Problem 7.65)

a)
$$\rho_{12} = (n_1 - n_2)/(n_1 + n_2),$$

 $\tau_{12} = 2n_1/(n_1 + n_2).$
 $\rho_{21} = (n_2 - n_1)/(n_2 + n_1) = -\rho_{12},$
 $\tau_{21} = 2n_2/(n_2 + n_1).$
 $\tau_{23} = (n_2 - n_3)/(n_2 + n_3) = (n_2 - n - i\kappa)/(n_2 + n + i\kappa),$
 $\tau_{23} = 2n_2/(n_2 + n_3).$

b) Immediately beneath the entrance facet, $E_0^{(a)}$ receives a contribution from $E_0^{(i)}$ via the transmission coefficient τ_{12} . A second contribution comes from $E_0^{(b)}$ upon reflection at the upper dielectric surface (reflection coefficient = ρ_{21}). However, $E_0^{(b)}$ itself is obtained from $E_0^{(a)}$ after a downward propagation through the thickness *d*, reflection at the substrate interface (reflection coefficient = ρ_{23}), and an upward propagation, again through the thickness *d*. The self-consistency equation for $E_0^{(a)}$ may thus be written as follows:

$$E_0^{(a)} = \tau_{12} E_0^{(i)} + \rho_{21} \rho_{23} \exp(2in_2 k_0 d) E_0^{(a)} \rightarrow E_0^{(a)} = \frac{\tau_{12}}{1 - \rho_{21} \rho_{23} \exp(i4\pi n_2 d/\lambda_0)} E_0^{(i)}$$

c) The *E*-field amplitude transmitted into the substrate is obtained by propagating $E_0^{(a)}$ downward through the thickness *d*, then multiplying by τ_{23} to account for transmission from immediately above to immediately below the dielectric-substrate interface. We will have

$$E_0^{(t)} = \tau_{23} \exp(in_2 k_0 d) E_0^{(a)} = \frac{\tau_{12} \tau_{23} \exp(i2\pi n_2 d/\lambda_0)}{1 - \rho_{21} \rho_{23} \exp(i4\pi n_2 d/\lambda_0)} E_0^{(i)}.$$

d) The reflected *E*-field amplitude at the top of the dielectric layer has two contributions. The first comes from direct reflection from the top facet of the incident amplitude $E_0^{(i)}$. The second contribution comes from $E_0^{(b)}$ after multiplication by τ_{21} . However, $E_0^{(b)}$ itself arises from the propagation of $E_0^{(a)}$ downward through the thickness *d*, reflection at the substrate interface, then upward propagation through the thickness *d* of the dielectric layer. We will have

$$E_0^{(\mathbf{r})} = \rho_{12} E_0^{(\mathbf{i})} + \tau_{21} \rho_{23} \exp(2in_2 k_0 d) E_0^{(\mathbf{a})}$$

= $\left[\rho_{12} + \frac{\tau_{12} \tau_{21} \rho_{23} \exp(2in_2 k_0 d)}{1 - \rho_{21} \rho_{23} \exp(2in_2 k_0 d)} \right] E_0^{(\mathbf{i})} = \left[\frac{\rho_{12} + (\tau_{12} \tau_{21} - \rho_{12} \rho_{21}) \rho_{23} \exp(2in_2 k_0 d)}{1 - \rho_{21} \rho_{23} \exp(2in_2 k_0 d)} \right] E_0^{(\mathbf{i})}.$

Now, using the expressions for ρ_{12} , τ_{12} , ρ_{21} , τ_{21} obtained in part (a), we write

$$\tau_{12}\tau_{21} - \rho_{12}\rho_{21} = \frac{4n_1n_2}{(n_1 + n_2)^2} + \frac{(n_1 - n_2)^2}{(n_1 + n_2)^2} = 1.0$$

Consequently,

$$E_0^{(\mathbf{r})} = \frac{\rho_{12} + \rho_{23} \exp(i4\pi n_2 d/\lambda_0)}{1 + \rho_{12}\rho_{23} \exp(i4\pi n_2 d/\lambda_0)} E_0^{(\mathbf{i})}.$$

For a given refractive index n_2 , the thickness d of the dielectric layer can be adjusted to control the reflectance of the bare substrate.

e) When $d = m\lambda_0/(2n_2)$, the phase-factor $\exp(i4\pi n_2 d/\lambda_0)$ appearing in the preceding equation becomes equal to 1.0. We will then have

$$E_0^{(\mathbf{r})}/E_0^{(\mathbf{i})} = \frac{\rho_{12} + \rho_{23}}{1 + \rho_{12}\rho_{23}} = \frac{\left(\frac{n_1 - n_2}{n_1 + n_2}\right) + \left(\frac{n_2 - n_3}{n_2 + n_3}\right)}{1 + \left(\frac{n_1 - n_2}{n_1 + n_2}\right)\left(\frac{n_2 - n_3}{n_2 + n_3}\right)} = \frac{(n_1 - n_2)(n_2 + n_3) + (n_2 - n_3)(n_1 + n_2)}{(n_1 + n_2)(n_2 + n_3) + (n_1 - n_2)(n_2 - n_3)}$$
$$= \frac{n_1 n_2 + n_1 n_3 - n_2^2 - n_2 n_3 + n_1 n_2 + n_2^2 - n_1 n_3 - n_2 n_3}{n_1 n_2 + n_1 n_3 + n_2^2 + n_2 n_3 + n_1 n_2 - n_1 n_3 - n_2^2 + n_2 n_3} = \frac{2n_1 n_2 - 2n_2 n_3}{2n_1 n_2 + 2n_2 n_3} = \frac{n_1 - n_3}{n_1 + n_3}.$$

Clearly, the overall reflection coefficient $E_0^{(r)}/E_0^{(i)}$ in this case is independent of n_2 , having the value it would have if the beam was directly incident from free space onto the substrate.