## **Problem 7.65**)

a) 
$$
\rho_{12} = (n_1 - n_2)/(n_1 + n_2),
$$
  
\n $\rho_{21} = (n_2 - n_1)/(n_2 + n_1) = -\rho_{12},$   
\n $\rho_{23} = (n_2 - n_3)/(n_2 + n_3) = (n_2 - n - i\kappa)/(n_2 + n + i\kappa),$   
\n $\tau_{23} = 2n_2/(n_2 + n_3).$   
\n $\tau_{23} = 2n_2/(n_2 + n_3).$ 

b) Immediately beneath the entrance facet,  $E_0^{(a)}$  receives a contribution from  $E_0^{(i)}$  via the transmission coefficient  $\tau_{12}$ . A second contribution comes from  $E_0^{(b)}$  upon reflection at the upper dielectric surface (reflection coefficient =  $\rho_{21}$ ). However,  $E_0^{(b)}$  itself is obtained from  $E_0^{(a)}$  after a downward propagation through the thickness  $d$ , reflection at the substrate interface (reflection coefficient =  $\rho_{23}$ ), and an upward propagation, again through the thickness d. The selfconsistency equation for  $E_0^{(a)}$  may thus be written as follows:

$$
E_0^{(a)} = \tau_{12} E_0^{(i)} + \rho_{21} \rho_{23} \exp(2i n_2 k_0 d) E_0^{(a)} \rightarrow E_0^{(a)} = \frac{\tau_{12}}{1 - \rho_{21} \rho_{23} \exp(i 4 \pi n_2 d / \lambda_0)} E_0^{(i)}.
$$

c) The E-field amplitude transmitted into the substrate is obtained by propagating  $E_0^{(a)}$ downward through the thickness d, then multiplying by  $\tau_{23}$  to account for transmission from immediately above to immediately below the dielectric-substrate interface. We will have

$$
E_0^{(t)} = \tau_{23} \exp(i n_2 k_0 d) E_0^{(a)} = \frac{\tau_{12} \tau_{23} \exp(i 2 \pi n_2 d / \lambda_0)}{1 - \rho_{21} \rho_{23} \exp(i 4 \pi n_2 d / \lambda_0)} E_0^{(i)}.
$$

d) The reflected  $E$ -field amplitude at the top of the dielectric layer has two contributions. The first comes from direct reflection from the top facet of the incident amplitude  $E_0^{(i)}$ . The second contribution comes from  $E_0^{(b)}$  after multiplication by  $\tau_{21}$ . However,  $E_0^{(b)}$  itself arises from the propagation of  $E_0^{(a)}$  downward through the thickness d, reflection at the substrate interface, then upward propagation through the thickness  $d$  of the dielectric layer. We will have

$$
E_0^{(r)} = \rho_{12} E_0^{(i)} + \tau_{21} \rho_{23} \exp(2i n_2 k_0 d) E_0^{(a)}
$$
  
= 
$$
\left[ \rho_{12} + \frac{\tau_{12} \tau_{21} \rho_{23} \exp(2i n_2 k_0 d)}{1 - \rho_{21} \rho_{23} \exp(2i n_2 k_0 d)} \right] E_0^{(i)} = \left[ \frac{\rho_{12} + (\tau_{12} \tau_{21} - \rho_{12} \rho_{21}) \rho_{23} \exp(2i n_2 k_0 d)}{1 - \rho_{21} \rho_{23} \exp(2i n_2 k_0 d)} \right] E_0^{(i)}.
$$

Now, using the expressions for  $\rho_{12}$ ,  $\tau_{12}$ ,  $\rho_{21}$ ,  $\tau_{21}$  obtained in part (a), we write

$$
\tau_{12}\tau_{21} - \rho_{12}\rho_{21} = \frac{4n_1n_2}{(n_1+n_2)^2} + \frac{(n_1-n_2)^2}{(n_1+n_2)^2} = 1.0
$$

Consequently,

$$
E_0^{(r)} = \frac{\rho_{12} + \rho_{23} \exp(i4\pi n_2 d/\lambda_0)}{1 + \rho_{12}\rho_{23} \exp(i4\pi n_2 d/\lambda_0)} E_0^{(i)}.
$$

For a given refractive index  $n_2$ , the thickness  $d$  of the dielectric layer can be adjusted to control the reflectance of the bare substrate.

e) When  $d = m\lambda_0/(2n_2)$ , the phase-factor  $exp(i4\pi n_2 d/\lambda_0)$  appearing in the preceding equation becomes equal to 1.0. We will then have

$$
E_0^{(r)}/E_0^{(i)} = \frac{\rho_{12} + \rho_{23}}{1 + \rho_{12}\rho_{23}} = \frac{\left(\frac{n_1 - n_2}{n_1 + n_2}\right) + \left(\frac{n_2 - n_3}{n_2 + n_3}\right)}{1 + \left(\frac{n_1 - n_2}{n_1 + n_2}\right)\left(\frac{n_2 - n_3}{n_2 + n_3}\right)} = \frac{(n_1 - n_2)(n_2 + n_3) + (n_2 - n_3)(n_1 + n_2)}{(n_1 + n_2)(n_2 + n_3) + (n_1 - n_2)(n_2 - n_3)}
$$
  
=  $\frac{n_1 n_2 + n_1 n_3 - n_2^2 - n_2 n_3 + n_1 n_2 + n_2^2 - n_1 n_3 - n_2 n_3}{n_1 n_2 + n_1 n_3 + n_2^2 + n_2 n_3 + n_1 n_2 - n_1 n_3 - n_2^2 + n_2 n_3} = \frac{2n_1 n_2 - 2n_2 n_3}{2n_1 n_2 + 2n_2 n_3} = \frac{n_1 - n_3}{n_1 + n_3}.$ 

Clearly, the overall reflection coefficient  $E_0^{(r)}/E_0^{(i)}$  in this case is independent of  $n_2$ , having the value it would have if the beam was directly incident from free space onto the substrate.