

Problem 10) a) The E - and H -fields of the incident plane-wave are given by

$$\mathbf{E}(\mathbf{r}, t) = \mathbf{E}_{so}^{(i)} \exp[i(\mathbf{k}^{(i)} \cdot \mathbf{r} - \omega t)]; \quad (1a)$$

$$\mathbf{H}(\mathbf{r}, t) = \mathbf{H}_{so}^{(i)} \exp[i(\mathbf{k}^{(i)} \cdot \mathbf{r} - \omega t)]. \quad (1b)$$

The dispersion relation in free space is $k^2 = (\omega/c)^2$. Therefore,

$$\mathbf{k}^{(i)} = k_x \hat{\mathbf{x}} + k_z \hat{\mathbf{z}} = (\omega/c)(\sin \theta \hat{\mathbf{x}} + \cos \theta \hat{\mathbf{z}}). \quad (2)$$

The incident E -field amplitude, as shown in the figure, is given by

$$\mathbf{E}_{so}^{(i)} = E_{so}^{(i)} \hat{\mathbf{y}}. \quad (3)$$

It may be readily verified that this E -field satisfies Maxwell's first equation, namely, $\nabla \cdot \mathbf{E} = 0$, which is equivalent to $\mathbf{k}^{(i)} \cdot \mathbf{E}_{so}^{(i)} = 0$. As for the incident H -field, Maxwell's third equation, $\nabla \times \mathbf{E} = -\partial \mathbf{B} / \partial t$, yields

$$\begin{aligned} i\mathbf{k}^{(i)} \times \mathbf{E}_{so}^{(i)} &= i\omega\mu_0 \mathbf{H}_{so}^{(i)} \rightarrow (\omega/c)(\sin \theta \hat{\mathbf{x}} + \cos \theta \hat{\mathbf{z}}) \times E_{so}^{(i)} \hat{\mathbf{y}} = \omega\mu_0 \mathbf{H}_{so}^{(i)} \\ &\rightarrow \mathbf{H}_{so}^{(i)} = -(E_{so}^{(i)} / Z_0)(\cos \theta \hat{\mathbf{x}} - \sin \theta \hat{\mathbf{z}}). \end{aligned} \quad (4)$$

A similar treatment yields for the reflected plane-wave,

$$\mathbf{k}^{(r)} = k_x \hat{\mathbf{x}} - k_z \hat{\mathbf{z}} = (\omega/c)(\sin \theta \hat{\mathbf{x}} - \cos \theta \hat{\mathbf{z}}), \quad (5)$$

$$\mathbf{E}_{so}^{(r)} = E_{so}^{(r)} \hat{\mathbf{y}}, \quad (6)$$

$$\mathbf{H}_{so}^{(r)} = (E_{so}^{(r)} / Z_0)(\cos \theta \hat{\mathbf{x}} + \sin \theta \hat{\mathbf{z}}). \quad (7)$$

As for the transmitted beam, the dispersion relation in the dielectric medium is $k^2 = (\omega/c)^2 n^2(\omega)$; also, in accordance with Snell's law, we must have $k_x^{(t)} = k_x^{(i)}$ and $k_y^{(t)} = k_y^{(i)} = 0$. Therefore,

$$\mathbf{k}^{(t)} = k_x^{(i)} \hat{\mathbf{x}} + k_z^{(t)} \hat{\mathbf{z}} = (\omega/c) [\sin \theta \hat{\mathbf{x}} + \sqrt{n^2(\omega) - \sin^2 \theta} \hat{\mathbf{z}}]. \quad (8)$$

Next, we obtain the transmitted E -field using the continuity of tangential \mathbf{E} at the interface:

$$\mathbf{E}_{so}^{(t)} = (E_{so}^{(i)} + E_{so}^{(r)}) \hat{\mathbf{y}}. \quad (9)$$

Subsequently, the transmitted H -field is obtained from Maxwell's third equation, as follows:

$$\begin{aligned} \mathbf{k}^{(t)} \times \mathbf{E}_{so}^{(t)} &= \omega\mu_0 \mathbf{H}_{so}^{(t)} \rightarrow (\omega/c) [\sin \theta \hat{\mathbf{x}} + \sqrt{n^2(\omega) - \sin^2 \theta} \hat{\mathbf{z}}] \times E_{so}^{(t)} \hat{\mathbf{y}} = \omega\mu_0 \mathbf{H}_{so}^{(t)} \\ &\rightarrow \mathbf{H}_{so}^{(t)} = -(E_{so}^{(t)} / Z_0) [\sqrt{n^2(\omega) - \sin^2 \theta} \hat{\mathbf{x}} - \sin \theta \hat{\mathbf{z}}]. \end{aligned} \quad (10)$$

b) Continuity of the tangential E -field is already assured by means of Eq.(9). The only remaining constraint involves the tangential H -field, whose continuity equation is written

$$\mathbf{H}_x^{(i)} + \mathbf{H}_x^{(r)} = \mathbf{H}_x^{(t)} \rightarrow -(E_{so}^{(i)} / Z_0) \cos \theta + (E_{so}^{(r)} / Z_0) \cos \theta = -(E_{so}^{(t)} / Z_0) \sqrt{n^2(\omega) - \sin^2 \theta}. \quad (11)$$

The Fresnel reflection and transmission coefficients, defined as $\rho_s = E_{so}^{(r)} / E_{so}^{(i)}$ and $\tau_s = E_{so}^{(t)} / E_{so}^{(i)}$, may now be used in conjunction with Eqs.(9) and (11) to yield

$$-E_{so}^{(i)} \cos \theta + \rho_s E_{so}^{(i)} \cos \theta = -(1 + \rho_s) E_{so}^{(i)} \sqrt{n^2(\omega) - \sin^2 \theta}. \quad (12)$$

Solving the above equation for ρ_s , we find

$$\rho_s = \frac{\cos \theta - \sqrt{n^2(\omega) - \sin^2 \theta}}{\cos \theta + \sqrt{n^2(\omega) - \sin^2 \theta}}. \quad (13)$$

From Eq.(9) and the definitions of the Fresnel coefficients, it is obvious that $\tau_s = 1 + \rho_s$; therefore,

$$\tau_s = \frac{2 \cos \theta}{\cos \theta + \sqrt{n^2(\omega) - \sin^2 \theta}}. \quad (14)$$

c) The rate-of-flow of energy per unit cross-sectional area per unit time for each of the three plane-waves is given by the corresponding time-averaged Poynting vector, as follows:

$$\begin{aligned} \langle \mathbf{S}^{(i)}(\mathbf{r}, t) \rangle &= \frac{1}{2} \text{Re}[\mathbf{E}_{so}^{(i)} \times \mathbf{H}_{so}^{(i)*}] = -\frac{1}{2} \text{Re}[E_{so}^{(i)} \hat{\mathbf{y}} \times (E_{so}^{(i)*} / Z_o)(\cos \theta \hat{\mathbf{x}} - \sin \theta \hat{\mathbf{z}})] \\ &= \frac{|E_{so}^{(i)}|^2}{2Z_o} (\sin \theta \hat{\mathbf{x}} + \cos \theta \hat{\mathbf{z}}). \end{aligned} \quad (15)$$

$$\begin{aligned} \langle \mathbf{S}^{(r)}(\mathbf{r}, t) \rangle &= \frac{1}{2} \text{Re}[\mathbf{E}_{so}^{(r)} \times \mathbf{H}_{so}^{(r)*}] = \frac{1}{2} \text{Re}[E_{so}^{(r)} \hat{\mathbf{y}} \times (E_{so}^{(r)*} / Z_o)(\cos \theta \hat{\mathbf{x}} + \sin \theta \hat{\mathbf{z}})] \\ &= \frac{|E_{so}^{(r)}|^2}{2Z_o} (\sin \theta \hat{\mathbf{x}} - \cos \theta \hat{\mathbf{z}}) = |\rho_s|^2 \frac{|E_{so}^{(i)}|^2}{2Z_o} (\sin \theta \hat{\mathbf{x}} - \cos \theta \hat{\mathbf{z}}). \end{aligned} \quad (16)$$

$$\begin{aligned} \langle \mathbf{S}^{(t)}(\mathbf{r}, t) \rangle &= \frac{1}{2} \text{Re}[\mathbf{E}_{so}^{(t)} \times \mathbf{H}_{so}^{(t)*}] = -\frac{1}{2} \text{Re}[E_{so}^{(t)} \hat{\mathbf{y}} \times (E_{so}^{(t)*} / Z_o)[\sqrt{n^2(\omega) - \sin^2 \theta} \hat{\mathbf{x}} - \sin \theta \hat{\mathbf{z}}]] \\ &= \frac{|E_{so}^{(t)}|^2}{2Z_o} [\sin \theta \hat{\mathbf{x}} + \sqrt{n^2(\omega) - \sin^2 \theta} \hat{\mathbf{z}}] \\ &= |\tau_s|^2 \frac{n(\omega) |E_{so}^{(i)}|^2}{2Z_o} (\sin \theta' \hat{\mathbf{x}} + \cos \theta' \hat{\mathbf{z}}). \end{aligned} \quad (17)$$

To verify the conservation of energy, consider an incident beam whose cross-sectional diameter in the xz -plane is D . The footprint of this beam on the x -axis will then be $D/\cos \theta$, resulting in a transmitted beam whose cross-sectional diameter in the xz -plane is $D(\cos \theta'/\cos \theta)$. Considering the various Poynting vectors in Eqs.(15)-(17), and the fact that the reflected beam diameter in the xz -plane remains equal to D , we must show that the following identity holds:

$$|\rho_s|^2 + (\cos \theta'/\cos \theta) n(\omega) |\tau_s|^2 = 1. \quad (18)$$

Substitution from Eqs.(13) and (14) into Eq.(18), and noting that $n(\omega) \cos \theta' = \sqrt{n^2(\omega) - \sin^2 \theta}$, then yields

$$\frac{[\cos \theta - \sqrt{n^2(\omega) - \sin^2 \theta}]^2}{[\cos \theta + \sqrt{n^2(\omega) - \sin^2 \theta}]^2} + \frac{[\sqrt{n^2(\omega) - \sin^2 \theta} / \cos \theta] (2 \cos \theta)^2}{[\cos \theta + \sqrt{n^2(\omega) - \sin^2 \theta}]^2} = 1. \quad (19)$$

The energy fluxes of the reflected and transmitted beams thus add up to that of the incident beam, proving that electromagnetic energy in the present problem is conserved.