

## Problem 36)

a)  $\vec{J} \times \vec{H} = \vec{J} \Rightarrow \oint \vec{H} \cdot d\vec{l} = \int \vec{J} \cdot d\vec{s} \Rightarrow 2\pi r H_\phi = \begin{cases} (\rho/r^2) I_0 & r \leq R \\ I_0 & r > R \end{cases}$

$$\Rightarrow \vec{H}(r, \phi, z) = \begin{cases} \frac{\rho I_0}{2\pi R^2} \hat{\phi} & r \leq R \\ \left[ \frac{I_0}{(2\pi\rho)} \right] \hat{\phi} & r \geq R \end{cases}$$

b) Inside the rod, the  $\vec{E}$ -field is uniform ( $E = E_0 \hat{z}$ ). Therefore, its curl and divergence must be zero. Outside the rod, we have

$$\vec{D} \times \vec{E} = \left( \frac{\partial E_p}{\partial z} - \frac{\partial E_z}{\partial p} \right) \hat{\phi} = E_0 \left\{ \frac{-1}{p \ln(R_0/R)} + \frac{1/p}{\ln(R_0/R)} \right\} \hat{\phi} = 0.$$

Also note that at  $p=R$  we have  $E_z(R, \phi, z) = E_0$  on both sides of the cylinder surface; in other words,  $E_z$  is continuous at the surface of the cylindrical rod. The fact that  $\vec{D} \times \vec{E} = 0$  throughout the entire space ( $0 \leq z \leq L, 0 \leq p \leq R_0$ ) indicates that a potential function  $\psi(p, \phi, z)$  can be specified (with the relevant space) in this static problem, as it should. Finally,  $\vec{D} \cdot \vec{E}$  outside the rod is given by

$$\vec{D} \cdot \vec{E} = \frac{1}{p} \frac{\partial}{\partial p} (p E_p) + \frac{\partial E_z}{\partial z} = E_0 \left\{ \frac{1}{p} \frac{\partial}{\partial p} \left[ \frac{L-z}{\ln(R_0/R)} \right] + \frac{\partial}{\partial z} \left[ 1 - \frac{\ln(p/R)}{\ln(R_0/R)} \right] \right\} = 0 \checkmark$$

c) The  $\vec{E}$ -field perpendicular to the cylinder surface,  $E_p$ , is discontinuous.

$$\text{Therefore, } \sigma_s(p=R, \phi, z) = \epsilon_0 [E_p(p=R, \phi, z) - E_p(p=\bar{R}, \phi, z)] = \frac{\epsilon_0 E_0}{R \ln(R_0/R)} \frac{L-z}{R}$$

Note that the charge density is strong at  $z=0$ , decreasing linearly with  $z$ , until it drops to zero at  $z=L$ . To get a feel for the numbers involved, suppose  $E_0 = 1000 \text{ V/m}$ ,  $L = 1 \text{ km}$ ,  $R = 1 \text{ mm}$ ,  $R_0 = 1 \text{ m}$ ,  $z=0$ . We find (using  $\epsilon_0 = 8.854 \times 10^{-12} \text{ F/m}$ ) that  $\sigma_s(p=R, \phi, z=0) = 1.3 \times 10^{-3} \text{ Coulomb/m}^2$ .

Compare this with the charge density at the cylinder surface if only one

atomic layer had been left "naked," i.e., without electrons. A single atom typically is about  $1\text{ \AA} = 10^{-10}\text{ m}$  in diameter; therefore, a square meter of the surface area contains about  $10^{20}$  atoms. Multiply this with the electronic charge of  $e = 1.6 \times 10^{-19}\text{ C}$ , and you get  $\sigma_s \approx 16 \text{ C/m}^2$ , which is 4 orders of magnitude greater than  $\sigma_s$  in the present problem.

The surface charge distribution on the cylindrical rod is responsible for creating the field  $\vec{E} = E_0 \hat{z}$  inside the conductor. The linear decrease of  $\sigma_s$  with  $z$  allows for the uniform  $\vec{E}$ -field inside the rod to be directed along the  $z$ -axis. Note that the voltage drop along the length of the conductor is  $E_0 L$ , which is equal to the initial voltage at  $z=0$ ,

$$\text{given by } V_0 = \int_{P=R}^{R_0} E_p(P, \phi, z=0) dP = \frac{E_0 L}{\ln(R_0/R)} \int_R^{R_0} \frac{dP}{P} = E_0 L \quad \checkmark$$

d)  $\vec{S} = \vec{E} \times \vec{H}$

outside the rod  $\vec{S} = E_0 \left\{ \frac{L-z}{\rho \ln(R_0/R)} \hat{\rho} + \left[ 1 - \frac{\ln(\rho/R)}{\ln(R_0/R)} \right] \hat{z} \right\} \times \frac{I_0}{2\pi\rho} \hat{\phi}$

$$\Rightarrow \vec{S}(P, \phi, z) = E_0 I_0 \underbrace{\frac{L-z}{2\pi\rho^2 \ln(R_0/R)} \hat{z}}_{\vec{S}_z} - \frac{E_0 I_0}{2\pi\rho} \left[ 1 - \frac{\ln(P/R)}{\ln(R_0/R)} \right] \hat{\rho}$$

The energy enters the system at  $z=0$ , through the  $z$ -component of the Poynting Vector,  $S_z(P, \phi, z=0) = \frac{E_0 I_0 L}{2\pi\rho^2 \ln(R_0/R)}$ :

$$\int_{P=R}^{R_0} \frac{E_0 I_0 L}{2\pi\rho^2 \ln(R_0/R)} 2\pi\rho dP = E_0 I_0 L = V_0 I_0 \quad \checkmark$$

No energy enters the system along the radial direction, because at  $P=R_0$  the radial component of the  $\vec{S}$ -field is zero:

$$S_\rho(P=R_0, \phi, z) = - \frac{E_0 I_0}{2\pi\rho} \left[ 1 - \frac{\ln(R_0/R)}{\ln(R_0/R)} \right] = 0 \quad \checkmark$$

However, at other points along the  $\rho$ -direction,  $S_p$  is non-zero and points toward the rod. The integral of  $S_p$  around a cylinder of radius  $\rho$  and unit length is thus given by:

$$\int_{\phi=0}^{2\pi} \int_{z=z_0}^{z_0+1} S_p(\rho, \phi, z) \rho d\phi dz = -E_o I_o \left[ 1 - \frac{\ln(\rho/R)}{\ln(R_0/R)} \right].$$

The energy entering the system along the  $z$ -axis is thus seen to turn toward the rod (i.e., in the  $\rho$ -direction) at a rate that is independent of  $z$ , but increases as  $\rho$  moves from  $R_0$  to  $R$ . At  $\rho = R$ , i.e., at the cylinder surface, the energy enters the cylinder at a rate of  $E_o I_o$  per unit length per second. By the time it gets to  $z = L$ , all the energy has gone into the rod (and converted into heat); that is why  $S_z(\rho, \phi, z=L) = 0$ , i.e., no energy leaves the system at  $z=L$  along the  $z$ -axis.

Inside the rod  $\vec{S} = E_o \hat{z} \times \frac{\rho I_o}{2\pi R^2} \hat{\phi} = -\frac{E_o I_o \rho}{2\pi R^2} \hat{P}$

$$\int_{\phi=0}^{2\pi} \int_{z=z_0}^{z_0+1} S_p(\rho, \phi, z) \rho d\phi dz = -E_o I_o (\rho/R)^2$$

The energy thus enters the rod <sup>radially</sup> at the surface, at a rate of  $E_o I_o$  per unit length per second. It is deposited (in the form of heat) as it moves toward the center, until it reaches zero at  $\rho=0$ . Note that no energy enters from the bottom of the rod at  $z=0$ ; all energy flows in radially from the air outside the rod.