

Problem 2-31)

a) $Q = CV$, where $C = \epsilon_0 A/d$ is the capacitance. (A is the area of each capacitor plate.) We have

$$dQ/dt = C dV/dt \rightarrow dV/dt = (I_0/C) \sin(2\pi ft) \rightarrow V(t) = -(I_0/2\pi f C) \cos(2\pi ft).$$

Considering that $V(t)$ is the integral of E_z across the gap and that, to a first approximation, E_z is a uniform function of ρ and z , we write

$$\mathbf{E}(\rho, t) = \left(\frac{I_0}{2\pi f C d}\right) \cos(2\pi ft) \hat{\mathbf{z}} \rightarrow \mathbf{E}(\rho, t) = \left(\frac{I_0}{\epsilon_0 A}\right) \left(\frac{1}{2\pi f}\right) \cos(2\pi ft) \hat{\mathbf{z}}.$$

b) $\nabla \times \mathbf{H} = \mathbf{J}_{\text{free}} + \partial_t \mathbf{D}$. Since there is no \mathbf{J}_{free} in the gap between the plates, we will have

$$\nabla \times [H_\phi(\rho, t) \hat{\boldsymbol{\phi}}] = -(I_0/A) \sin(2\pi ft) \hat{\mathbf{z}} \rightarrow \frac{1}{\rho} \frac{\partial}{\partial \rho} (\rho H_\phi) \hat{\mathbf{z}} = -(I_0/A) \sin(2\pi ft) \hat{\mathbf{z}}$$

$$\rightarrow \frac{\partial}{\partial \rho} (\rho H_\phi) = -(I_0/A) \rho \sin(2\pi ft) \rightarrow \rho H_\phi(\rho, t) = -(I_0/2A) \rho^2 \sin(2\pi ft)$$

$$\rightarrow \mathbf{H}(\rho, t) = -(I_0/2A) \rho \sin(2\pi ft) \hat{\boldsymbol{\phi}}.$$

c) $\nabla \times \mathbf{E} = -\partial_t \mathbf{B} \rightarrow \nabla \times [E_z(\rho, t) \hat{\mathbf{z}}] = \mu_0 (I_0/2A) \rho (2\pi f) \cos(2\pi ft) \hat{\boldsymbol{\phi}}$

$$\rightarrow -\frac{\partial}{\partial \rho} E_z(\rho, t) \hat{\boldsymbol{\phi}} = \left(\frac{\sqrt{\mu_0/\epsilon_0} I_0}{2Ac}\right) (2\pi f) \rho \cos(2\pi ft) \hat{\boldsymbol{\phi}} \leftarrow c = 1/\sqrt{\mu_0 \epsilon_0}$$

$$\rightarrow \mathbf{E}(\rho, t) = -\left(\frac{\sqrt{\mu_0/\epsilon_0} I_0}{4Ac}\right) (2\pi f) \rho^2 \cos(2\pi ft) \hat{\mathbf{z}}.$$

This term must be added to the zeroth-order approximation to the E -field, derived in part (a).

d) $\nabla \times \mathbf{H} = \partial_t \mathbf{D} \rightarrow \nabla \times [H_\phi(\rho, t) \hat{\boldsymbol{\phi}}] = \epsilon_0 \left(\frac{\sqrt{\mu_0/\epsilon_0} I_0}{4Ac}\right) (2\pi f)^2 \rho^2 \sin(2\pi ft) \hat{\mathbf{z}}$

$$\rightarrow \frac{1}{\rho} \frac{\partial}{\partial \rho} (\rho H_\phi) \hat{\mathbf{z}} = \left(\frac{I_0}{4A}\right) \left(\frac{2\pi f}{c}\right)^2 \rho^2 \sin(2\pi ft) \hat{\mathbf{z}}$$

$$\rightarrow \mathbf{H}(\rho, t) = \left(\frac{I_0}{16A}\right) \left(\frac{2\pi f}{c}\right)^2 \rho^3 \sin(2\pi ft) \hat{\boldsymbol{\phi}}.$$

This term must be added to the first-order approximation to the H -field, obtained in part (b).

e) $\sigma_s(\rho, t) = \pm \epsilon_0 E_z(\rho, t) = \pm \left(\frac{I_0}{A}\right) \left(\frac{1}{2\pi f}\right) \left[1 - \frac{1}{4} \left(\frac{2\pi f}{c}\right)^2 \rho^2\right] \cos(2\pi ft).$

In the above equation, the + sign is for the lower plate, and the - sign for the upper plate.

At the interior facets of the two plates, the surface current-density $\mathbf{J}_s(\rho, t)$ is perpendicular in direction to $\mathbf{H}(\rho, t)$, and equal in magnitude to $|\mathbf{H}(\rho, t)|$. We thus have

$$\mathbf{J}_s(\rho, t) = \pm \left(\frac{I_0}{2A}\right) \rho \left[1 - \frac{1}{8} \left(\frac{2\pi f}{c}\right)^2 \rho^2\right] \sin(2\pi ft) \hat{\boldsymbol{\rho}}.$$

In the above equation, the + sign is for the lower plate, and the - sign for the upper plate.