**Problem 2.19**) a) Using symmetry, it is easy to see that  $H_0$ ,  $H_{\omega}$ , and  $H_z$  must be independent of the  $\varphi$  and z coordinates; these H-field components are functions of  $\rho$  only. In conjunction with Maxwell's 4<sup>th</sup> equation,  $\nabla \cdot \mathbf{B} = 0$ , we use a cylindrical volume centered on the z-axis to show that  $H_{\rho} = 0$ . We then use a circular loop in the *xy*-plane in conjunction with Maxwell's 2<sup>nd</sup> equation,  $\nabla \times H = J_{\text{free}}$ , to demonstrate that  $H_{\varphi} = 0$ . Finally, the use of rectangular loops in the  $\rho$ z-plane, again in conjunction with Maxwell's  $2<sup>nd</sup>$  equation, reveals that

i)  $H<sub>z</sub>$  *inside* the solenoid is uniform;

ii)  $H<sub>z</sub>$  *outside* the solenoid is also uniform;

iii)  $H_z^{\text{(inside)}} - H_z^{\text{(outside)}} = J_{s0}.$ 

Given that a uniform  $H_z$  field residing in the entire space cannot, in any way, be related to the solenoidal current  $J_{s0}\hat{\varphi}$  via Maxwell's equations, we conclude that  $H_z^{(outside)} = 0$ . Therefore,

$$
H(\rho, \varphi, z) = \begin{cases} J_{s0}\hat{z}; & 0 \le \rho < R_1, \\ 0; & \rho > R_1. \end{cases}
$$
 (1)

b) Applying Maxwell's  $1^{st}$  equation (Gauss' law) to a cylindrical surface of radius  $\rho$  and height L centered on the z-axis, we find

$$
\boldsymbol{E}(\rho,\varphi,z) = \begin{cases} (R_2 \sigma_{s0} / \varepsilon_0 \rho) \hat{\boldsymbol{\rho}}; & R_2 < \rho < R_1, \\ 0; & \rho < R_2 \end{cases}
$$
 and also  $\rho > R_1$ . (2)

c) 
$$
\mathbf{S}(\mathbf{r}) = \mathbf{E}(\mathbf{r}) \times \mathbf{H}(\mathbf{r}) = \begin{cases} -(R_2 \sigma_{s0} J_{s0} / \varepsilon_0 \rho) \hat{\boldsymbol{\varphi}}; & R_2 < \rho < R_1, \\ 0; & \rho < R_2 \end{cases}
$$
 and also  $\rho > R_1$ . (3)

Thus, in the free-space region between the cylinders, the electromagnetic energy appears to be circulating at a constant rate in the  $-\hat{\varphi}$  direction.

(d) 
$$
\boldsymbol{\nabla} \cdot \mathbf{S}(\boldsymbol{r}) = \frac{1}{\rho} \frac{\partial S_{\varphi}}{\partial \varphi} = 0.
$$

(**Note**: The above result is consistent with the result obtained in Problem 2.17, as the  $E$ -field of the inner cylinder in the present problem is perpendicular to the current-density  $\mathbf{J}_s$  of the solenoid.)

Application of Gauss' theorem to Eq.(4) now yields  $\oint_{\text{surface}} \mathbf{S} \cdot d\mathbf{s} = \int_{\text{volume}} (\mathbf{\nabla} \cdot \mathbf{S}) d\mathbf{v} = 0$ , where the closed surface of integration may be inside one or both cylinders, or it may cross their boundaries.

e) The electromagnetic angular momentum per unit-length along the z-axis is readily found to be

$$
\mathbf{L} = \int_{\text{volume}} (\rho \hat{\boldsymbol{\rho}}) \times (\mathbf{S}/c^2) \, \mathrm{d}v = -(R_2 \sigma_{s0} \int_{s0} / \varepsilon_0 c^2) \pi (R_1^2 - R_2^2) \hat{\mathbf{z}} \\
= -\mu_0 \pi (R_1^2 - R_2^2) R_2 \sigma_{s0} \int_{s0} \hat{\mathbf{z}}.\n\tag{5}
$$

volume

The above angular momentum is created in the beginning, when the current-density of the solenoid rises from zero to  $J_{s0}\hat{\varphi}$ . During this early phase, say, from  $t = 0$  to  $t = \tau$ , the magnetic field inside the solenoid rises from  $\mathbf{B} = 0$  to  $\mathbf{B} = \mu_0 \int_{S_0} \hat{\mathbf{z}}$ . In accordance with Maxwell's 3<sup>rd</sup> equation,  $\nabla \times \vec{E} = -\partial \vec{B}/\partial t$ , the induced E-field within the solenoid must have been

$$
\mathbf{E}(\rho, t) = -\frac{1}{2}\mu_0 \rho \left(\frac{\partial J_{s0}}{\partial t}\right) \hat{\boldsymbol{\varphi}}.\tag{6}
$$

The above E-field exerts an azimuthal force on the charge-density  $\sigma_{s0}$  of the inner cylinder (radius =  $R_2$ ), as well as on the charge-density  $-(R_2/R_1)\sigma_{s0}$  residing on the inner surface of the solenoid (radius =  $R_1$ ). The net torque (per unit length along z) exerted on the two cylinders is thus given by

$$
\boldsymbol{T}(t) = \int_{z=z_0}^{z_0+1} \int_{\varphi=0}^{2\pi} \{ \left[ R_2 \hat{\boldsymbol{\rho}} \times \sigma_{s0} E_{\varphi}(R_2, t) \hat{\boldsymbol{\varphi}} \right] R_2 d\varphi - \left[ R_1 \hat{\boldsymbol{\rho}} \times (R_2/R_1) \sigma_{s0} E_{\varphi}(R_1, t) \hat{\boldsymbol{\varphi}} \right] R_1 d\varphi \} dz
$$
  
\nInner cylinder  
\n
$$
= -\mu_0 \pi R_2^3 \sigma_{s0} (\partial J_{s0}/\partial t) \hat{\boldsymbol{z}} + \mu_0 \pi R_2 R_1^2 \sigma_{s0} (\partial J_{s0}/\partial t) \hat{\boldsymbol{z}}
$$
  
\n
$$
= \mu_0 \pi (R_1^2 - R_2^2) R_2 \sigma_{s0} (\partial J_{s0}/\partial t) \hat{\boldsymbol{z}}.
$$
\n(7)

Considering that  $T(t) = dL(t)/dt$ , the integral of  $T(t)$  over the time interval  $[0, \tau]$  during which the solenoidal surface-current-density rises from zero to its final value,  $J_{s0}$ , must equal the mechanical angular momentum imparted to the cylinders during the same period of time. Thus,

$$
\int_0^T \boldsymbol{T}(t) \mathrm{d}t = \mu_0 \pi (R_1^2 - R_2^2) R_2 \sigma_{s0} J_{s0} \hat{\boldsymbol{z}}.
$$
 (8)

Conservation of angular momentum then dictates that an equal but opposite angular momentum must reside in the electromagnetic field, in agreement with Eq.(5).