [(cZ_0)^{-1} - \epsilon_0] E_{p_0} \sin \theta \exp[i(\omega/c)(x \sin \theta - ct)] = 0. \tag{13}
\end{aligned}$$

The continuity equation is thus satisfied by the induced surface-charge and surface-current.

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**Problem 2)** a) The  $E$ - and  $H$ -fields of the incident plane-wave are given by

$$\mathbf{E}(\mathbf{r}, t) = \mathbf{E}_{so}^{(i)} \exp[i(\mathbf{k}^{(i)} \cdot \mathbf{r} - \omega t)]; \quad (1a)$$

$$\mathbf{H}(\mathbf{r}, t) = \mathbf{H}_{so}^{(i)} \exp[i(\mathbf{k}^{(i)} \cdot \mathbf{r} - \omega t)]. \quad (1b)$$

The dispersion relation in free space is  $k^2 = (\omega/c)^2$ . Therefore,

$$\mathbf{k}^{(i)} = k_x \hat{\mathbf{x}} + k_z \hat{\mathbf{z}} = (\omega/c)(\sin \theta \hat{\mathbf{x}} + \cos \theta \hat{\mathbf{z}}). \quad (2)$$

The incident  $E$ -field amplitude, as shown in the figure, is given by

$$\mathbf{E}_{so}^{(i)} = E_{so}^{(i)} \hat{\mathbf{y}}. \quad (3)$$

It may be readily verified that this  $E$ -field satisfies Maxwell's first equation, namely,  $\nabla \cdot \mathbf{E} = 0$ , which is equivalent to  $\mathbf{k}^{(i)} \cdot \mathbf{E}_{so}^{(i)} = 0$ . As for the incident  $H$ -field, Maxwell's third equation,  $\nabla \times \mathbf{E} = -\partial \mathbf{B} / \partial t$ , yields

$$\begin{aligned} i\mathbf{k}^{(i)} \times \mathbf{E}_{so}^{(i)} = i\omega\mu_0 \mathbf{H}_{so}^{(i)} &\rightarrow (\omega/c)(\sin \theta \hat{\mathbf{x}} + \cos \theta \hat{\mathbf{z}}) \times E_{so}^{(i)} \hat{\mathbf{y}} = \omega\mu_0 \mathbf{H}_{so}^{(i)} \\ &\rightarrow \mathbf{H}_{so}^{(i)} = -(E_{so}^{(i)} / Z_0)(\cos \theta \hat{\mathbf{x}} - \sin \theta \hat{\mathbf{z}}). \end{aligned} \quad (4)$$

A similar treatment yields for the reflected plane-wave,

$$\mathbf{k}^{(r)} = k_x \hat{\mathbf{x}} - k_z \hat{\mathbf{z}} = (\omega/c)(\sin \theta \hat{\mathbf{x}} - \cos \theta \hat{\mathbf{z}}), \quad (5)$$

$$\mathbf{E}_{so}^{(r)} = E_{so}^{(r)} \hat{\mathbf{y}}, \quad (6)$$

$$\mathbf{H}_{so}^{(r)} = (E_{so}^{(r)} / Z_0)(\cos \theta \hat{\mathbf{x}} + \sin \theta \hat{\mathbf{z}}). \quad (7)$$

As for the transmitted beam, the dispersion relation in the dielectric medium is  $k^2 = (\omega/c)^2 n^2(\omega)$ ; also, in accordance with Snell's law, we must have  $k_x^{(t)} = k_x^{(i)}$  and  $k_y^{(t)} = k_y^{(i)} = 0$ . Therefore,

$$\mathbf{k}^{(t)} = k_x^{(i)} \hat{\mathbf{x}} + k_z^{(t)} \hat{\mathbf{z}} = (\omega/c) [\sin \theta \hat{\mathbf{x}} + \sqrt{n^2(\omega) - \sin^2 \theta} \hat{\mathbf{z}}]. \quad (8)$$

Next, we obtain the transmitted  $E$ -field using the continuity of tangential  $\mathbf{E}$  at the interface:

$$\mathbf{E}_{so}^{(t)} = (E_{so}^{(i)} + E_{so}^{(r)}) \hat{\mathbf{y}}. \quad (9)$$

Subsequently, the transmitted  $H$ -field is obtained from Maxwell's third equation, as follows:

$$\begin{aligned} \mathbf{k}^{(t)} \times \mathbf{E}_{so}^{(t)} = \omega\mu_0 \mathbf{H}_{so}^{(t)} &\rightarrow (\omega/c) [\sin \theta \hat{\mathbf{x}} + \sqrt{n^2(\omega) - \sin^2 \theta} \hat{\mathbf{z}}] \times E_{so}^{(t)} \hat{\mathbf{y}} = \omega\mu_0 \mathbf{H}_{so}^{(t)} \\ &\rightarrow \mathbf{H}_{so}^{(t)} = -(E_{so}^{(t)} / Z_0) [\sqrt{n^2(\omega) - \sin^2 \theta} \hat{\mathbf{x}} - \sin \theta \hat{\mathbf{z}}]. \end{aligned} \quad (10)$$

b) Continuity of the tangential  $E$ -field is already assured by means of Eq.(9). The only remaining constraint involves the tangential  $H$ -field, whose continuity equation is written

$$H_x^{(i)} + H_x^{(r)} = H_x^{(t)} \rightarrow -(E_{so}^{(i)} / Z_0) \cos \theta + (E_{so}^{(r)} / Z_0) \cos \theta = -(E_{so}^{(t)} / Z_0) \sqrt{n^2(\omega) - \sin^2 \theta}. \quad (11)$$

The Fresnel reflection and transmission coefficients, defined as  $\rho_s = E_{so}^{(r)} / E_{so}^{(i)}$  and  $\tau_s = E_{so}^{(t)} / E_{so}^{(i)}$ , may now be used in conjunction with Eqs.(9) and (11) to yield

$$-E_{so}^{(i)} \cos \theta + \rho_s E_{so}^{(i)} \cos \theta = -(1 + \rho_s) E_{so}^{(i)} \sqrt{n^2(\omega) - \sin^2 \theta}. \quad (12)$$

Solving the above equation for  $\rho_s$ , we find

$$\rho_s = \frac{\cos \theta - \sqrt{n^2(\omega) - \sin^2 \theta}}{\cos \theta + \sqrt{n^2(\omega) - \sin^2 \theta}}. \quad (13)$$

From Eq.(9) and the definitions of the Fresnel coefficients, it is obvious that  $\tau_s = 1 + \rho_s$ ; therefore,

$$\tau_s = \frac{2 \cos \theta}{\cos \theta + \sqrt{n^2(\omega) - \sin^2 \theta}}. \quad (14)$$

c) The rate-of-flow of energy per unit cross-sectional area per unit time for each of the three plane-waves is given by the corresponding time-averaged Poynting vector, as follows:

$$\begin{aligned} \langle \mathbf{S}^{(i)}(\mathbf{r}, t) \rangle &= \frac{1}{2} \text{Re}[\mathbf{E}_{so}^{(i)} \times \mathbf{H}_{so}^{(i)*}] = -\frac{1}{2} \text{Re} [E_{so}^{(i)} \hat{\mathbf{y}} \times (E_{so}^{(i)*} / Z_o) (\cos \theta \hat{\mathbf{x}} - \sin \theta \hat{\mathbf{z}})] \\ &= \frac{|E_{so}^{(i)}|^2}{2Z_o} (\sin \theta \hat{\mathbf{x}} + \cos \theta \hat{\mathbf{z}}). \end{aligned} \quad (15)$$

$$\begin{aligned} \langle \mathbf{S}^{(r)}(\mathbf{r}, t) \rangle &= \frac{1}{2} \text{Re}[\mathbf{E}_{so}^{(r)} \times \mathbf{H}_{so}^{(r)*}] = \frac{1}{2} \text{Re} [E_{so}^{(r)} \hat{\mathbf{y}} \times (E_{so}^{(r)*} / Z_o) (\cos \theta \hat{\mathbf{x}} + \sin \theta \hat{\mathbf{z}})] \\ &= \frac{|E_{so}^{(r)}|^2}{2Z_o} (\sin \theta \hat{\mathbf{x}} - \cos \theta \hat{\mathbf{z}}) = |\rho_s|^2 \frac{|E_{so}^{(i)}|^2}{2Z_o} (\sin \theta \hat{\mathbf{x}} - \cos \theta \hat{\mathbf{z}}). \end{aligned} \quad (16)$$

$$\begin{aligned} \langle \mathbf{S}^{(t)}(\mathbf{r}, t) \rangle &= \frac{1}{2} \text{Re}[\mathbf{E}_{so}^{(t)} \times \mathbf{H}_{so}^{(t)*}] = -\frac{1}{2} \text{Re} [E_{so}^{(t)} \hat{\mathbf{y}} \times (E_{so}^{(t)*} / Z_o) [\sqrt{n^2(\omega) - \sin^2 \theta} \hat{\mathbf{x}} - \sin \theta \hat{\mathbf{z}}]] \\ &= \frac{|E_{so}^{(t)}|^2}{2Z_o} [\sin \theta \hat{\mathbf{x}} + \sqrt{n^2(\omega) - \sin^2 \theta} \hat{\mathbf{z}}] \\ &= |\tau_s|^2 \frac{n(\omega) |E_{so}^{(i)}|^2}{2Z_o} (\sin \theta' \hat{\mathbf{x}} + \cos \theta' \hat{\mathbf{z}}). \end{aligned} \quad (17)$$

To verify the conservation of energy, consider an incident beam whose cross-sectional diameter in the  $xz$ -plane is  $D$ . The footprint of this beam on the  $x$ -axis will then be  $D/\cos \theta$ , resulting in a transmitted beam whose cross-sectional diameter in the  $xz$ -plane is  $D(\cos \theta'/\cos \theta)$ . Considering the various Poynting vectors in Eqs.(15)-(17), and the fact that the reflected beam diameter in the  $xz$ -plane remains equal to  $D$ , we must show that the following identity holds:

$$|\rho_s|^2 + (\cos \theta'/\cos \theta) n(\omega) |\tau_s|^2 = 1. \quad (18)$$

Substitution from Eqs.(13) and (14) into Eq.(18), and noting that  $n(\omega) \cos \theta' = \sqrt{n^2(\omega) - \sin^2 \theta}$ , then yields

$$\frac{[\cos \theta - \sqrt{n^2(\omega) - \sin^2 \theta}]^2}{[\cos \theta + \sqrt{n^2(\omega) - \sin^2 \theta}]^2} + \frac{[\sqrt{n^2(\omega) - \sin^2 \theta} / \cos \theta] (2 \cos \theta)^2}{[\cos \theta + \sqrt{n^2(\omega) - \sin^2 \theta}]^2} = 1. \quad (19)$$

The energy fluxes of the reflected and transmitted beams thus add up to that of the incident beam, proving that electromagnetic energy in the present problem is conserved.