

Multiple Beam Interference

MB - 1

We found for multiple beam interference and no surface absorption, the coefficient of reflectance and transmittance are given by

$$\frac{I_r}{I_i} = \frac{4 R \sin[\delta / 2]^2}{(1 - R)^2 + 4 R \sin[\delta / 2]^2} = \frac{F \sin[\delta / 2]^2}{1 + F \sin[\delta / 2]^2}$$

$$\frac{I_t}{I_i} = \frac{T^2}{(1 - R)^2 + 4 R \sin[\delta / 2]^2} = \frac{1}{1 + F \sin[\delta / 2]^2}$$

How does the coefficient of reflectance change if the first reflected beam is suppressed?

Solution

From the multiple beam interference notes we have

$$E_r = E_i (r + t t' r' e^{i\delta} (1 + r'^2 e^{i\delta} + \dots + r'^{2(p-2)} e^{i(p-2)\delta}))$$

$$E_t = E_i t t' (1 + r'^2 e^{i\delta} + r'^4 e^{i2\delta} + \dots + r'^{2(p-1)} e^{i(p-1)\delta})$$

If the first reflected beam is suppressed

$$E_r = (r' e^{i\delta}) E_t$$

Thus,

$$\frac{I_r}{I_i} = R \frac{I_t}{I_i}$$

So,

$$\frac{I_r}{I_i} = R \left(\frac{1}{1 + F \sin[\delta / 2]^2} \right)$$

Thus, if the first reflected beam is suppressed the reflected beam and the transmitted beam have the same appearance.

MB - 2

The Airy formulas given above for multiple beam interference are for the situation where both surfaces have an intensity reflectance R . What are the formulas for reflectance and transmittance if the first surface has an intensity reflectance R_1 and the second surface has an intensity reflectance R_2 ? There is no absorption at either surface.

Solution

■ Reflected Light

$$E_r = E_i (r_1 + t_1 t_1' r_2' e^{i\delta} (1 + r_1' r_2' e^{i\delta} + \dots + r_1' (r_2')^{p-2} r_2' e^{i(p-2)\delta}))$$

$$E_r = E_i \left(r_1 + t_1 t_1' r_2' e^{i\delta} \sum_{n=0}^{p-2} (r_1')^n (r_2')^n e^{i n \delta} \right)$$

$$E_r = E_i \left(r_1 + t_1 t_1' r_2' e^{i\delta} \left(\frac{1 - r_1' (r_2')^{p-1} r_2' e^{i(p-1)\delta}}{1 - r_1' r_2' e^{i\delta}} \right) \right)$$

Substitute $r_1 = -r_1'$, $r_2 = -r_2'$, and let $p \rightarrow \infty$.

$$E_r = E_i \left(r_1 - \frac{t_1 t_1' r_2 e^{i\delta}}{1 - r_1 r_2 e^{i\delta}} \right)$$

$$E_r = E_i \left(\frac{r_1 - r_1^2 r_2 e^{i\delta} - t_1 t_1' r_2 e^{i\delta}}{1 - r_1 r_2 e^{i\delta}} \right)$$

$$E_r = E_i \left(\frac{r_1 - r_2 e^{i\delta} (r_1^2 + t_1 t_1')}{1 - r_1 r_2 e^{i\delta}} \right)$$

But since there is no absorption $(r_1^2 + t_1 t_1') = 1$. Also let $r_1 = \sqrt{R_1}$ and $r_2 = \sqrt{R_2}$.

$$E_r = E_i \left(\frac{\sqrt{R_1} - \sqrt{R_2} e^{i\delta}}{1 - \sqrt{R_1} \sqrt{R_2} e^{i\delta}} \right)$$

$$I_r = E_r E_r^* = I_i \left(\frac{R_1 + R_2 - 2 \sqrt{R_1 R_2} \cos[\delta]}{1 + R_1 R_2 - 2 \sqrt{R_1 R_2} \cos[\delta]} \right)$$

But $\cos[\delta] = 1 - 2 \sin[\delta/2]^2$

$$\frac{I_r}{I_i} = \frac{R_1 + R_2 - 2 \sqrt{R_1 R_2} + 4 \sqrt{R_1 R_2} \sin[\delta/2]^2}{1 + R_1 R_2 - 2 \sqrt{R_1 R_2} + 4 \sqrt{R_1 R_2} \sin[\delta/2]^2}$$

$$\frac{I_r}{I_i} = \frac{(\sqrt{R_1} - \sqrt{R_2})^2 + 4 \sqrt{R_1 R_2} \sin[\delta/2]^2}{(1 - \sqrt{R_1 R_2})^2 + 4 \sqrt{R_1 R_2} \sin[\delta/2]^2}$$

■ Transmitted Light

$$E_t = E_i t_1 t_2' (1 + r_2' r_1' e^{i\delta} + r_2'^2 r_1'^2 e^{i2\delta} + \dots + r_2'^{(p-1)} r_1'^{(p-1)} e^{i(p-1)\delta})$$

$$E_t = E_i t_1 t_2' \left(\frac{1 - (r_2')^p (r_1')^p e^{ip\delta}}{1 - r_2' r_1' e^{i\delta}} \right)$$

Substitute $r_1 = -r_1'$, $r_2 = -r_2'$, and let $p \rightarrow \infty$.

$$E_t = E_i \frac{t_1 t_2'}{1 - r_2 r_1 e^{i\delta}}$$

Let $t_1 = \sqrt{T_1}$, $t_2' = \sqrt{T_2}$, $r_1 = \sqrt{R_1}$, and $r_2 = \sqrt{R_2}$.

$$E_t = E_i \frac{\sqrt{T_1 T_2}}{1 - \sqrt{R_1 R_2} e^{i\delta}}$$

$$\frac{I_t}{I_i} = \frac{T_1 T_2}{1 + R_1 R_2 - 2 \sqrt{R_1 R_2} \cos[\delta]}$$

But $\cos[\delta] = 1 - 2 \sin[\delta/2]^2$

$$\frac{I_t}{I_i} = \frac{T_1 T_2}{(1 - \sqrt{R_1 R_2})^2 + 4 \sqrt{R_1 R_2} \sin[\delta/2]^2}$$

This can be derived from the Airy formula by replacing T with $\sqrt{T_1 T_2}$ and R with $\sqrt{R_1 R_2}$. This could have been guessed from above because every place we had an r_1' we also had an r_2' and we had $t_1 t_2'$ factored out of the equation.

As a check, derive $\frac{I_r}{I_i}$ from $\frac{I_r}{I_i} + \frac{I_t}{I_i} = 1$.

$$\frac{I_r}{I_i} = 1 - \frac{T_1 T_2}{(1 - \sqrt{R_1 R_2})^2 + 4 \sqrt{R_1 R_2} \sin[\delta/2]^2}$$

$$\frac{I_r}{I_i} = \frac{1 - 2 \sqrt{R_1 R_2} + R_1 R_2 + 4 \sqrt{R_1 R_2} \sin[\delta/2]^2 - T_1 T_2}{(1 - \sqrt{R_1 R_2})^2 + 4 \sqrt{R_1 R_2} \sin[\delta/2]^2}$$

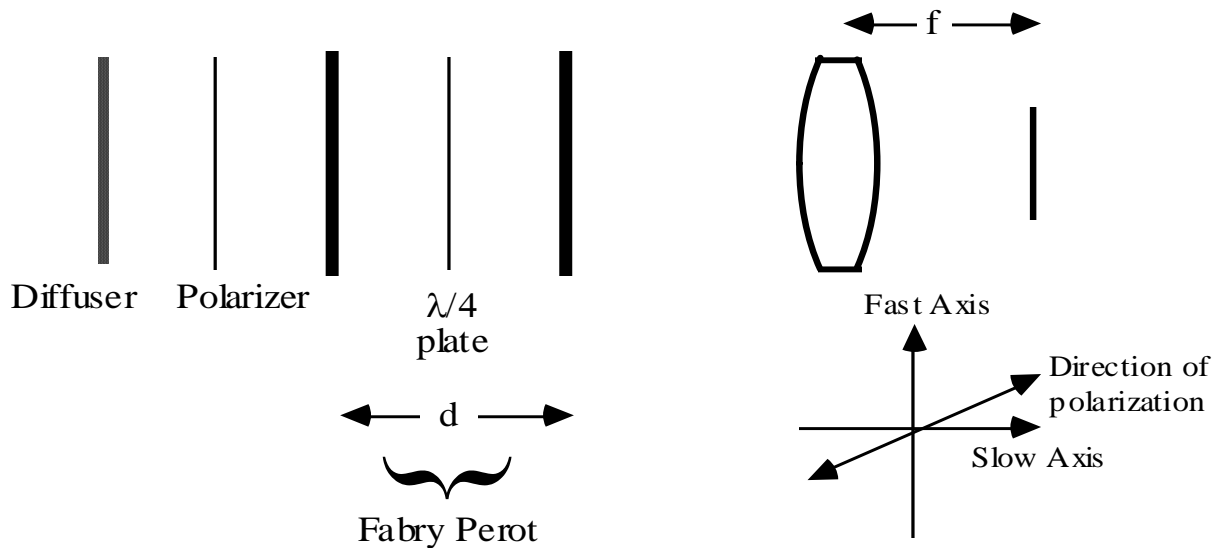
But $T_1 = 1 - R_1$ and $T_2 = 1 - R_2$. Therefore, $T_1 T_2 = 1 - R_1 - R_2 + R_1 R_2$ and

$$\frac{I_r}{I_i} = \frac{(\sqrt{R_1} - \sqrt{R_2})^2 + 4 \sqrt{R_1 R_2} \sin[\delta/2]^2}{(1 - \sqrt{R_1 R_2})^2 + 4 \sqrt{R_1 R_2} \sin[\delta/2]^2}$$

Which is the same result we had above.

MB - 3

A quarter-wave plate is placed inside a Fabry Perot cavity as shown below. The mirror separation is d . Both mirrors have an intensity reflectance of R and they introduce no phase change upon reflection and no absorption. A laser of wavelength λ is used to illuminate a diffuser placed before the Fabry Perot. Between the diffuser and Fabry Perot we place a polarizer such that the light entering the Fabry Perot is plane polarized at an angle θ with respect to the slow axis of the quarter-wave plate. Find the intensity distribution in the focal plane of the lens following the Fabry Perot. You can assume that the quarter-wave plate transmits 100% of all incident energy. Also, for simplicity assume that over the angles of interest the effective optical thickness of the quarter-wave plate is a constant.



Solution

For a normal Fabry-Perot

$$\frac{I_t}{I_i} = \frac{1}{1 + F \sin^2[\delta / 2]} ; F = \frac{4R}{(1-R)^2} ; \frac{\delta}{2} = \frac{2\pi}{\lambda} n d \cos[\theta']$$

For our problem we have two interference patterns. One pattern results from light having polarization along the slow axis, and the second pattern for light having polarization along the fast axis.

Assuming that the quarter-wave plate is independent of the angle of incidence we have

$$\text{For the fast axis} \quad \frac{\delta}{2} = \frac{2\pi}{\lambda} d \cos[\theta'] + \epsilon$$

$$\text{For the slow axis} \quad \frac{\delta}{2} = \frac{2\pi}{\lambda} d \cos[\theta'] + \epsilon + \frac{\pi}{2}$$

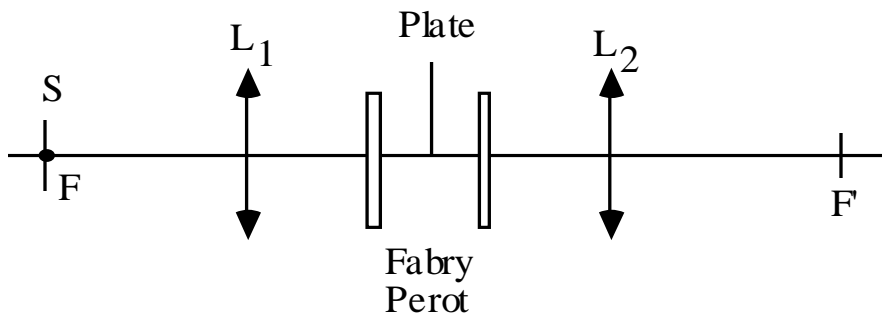
$$\frac{I_t}{I_i} = \frac{\sin^2[\theta]}{1 + F \sin^2\left[\frac{2\pi}{\lambda} d \cos[\theta'] + \epsilon\right]^2} + \frac{\cos^2[\theta]}{1 + F \cos^2\left[\frac{2\pi}{\lambda} d \cos[\theta'] + \epsilon\right]^2};$$

$$\theta' \approx \frac{\sqrt{x^2 + y^2}}{f}$$

MB - 4

The plates of a Fabry Perot etalon are held strictly parallel at a distance of 5 cm. The etalon is placed between two identical converging lenses L1 and L2 having a focal length of 15 cm. In the focal plane of L1 one places a source 1 cm in diameter (centered on the principal focus of L1). The source emits quasi-monochromatic radiation of wavelength of 500 nm. Take the index of air equal to 1.

- Calculate the interference order at point F'. How many bright fringes can one observe in the focal plane of L2?
- Between the half-silvered plates place an opaque screen which covers half the surface of these plates. How does the screen change the interference fringes observed in the focal plane of L2?
- Replace the opaque screen with a transparent 0.5 mm thick plate of index 1.5. Explain the appearance of the field in the focal plane of L2 and give the expression for the radii of the bright fringes.
- Using 25 words or less, describe what happens to the fringes if slowly a few seconds of wedge is introduced between the two Fabry Perot mirrors.



Solution

We will set the phase change due to reflection equal to zero.

■ a)

$$2 n d \cos[\theta] = m \lambda; \quad n = 1;$$

at F', $\theta = 0$

$$m = \frac{2 d}{\lambda} / . \{d \rightarrow 5 \text{ cm}, \lambda \rightarrow 500 \times 10^{-7} \text{ cm}\} = 200000$$

At the edge of the field $\theta_{\max} = \frac{0.5 \text{ cm}}{15 \text{ cm}} = \frac{1}{30}$ radian

$$m_{\text{edge}} = \frac{2 d \cos\left[\frac{1}{30}\right]}{\lambda} \text{ / . } \{d \rightarrow 5 \text{ cm}, \lambda \rightarrow 500 \times 10^{-7} \text{ cm}\} = 199889$$

Thus, there are $(200000 - 199889 + 1) = 112$ fringes

■ b)

The position and radius of the bright fringes remain unchanged, but their illumination is halved.

■ c)

We will obtain two sets of fringes - those coming from the top half of the etalon, and those coming from the bottom half. Both sets of fringes will be circular centered on F'.

For the bottom half of the etalon the expression for the appearance of bright fringes is

$$2 d \cos[\theta] = 2 d \left(1 - \frac{\theta^2}{2}\right) = m \lambda; \quad \rho = f \theta$$

where ρ is the radius of the fringe. Hence

$$\rho = f \sqrt{2 - \frac{m \lambda}{d}} \text{ / . } \{f \rightarrow 15 \text{ cm}, d \rightarrow 5 \text{ cm}, \lambda \rightarrow 500 \times 10^{-7} \text{ cm}\}$$

$$15 \text{ cm} \sqrt{2 - \frac{m}{100000}}$$

For the top half of the etalon

$$m \lambda = 2 \left((d - d_p) \cos[\theta] + n d_p \cos[\theta_p] \right)$$

where d_p is the thickness of the plate. $\theta_p = \frac{\theta}{n}$.

$$\frac{m \lambda}{2} = \left((d - d_p) \left(1 - \frac{\theta^2}{2}\right) + d_p n \left(1 - \frac{\theta^2}{2 n^2}\right) \right)$$

$$\text{theta} = \theta \text{ / . solve}\left[\frac{m \lambda}{2} == \left((d - d_p) \left(1 - \frac{\theta^2}{2}\right) + d_p n \left(1 - \frac{\theta^2}{2 n^2}\right) \right), \theta\right]$$

$$\left\{ -\frac{\sqrt{d - \frac{m \lambda}{2} - d_p + n d_p}}{\sqrt{\frac{d}{2} - \frac{d_p}{2} + \frac{d_p}{2n}}}, \frac{\sqrt{d - \frac{m \lambda}{2} - d_p + n d_p}}{\sqrt{\frac{d}{2} - \frac{d_p}{2} + \frac{d_p}{2n}}} \right\}$$

$$\rho = f \theta$$

$\rho = f \text{ Simplify}[\text{theta}[[2]]]$

$$\frac{f \sqrt{2 d - m \lambda + 2 (-1 + n) d_p}}{\sqrt{d + (-1 + \frac{1}{n}) d_p}}$$

$\text{Simplify}[\rho /. \{f \rightarrow 15 \text{ cm}, d \rightarrow 5 \text{ cm}, d_p \rightarrow .05 \text{ cm}, \lambda \rightarrow 500 \times 10^{-7} \text{ cm}, n \rightarrow 1.5\}, \{\text{cm} > 0\}]$

6.71941 cm $\sqrt{10.05 - 0.00005 m}$

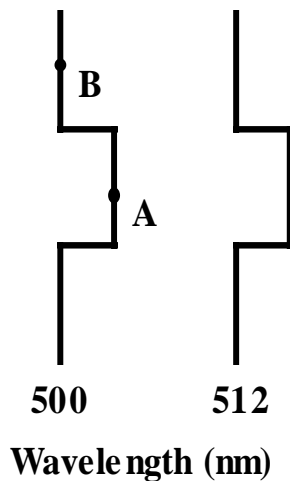
■ d)

Fringe contrast will reduce because d is not a constant value.

MB - 5

The following interferogram is obtained using a FECO interferometer to test a nearly flat mirror.

- Does point A correspond to a bump or a hole on the mirror surface?
- What is the approximate surface height difference between point A and point B?
- How would the fringes change if tilt in the x direction, or in the y direction, were introduced between the sample and the reference surface?



Solution

■ a)

The basic equation is $2 d + \frac{\phi}{\pi} \lambda = m \lambda$. That is, for a given fringe d/λ is a constant. Since λ is larger for point A than for point B, d must be larger at point A than at point B. Therefore, point A corresponds to a hole (valley) on the mirror surface.

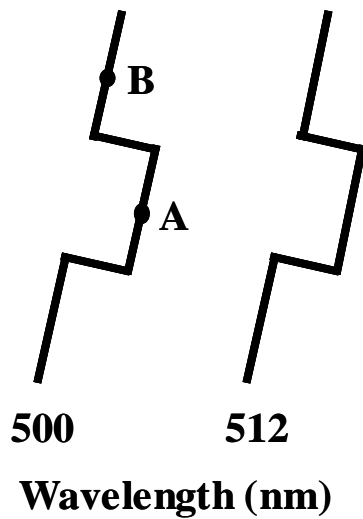
■ b)

$$d_2 - d_1 = \frac{\lambda_{1,m+1}}{\lambda_{1,m} - \lambda_{1,m+1}} \left(\frac{\lambda_{2,m} - \lambda_{1,m}}{2} \right)$$

$$d_2 - d_1 = \frac{500 \text{ nm}}{512 \text{ nm} - 500 \text{ nm}} \left(\frac{516 \text{ nm} - 512 \text{ nm}}{2} \right) = 83.33 \text{ nm}$$

■ c)

Tilt in the x-direction will not change the fringes since we are looking at a slit portion of the sample where the narrow dimension of the slit is in the x-direction. Tilt in the y-direction will cause the fringes to rotate since along a fringe d/λ is a constant.

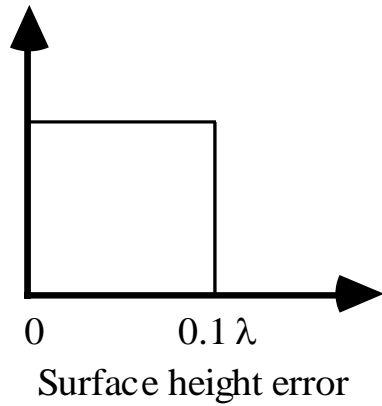


MB - 6

A Fabry Perot interferometer is made using two mirrors having 98% reflectivity.

a) What is the finesse of the interferometer?

b) Let one of the mirrors be perfectly flat while the other mirror has a surface roughness distribution as shown below. Estimate the finesse of the interferometer. (There are no height errors greater than 0.1 wave, and there is a uniform distribution for errors less than 0.1 wave.)



Solution

■ a

$$\text{finesse} = \frac{\pi \sqrt{F}}{2} = \frac{\pi \sqrt{R}}{1 - R}$$

$$\text{finesse} = \frac{\pi \sqrt{R}}{1 - R}; \quad \text{finesse} / . R \rightarrow 0.98$$

155.501

■ b

$$\text{finesse} = \frac{\text{fringe separation}}{\text{full width half max}}$$

The height variation is 0.1 wave, so the fringes will be smeared 1/5 the fringe spacing. Thus

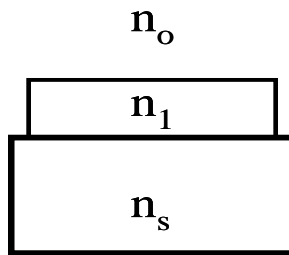
$$\text{finesse} = 5$$

MB - 7

a) Show that a film of optical thickness 1/4 wave and index n_1 will always reduce the reflectance of the substrate on which it is deposited as long as $n_s > n_1 > n_o$. Consider the simplest case of normal incidence and $n_o = 1$.

b) Show that the reflectance of a substrate can be increased by coating it with a 1/4 wave high index layer i.e., $n_1 > n_s$. Show that the reflected waves interfere constructively. The quarter-wave stack $(HL)^m$ can be thought of as a series of such structures.

c) Determine the refractive index and thickness of a film to be deposited on a glass surface ($n_g = 1.54$) such that no normally incident light of wavelength 540 nm is reflected.

Solution**■ a**

$$n_s > n_1 > n_o$$

Same phase change on reflection of $n_o n_s$ and $n_1 n_s$ boundary, therefore two reflected rays are 180° out of phase and destructively interfere. Also, since $n_1 < n_s$ and $n_1 > n_o$, amount reflected off each interface must be less than amount reflected off $n_o n_s$ interface.

■ b

$$n_1 > n_s$$

Phase between two reflected beams is

$$\frac{2\pi}{\lambda} \left(\frac{1}{4} \lambda \right) (2) + \pi = 2\pi$$

Therefore, the waves are in phase and interfere constructively.

■ c

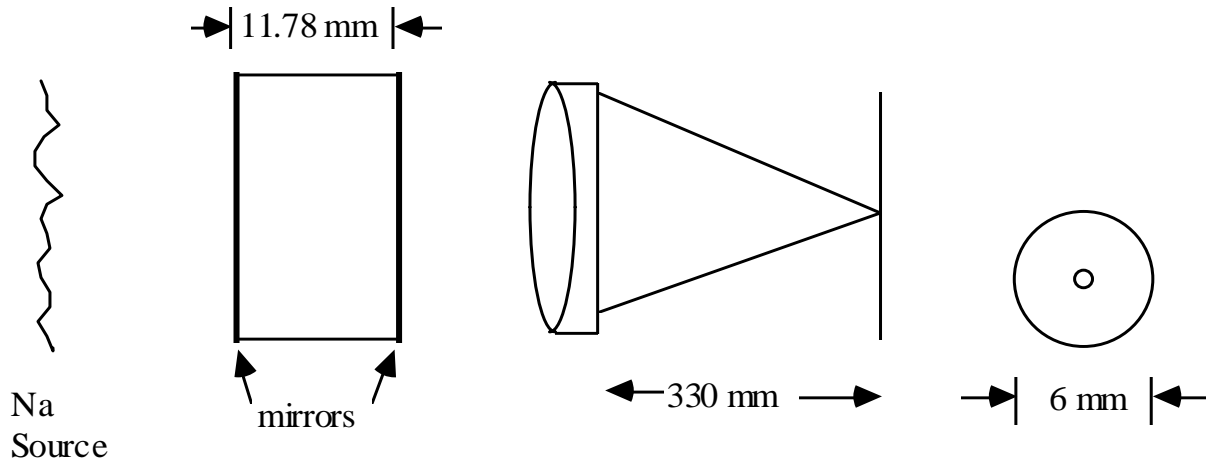
$$n_1 = \sqrt{1.54} = 1.24$$

$$n d = \frac{\lambda}{4}$$

$$d = \frac{\lambda}{4 n} = \frac{0.540 \mu\text{m}}{4 (1.24)} = 0.11 \mu\text{m}$$

MB - 8

A slab of optically homogeneous material of unknown refractive index is illuminated with yellow light (wavelength = 589 nm) from a sodium lamp. The surfaces of the slab are coated with semi-transparent mirrors and the thickness of the slab is 11.78 mm. The focal length F of the lens is 330 mm. A bright spot is at the center of the screen and the diameter of the first bright fringe is 6 mm. What is the refractive index of the material?



Solution

First we will find the angle outside the slab for the first bright fringe from the center.

$$\theta_o = \frac{3 \text{ mm}}{330 \text{ mm}} = \frac{1}{110}$$

The corresponding angle inside the slab is

$$\theta = \frac{\theta_o}{n}$$

Since we also have a bright fringe at the center of the pattern we know that

$$2 n d - 2 n d \cos [\theta] = \lambda$$

d is the thickness of the slab, $d = 11.78 \text{ mm}$.

From above

$$2 n d - 2 n d \left(1 - \frac{\theta^2}{2} \right) = \lambda$$

or

$$n d \theta^2 = \lambda = n d \left(\frac{\theta_o}{n} \right)^2 = \frac{d \theta_o^2}{n}$$

$$n = \frac{d \theta_o^2}{\lambda} = \frac{11.78 \times 10^3 \mu\text{m} \left(\frac{1}{110} \right)^2}{0.589 \mu\text{m}} = 1.65289$$

MB - 9

Determine the refractive index and thickness of a thin film to be deposited on a glass surface ($n_g = 1.54$) such that no normally incident light of wavelength 633 nm is reflected. If the angle of incidence (incident from air to thin film) changes to 5 degrees, what is the wavelength for minimum reflection?

Solution

$$n = \sqrt{n_o n_g} = \sqrt{1 (1.54)} = 1.24$$

$$n d = \frac{\lambda}{4}$$

$$d = \frac{\lambda}{4 n} = \frac{0.633 \mu\text{m}}{4 (1.24)} = 0.13 \mu\text{m}$$

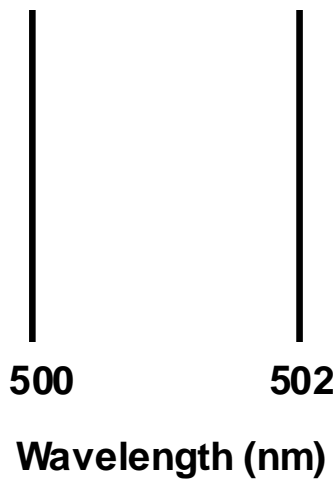
Using my favorite equation, $2 n d \cos[\theta] = m \lambda$, we see that as θ increases, $\cos[\theta]$ decreases and the wavelength must decrease to keep the two sides of the equation equal.

$$\lambda_{\text{new}} = \lambda \cos[\theta] = 0.633 \mu\text{m} \cos[5 \text{ Degree}] = 0.63059 \mu\text{m}$$

MB - 10

The following two fringes were obtained using a FECO to test two flat mirrors.

- What is the order number for the left fringe?
- What is the separation between the two mirrors?
- What would the fringes look like if one of the mirrors had a 250 nm high spot in the center?
- How would the fringe spacing change if the mirror separation were doubled?



Solution

For the two fringes we have

$$2d = m\lambda_{\text{left}}; \quad 2d = (m-1)\lambda_{\text{right}};$$

$$\lambda_{\text{left}} = 500 \text{ nm}; \quad \lambda_{\text{right}} = 502 \text{ nm};$$

■ a)

$$\text{ans} = \text{Solve}[m\lambda_{\text{left}} == (m-1)\lambda_{\text{right}}, m]$$

$$\left\{ \left\{ m \rightarrow -\frac{\lambda_{\text{right}}}{\lambda_{\text{left}} - \lambda_{\text{right}}} \right\} \right\}$$

$$\text{ans} /. \{\lambda_{\text{left}} \rightarrow 500 \text{ nm}, \lambda_{\text{right}} \rightarrow 502 \text{ nm}\}$$

$$\{ \{ m \rightarrow 251 \} \}$$

■ b)

$$d = \frac{m\lambda_{\text{left}}}{2} /. \{m \rightarrow 251, \lambda_{\text{left}} \rightarrow 0.5 \mu\text{m}\}$$

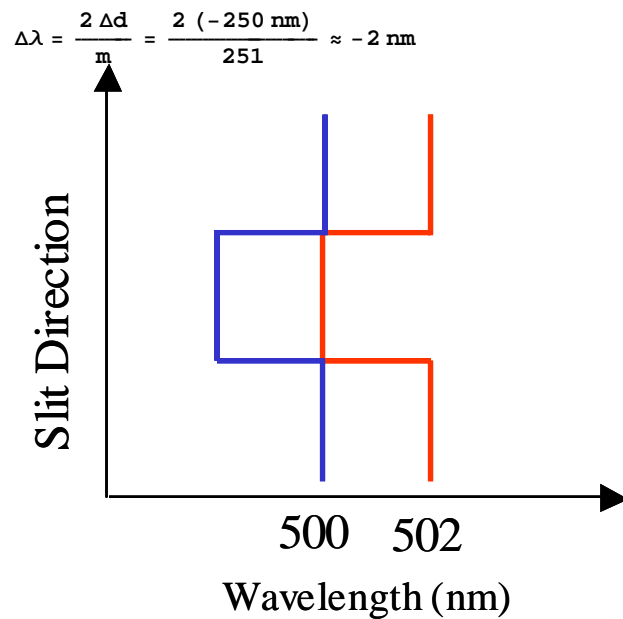
$$62.75 \mu\text{m}$$

■ c)

$$2d = m\lambda$$

Taking the derivative of both sides to see how the wavelength would change if d changes yields

$$2\Delta d = m\Delta\lambda$$



■ d)

$$2 d = m \lambda$$

Taking derivatives of both sign and letting $\Delta m = 1$

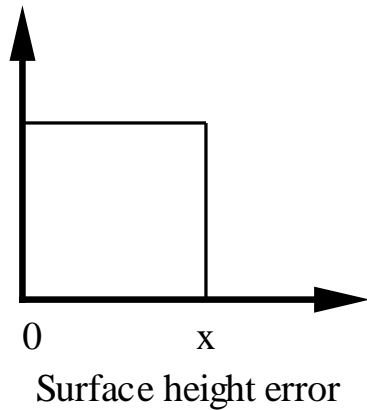
$$0 = m \Delta\lambda + \lambda$$

$$\Delta\lambda = \frac{-\lambda}{m} = \frac{-\lambda^2}{2 d}$$

Thus, doubling the mirror separation would cause the difference in wavelength for two adjacent fringes to reduce by a factor of 2.

MB - 11

A Fabry Perot interferometer is made using two mirrors having nearly 100 % reflectivity. While one of the mirrors is very flat, the other mirror has the surface roughness distribution shown below. The finesse of the fringes is measured to be 10. What is the maximum surface height error (shown as x in the figure) in units of the wavelength of light used in the interferometer?



Solution

A finesse of 10 means the fringes are smeared $1/10$ th of a fringe. The OPD is thus $1/10 \lambda$ and the surface height error is one-half of this or 0.05λ .

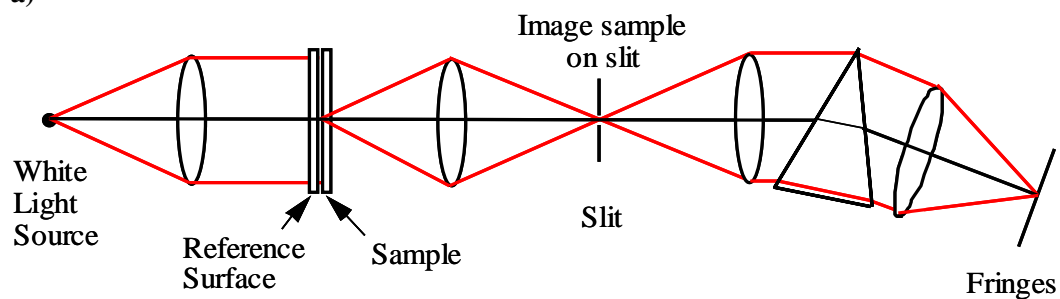
MB - 12

I am using a FEKO interferometer to measure the surface roughness of a bare piece of glass.

- Sketch the interferometer.
- What must I do to the bare piece of glass before the test?
- Sketch the fringes one would obtain if we are observing a nearly flat surface with a small bump. Carefully label the x and y axes of the plot.

Solution

■ a)



■ b)

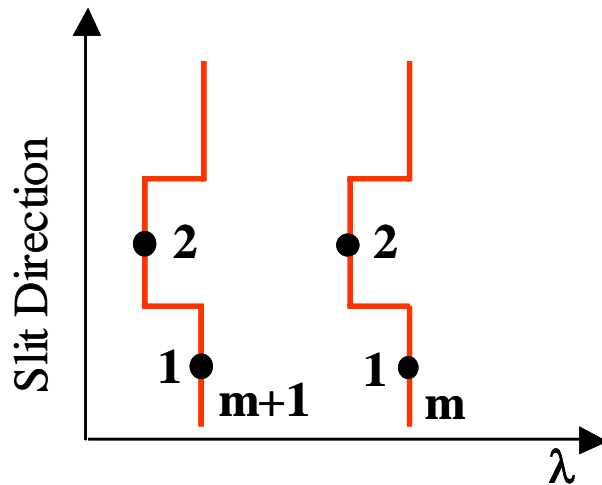
The glass must be coated to have a high reflectivity.

■ c)

For a given fringe

$$2 n d = m \lambda$$

For a bump d becomes smaller, so the wavelength will become smaller.



MB - 13

A film of optical thickness $1/4$ wave and index n_1 is placed on a substrate of index n_s . The film is used at normal incidence in air. Give a relationship between n_1 and n_s that will always cause the film to reduce the reflectivity? Explain.

Solution

$$n_s > n_1 > n_a$$

Same phase change on reflection of $n_a n_s$ and $n_1 n_s$ boundary, therefore two reflected rays are 180° out of phase and destructively interfere. Also, since $n_1 < n_s$ and $n_1 > n_a$, amount reflected off each interface must be less than amount reflected off $n_a n_s$ interface.

MB - 14

The so-called characteristic matrix was found to be very useful in analyzing multilayer films.

- a) How many elements are in the characteristic matrix?
- b) What does the characteristic matrix relate?
- c) What boundary conditions were used in deriving the characteristic matrix?
- d) Let us use the characteristic matrix to design an AR coating for wavelength λ_1 at normal incidence. Will the wavelength for minimum reflectance increase or decrease if the angle of incidence is changed to 5 degrees?

Solution**■ a)**

4

■ b)

The characteristic matrix relates the E and H fields at two adjacent boundaries.

■ c)

The tangential components of E and H are continuous across the boundaries.

■ d)

Using my favorite equation, $2 n d \cos[\theta] = m \lambda$, we see that as θ increases, $\cos[\theta]$ decreases and the wavelength must decrease to keep the two sides of the equation equal.

MB - 15

I am using a FECO interferometer to measure the surface of a highly reflecting piece of glass. The glass surface is flat except for a small area 200 nm high bump in the middle of the sample. Neglect any phase change upon reflection.

- The wedge between the sample and the reference is minimized and the separation between the flat portion of the sample and the reference surface is 2000 nm. Neglecting any phase change upon reflection, sketch the fringes for fringe order 8, 9, and 10. Carefully label the x and y axes of the plot.
- Repeat part a for the case where 2 fringes of tilt are introduced between the sample and reference and the tilt is along the long direction of the slit in the FECO interferometer. The average separation between the sample and reference is kept at 2000 nm.
- Repeat part b for the case where the tilt is perpendicular to the long direction of the slit.

Solution

$$2d = m\lambda;$$

$$\lambda[d_, m_] := \frac{2d}{m}$$

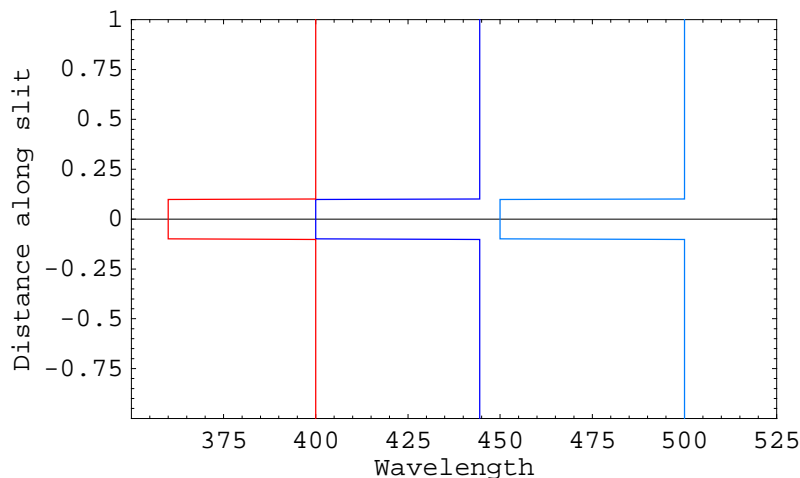
■ a)

$$\lambda[2000 \text{ nm}, 8] = 500 \text{ nm}; \quad \lambda[1800 \text{ nm}, 8] = 450 \text{ nm};$$

$$\lambda[2000 \text{ nm}, 9] = 444 \text{ nm}; \quad \lambda[1800 \text{ nm}, 9] = 400 \text{ nm};$$

$$\lambda[2000 \text{ nm}, 10] = 400 \text{ nm}; \quad \lambda[1800 \text{ nm}, 10] = 360 \text{ nm};$$

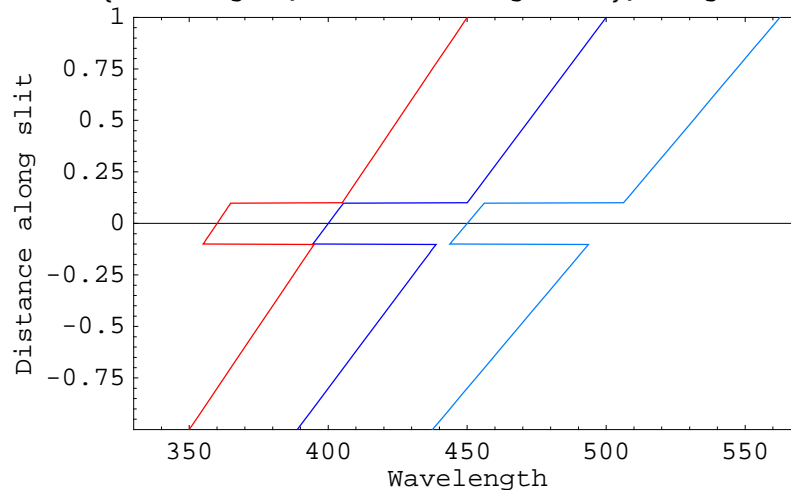
```
ParametricPlot[{ {λ[If[Abs[t] > .1, 2000, 1800], 8], t},
  {λ[If[Abs[t] > .1, 2000, 1800], 9], t}, {λ[If[Abs[t] > .1, 2000, 1800], 10], t}},
  {t, -1, 1}, PlotRange -> {{350, 525}, {-1, 1}},
  PlotStyle -> {RGBColor[0, .5, 1], RGBColor[0, 0, 1], RGBColor[1, 0, 0]}, Frame -> True,
  FrameLabel -> {"Wavelength", "Distance along slit"}, Background -> White];
```



■ b)

Same as above except tilt causes a variation of d along the slit of one wavelength. I did not give the wavelength for which we have 2 tilt fringes, but let pick the wavelength to be 500 nm. Then the tilt causes the value of d to vary by 500 nm. Letting the slit coordinate t go from -1 to 1 then the variation of d due to tilt can be written as $250 t$. Thus, d over the flat region can be written as $2000 + 250 t$ and over the step region d can be written as $1800 + 250 t$.

```
ParametricPlot[{{λ[If[Abs[t] > .1, 2000 + 250 t, 1800 + 250 t], 8], t},
  {λ[If[Abs[t] > .1, 2000 + 250 t, 1800 + 250 t], 9], t},
  {λ[If[Abs[t] > .1, 2000 + 250 t, 1800 + 250 t], 10], t}},
{t, -1, 1}, PlotRange -> {{330, 570}, {-1, 1}},
PlotStyle -> {RGBColor[0, .5, 1], RGBColor[0, 0, 1], RGBColor[1, 0, 0]}, Frame -> True,
FrameLabel -> {"Wavelength", "Distance along slit"}, Background -> White];
```



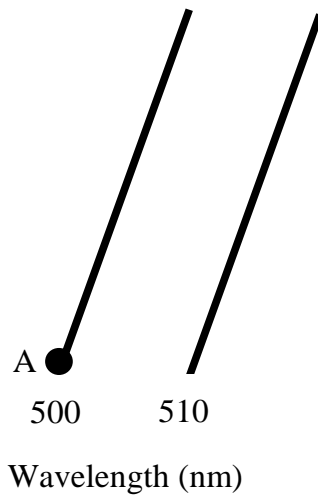
■ c)

Since the tilt is perpendicular to the slit the tilt will not change the results and the fringes are the same as in part a.

MB - 16

The following interferogram is obtained using a FECO interferometer to test a 5 cm x 5 cm square flat mirror.

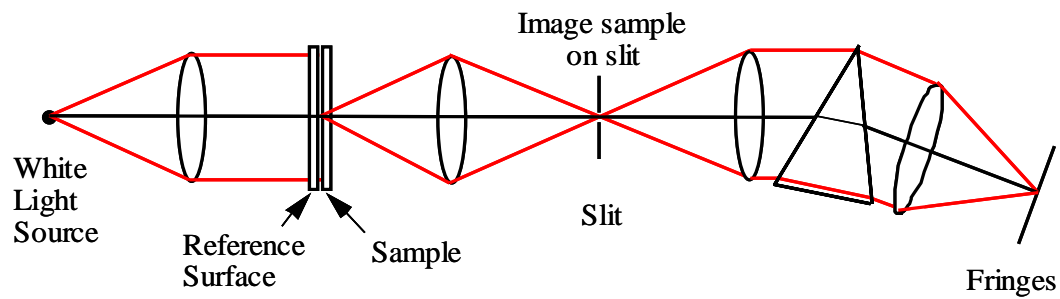
- Sketch the interferometer.
- For point A, what is the separation between the sample being measured and the reference surface?
- What is the wedge angle between the sample being measured and the reference surface?



State any assumptions you are making.

Solution

■ a



■ b

$$2d = m\lambda_1 = (m+1)\lambda_2, \text{ therefore } m = 50$$

$$d = \frac{50 (0.510 \mu\text{m})}{2}$$

12.75 μm

■ c

Let Δd be the OPD due to wedge

$$\Delta d = \frac{m \Delta \lambda}{2} \quad / . \{ m \rightarrow 51, \Delta \lambda \rightarrow 10 \text{ nm} \}$$

255 nm

$$\text{wedgeAngle} = \frac{255 \text{ nm}}{5 \cdot 10^7 \text{ nm}} // \text{N}$$
$$5.1 \times 10^{-6}$$

Thus, the wedge angle is approximately 1 arc second.